

Lecture 1
Tue. 8.25.2015

Axiomatic development of classical mechanics

(Ch. 1 and Ch. 2 of Unit 1)

Geometry of momentum conservation axiom

*Totally Inelastic “ka-runch” collisions**

*Perfectly Elastic “ka-bong” and Center Of Momentum (COM) symmetry**

Comments on idealization in classical models

Geometry of Galilean translation symmetry

45° shift in (V_1, V_2) -space

Time reversal symmetry

...of COM collisions

Algebra, Geometry, and Physics of momentum conservation axiom

Vector algebra of collisions

Matrix or tensor algebra of collisions

Deriving Energy Conservation Theorem

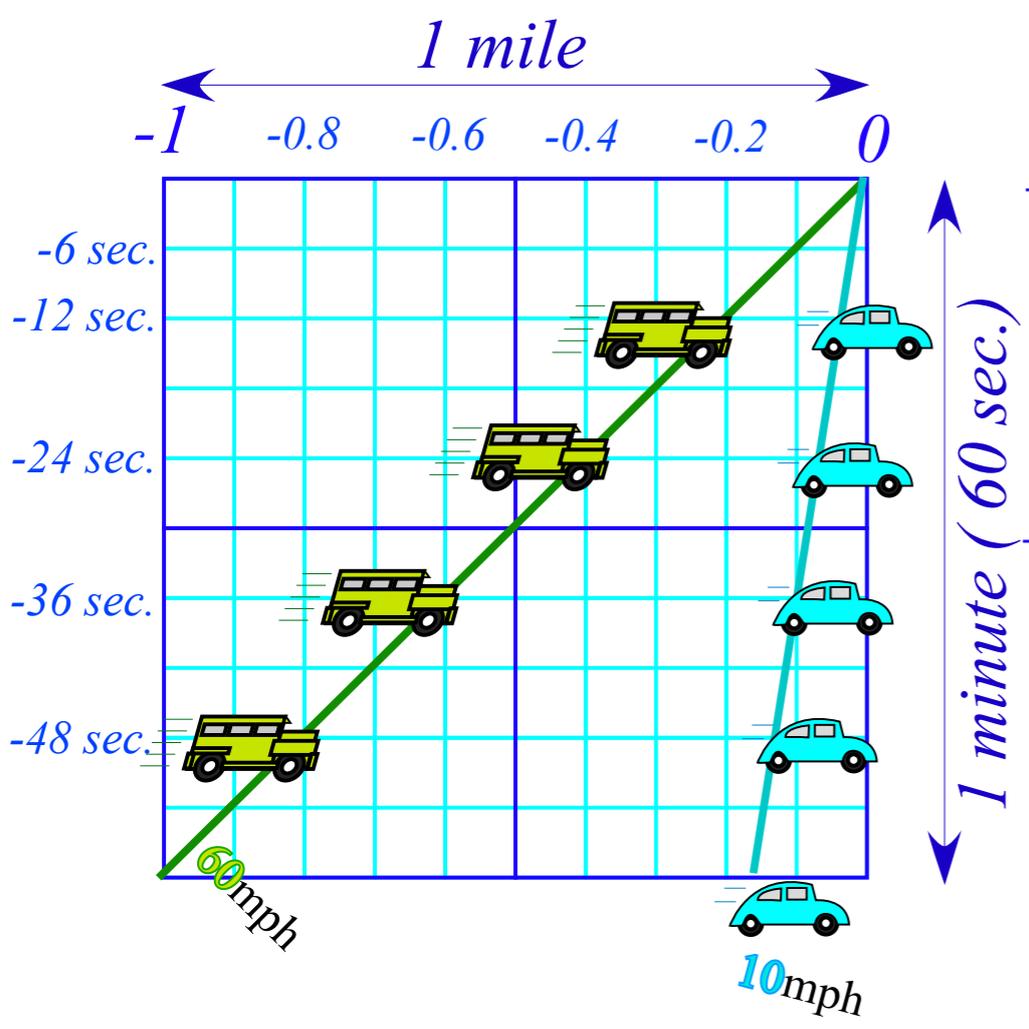
Numerical details of collision tensor algebra

**Car Collision simulator <http://www.uark.edu/ua/modphys/testing/markup/CMMotionWeb.html>*

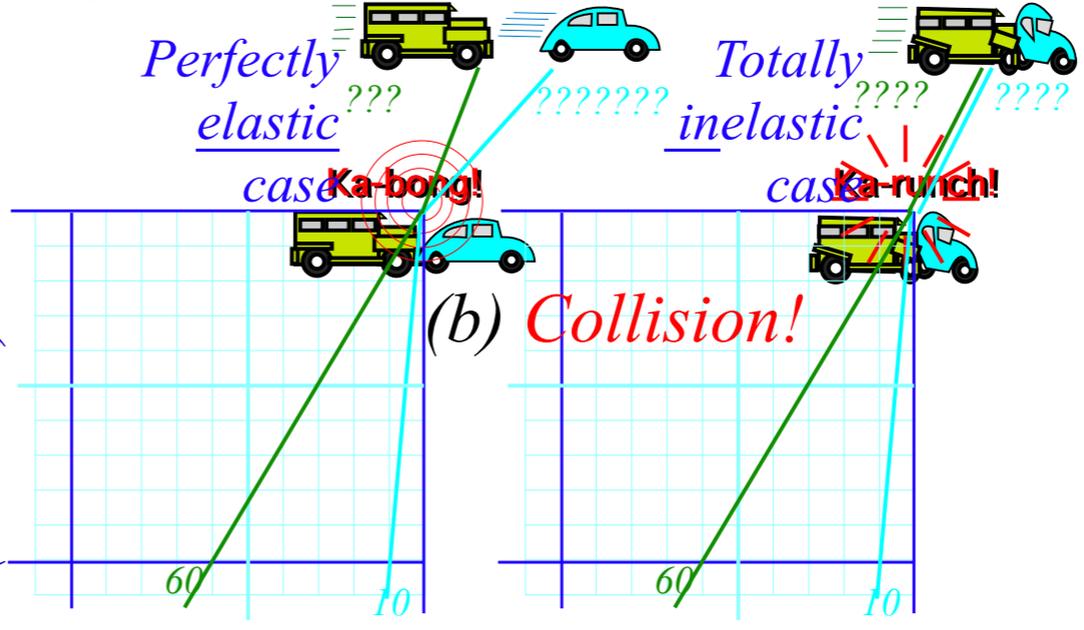
**Download Superball Collision Simulator <http://www.uark.edu/ua/modphys/testing/markup/BounceItWeb.html>*

A problem in *space-time* : (60mph Cell-faxing 4ton SUV rear-ends 10mph 1ton VW)

Before collision.....



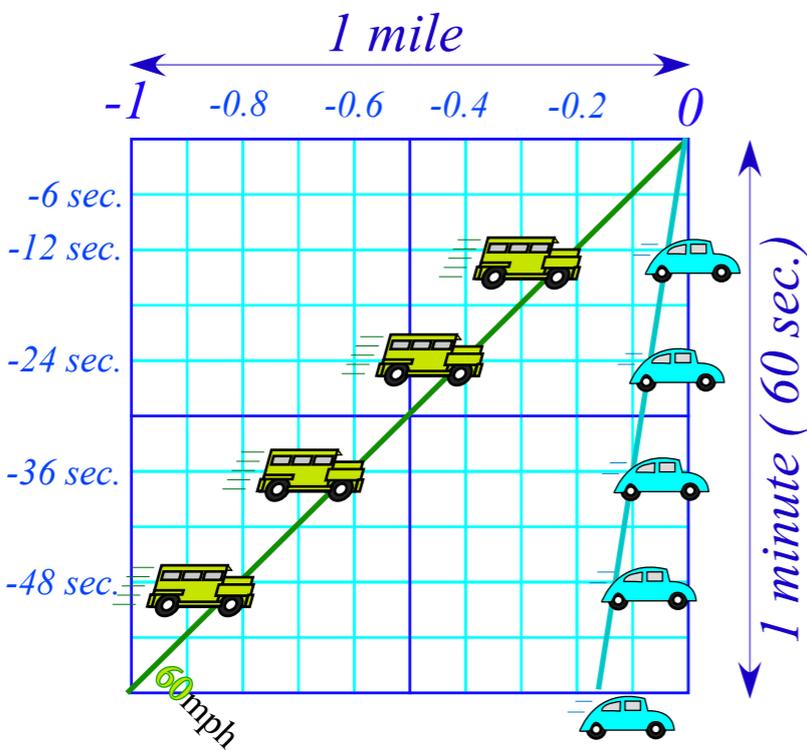
After collision...what velocities?



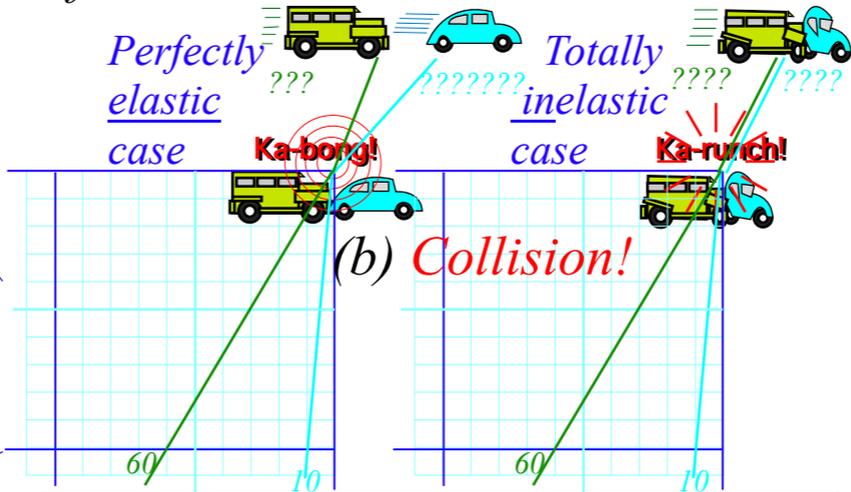
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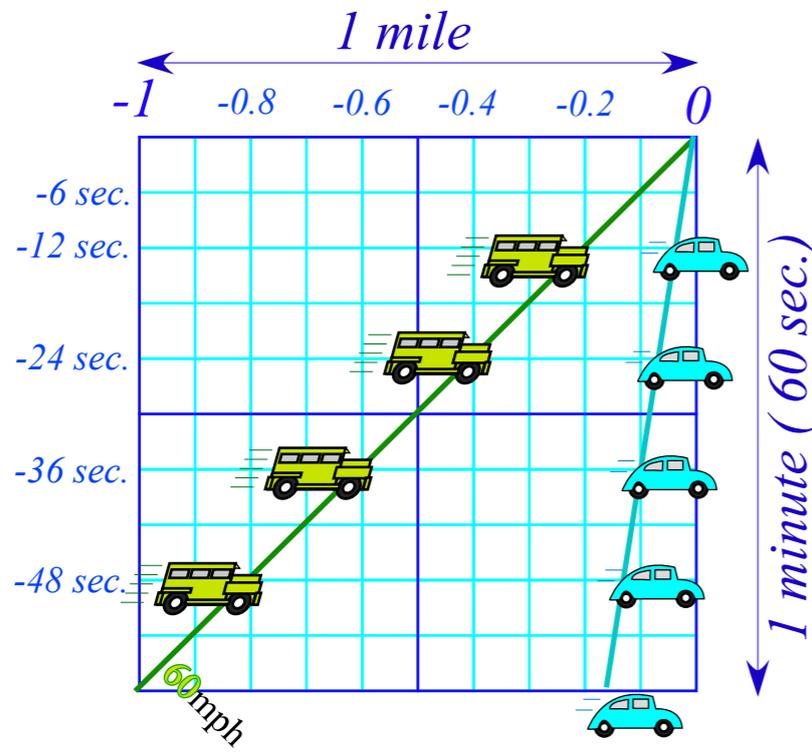


Conventional solution: Look up the usual momentum and energy formulas/axioms:
 $\sum_i m V_i(\text{initial}) = \sum_i m V_i(\text{final})$
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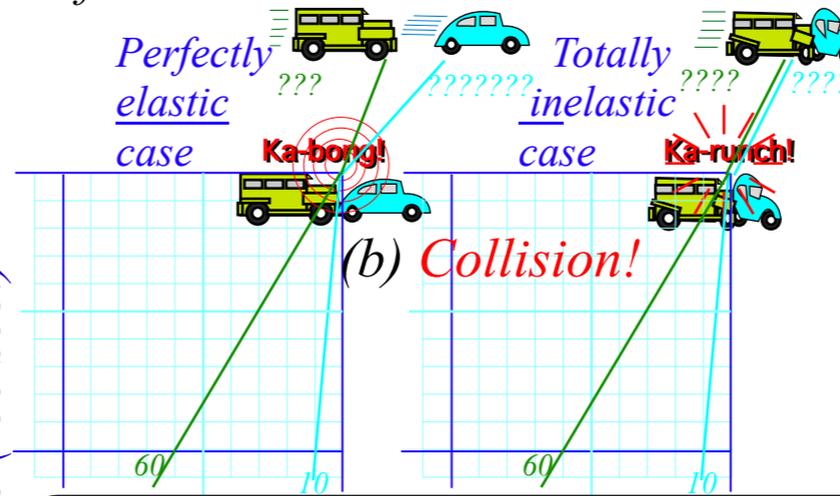
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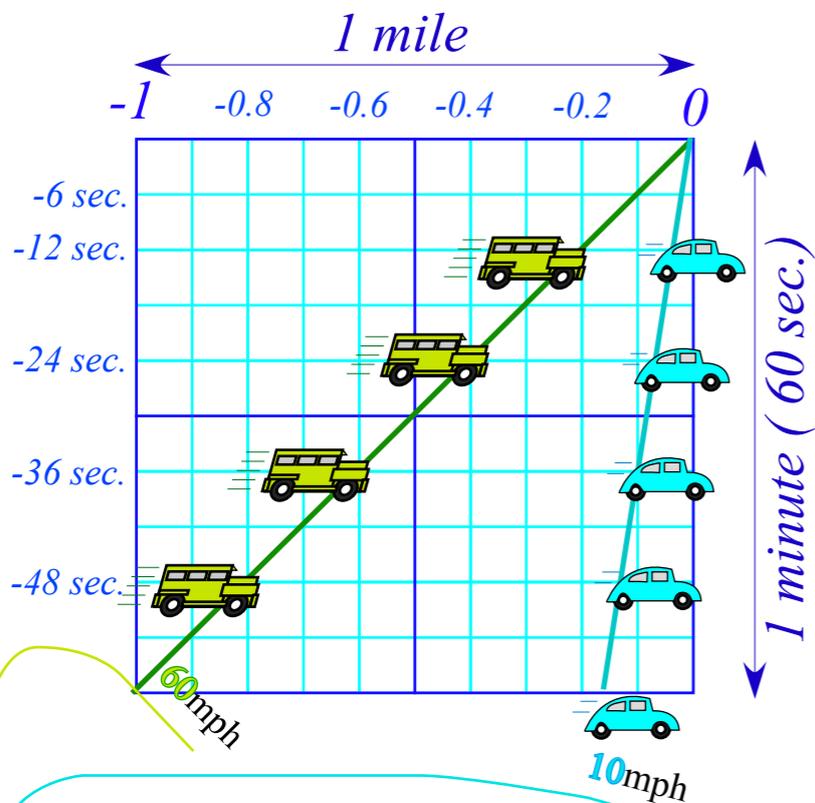
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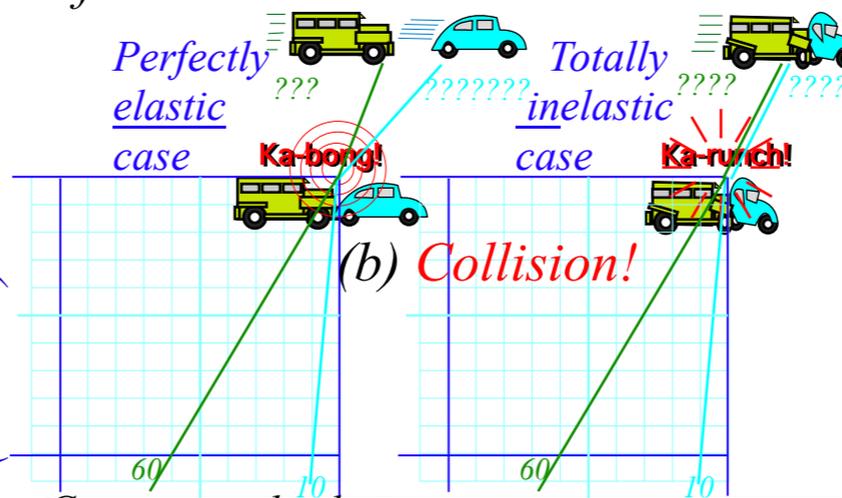
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..... (Just have to draw 2 lines!)

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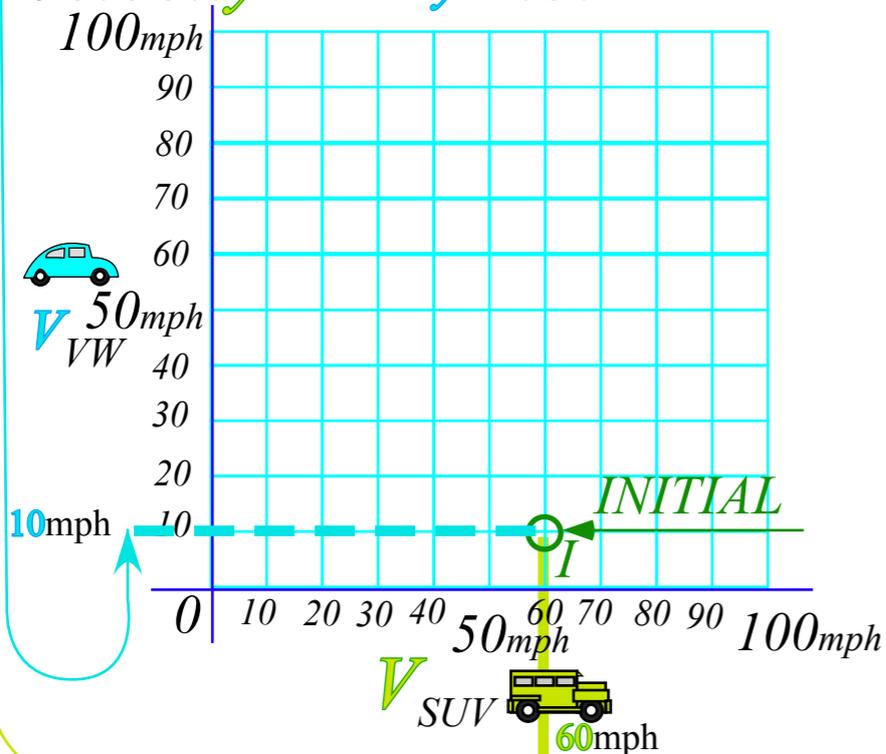
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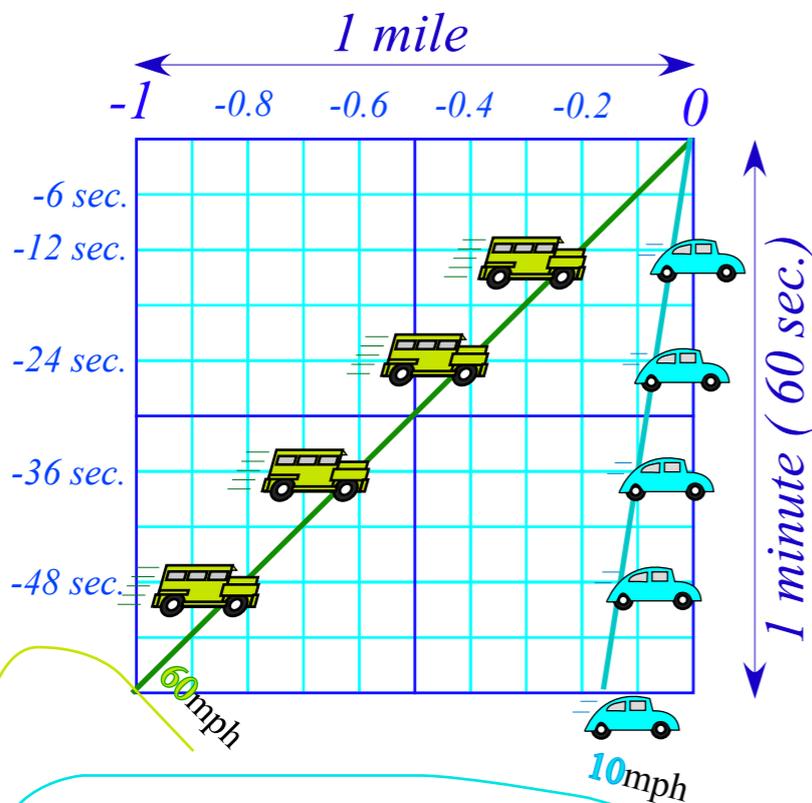
Velocity-velocity Plot



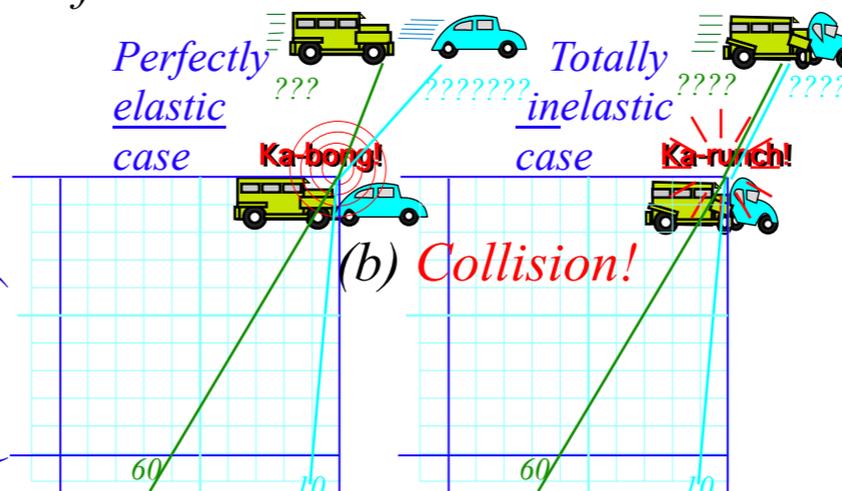
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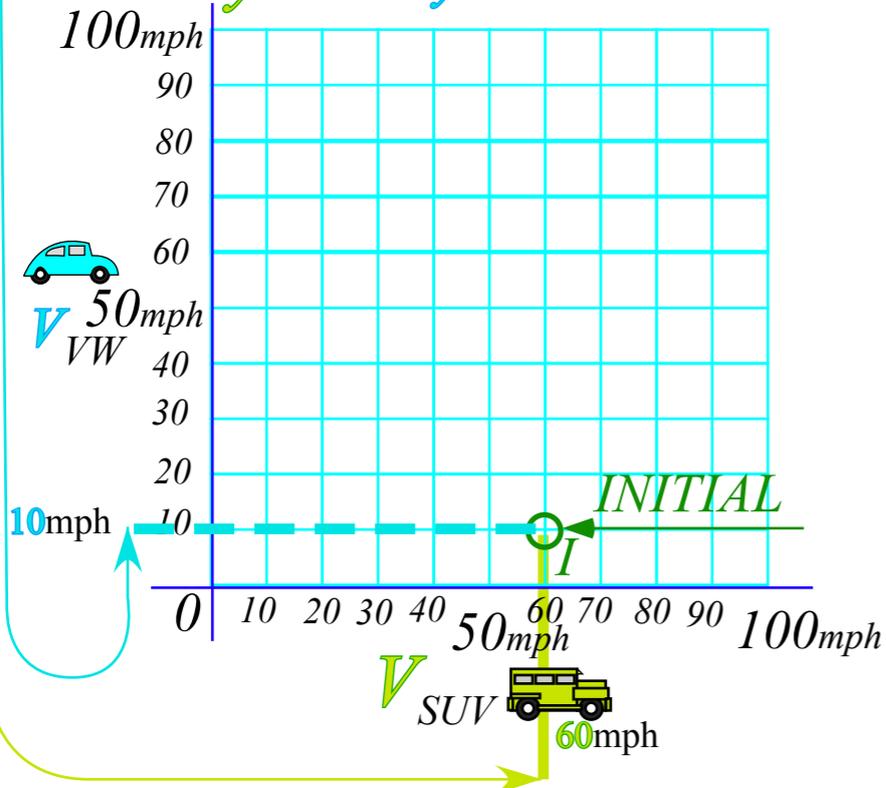
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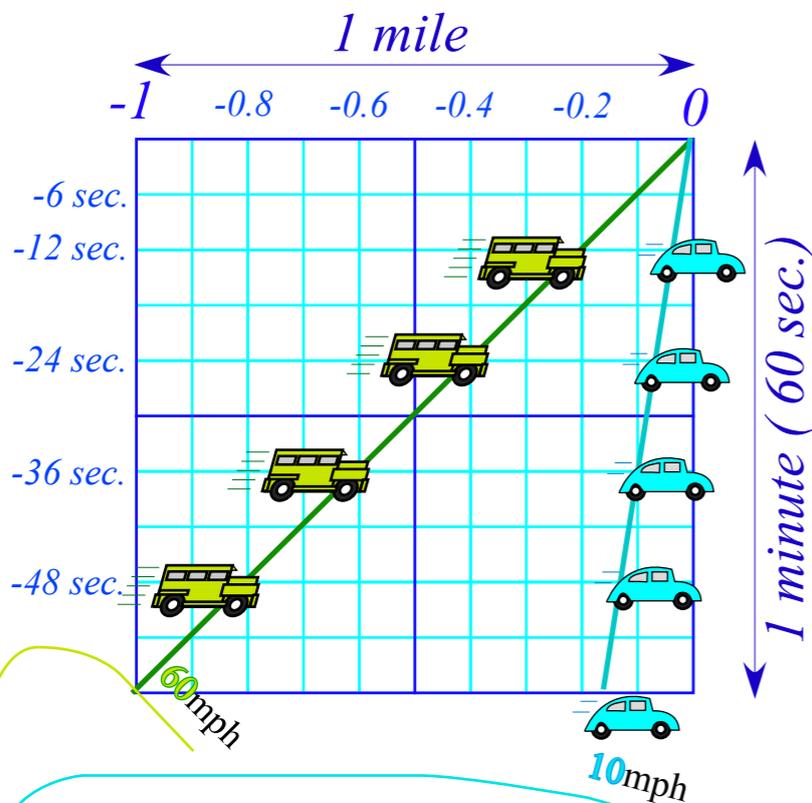
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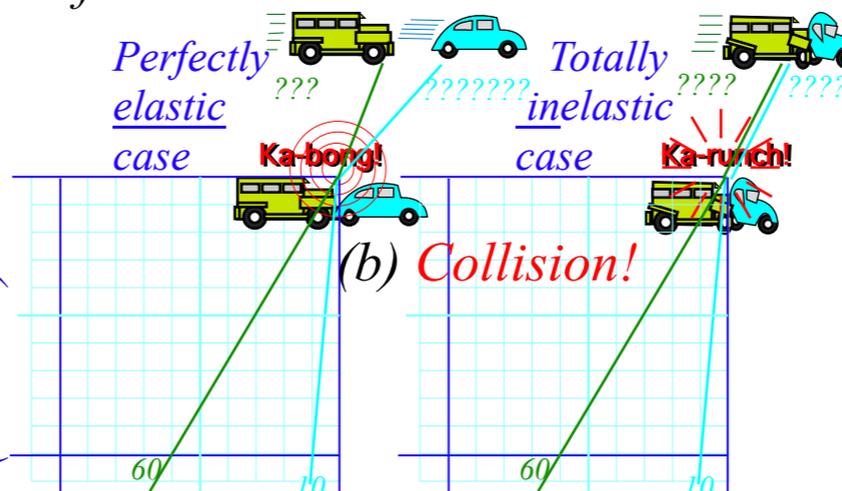
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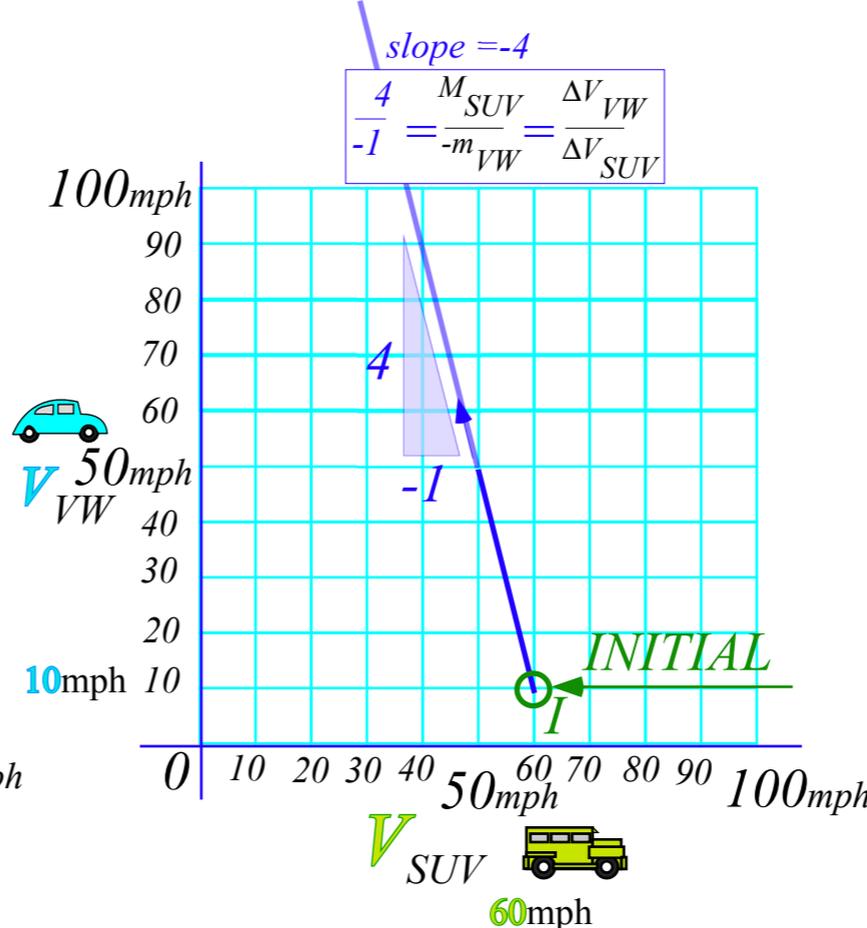
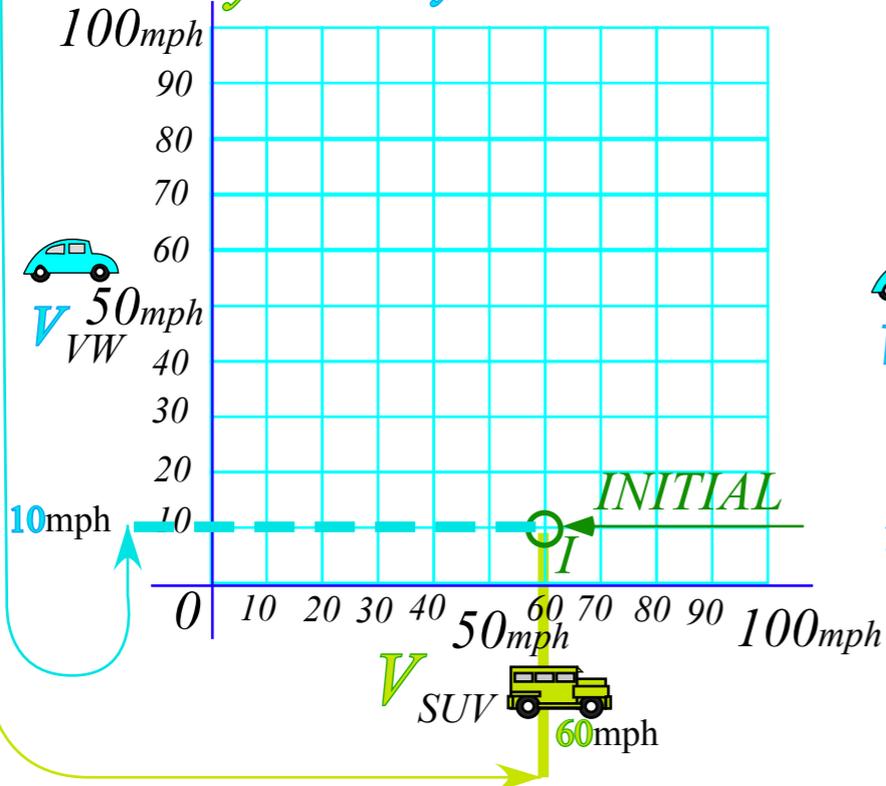
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Geometry of momentum conservation axiom

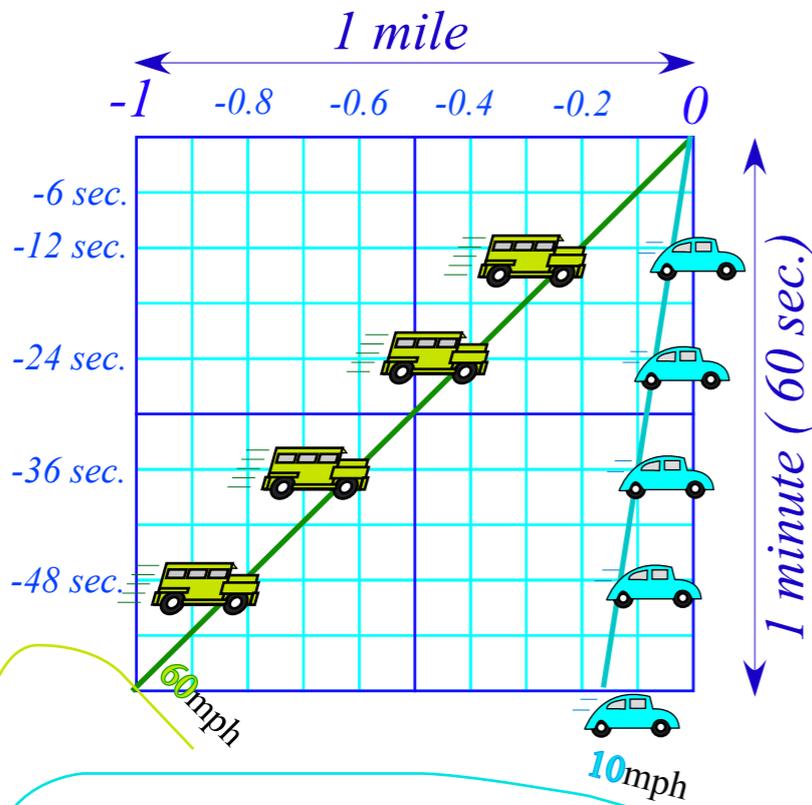
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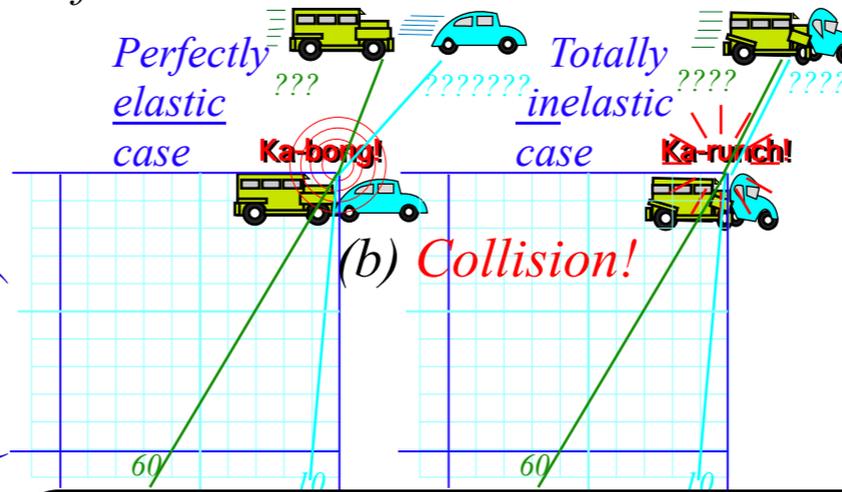
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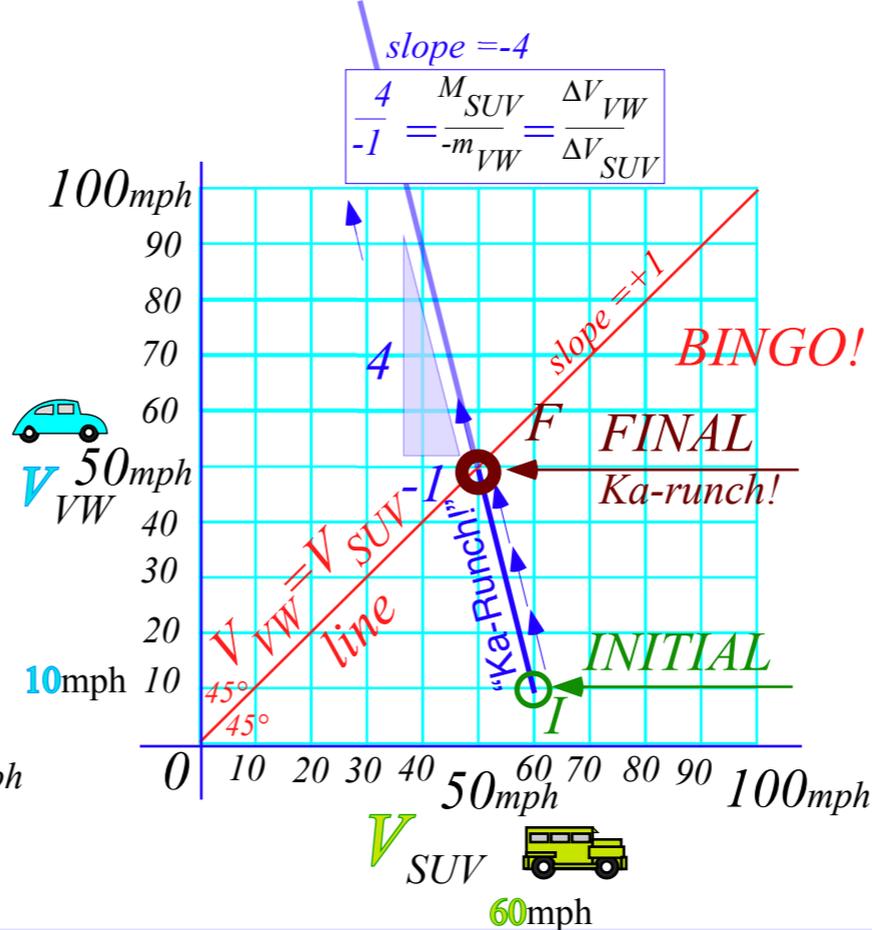
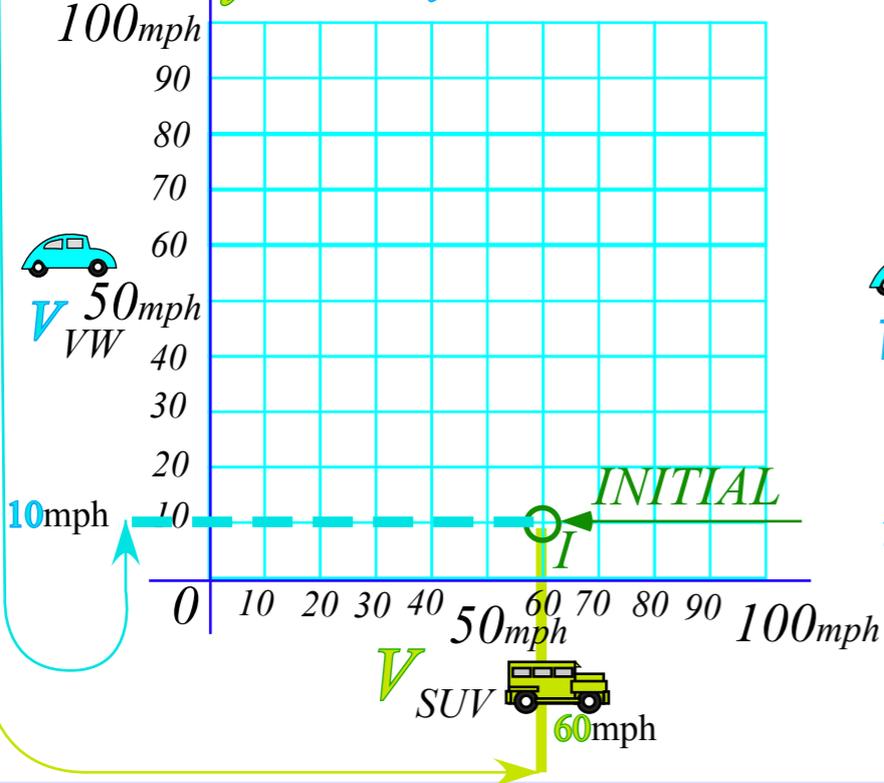
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Velocity-velocity Plot



Totally Inelastic
 (Ka - Runch!)

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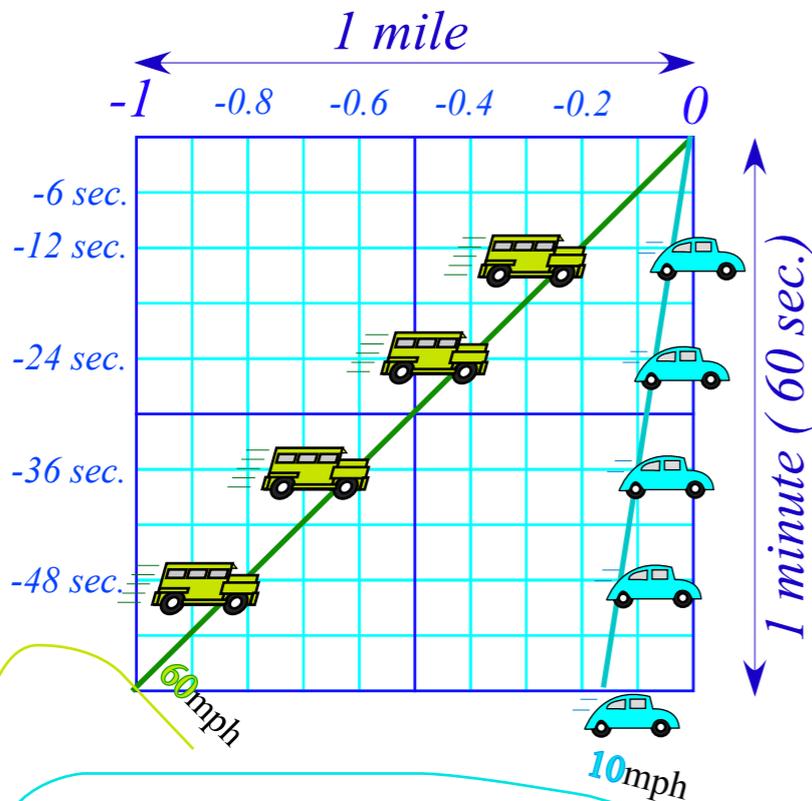
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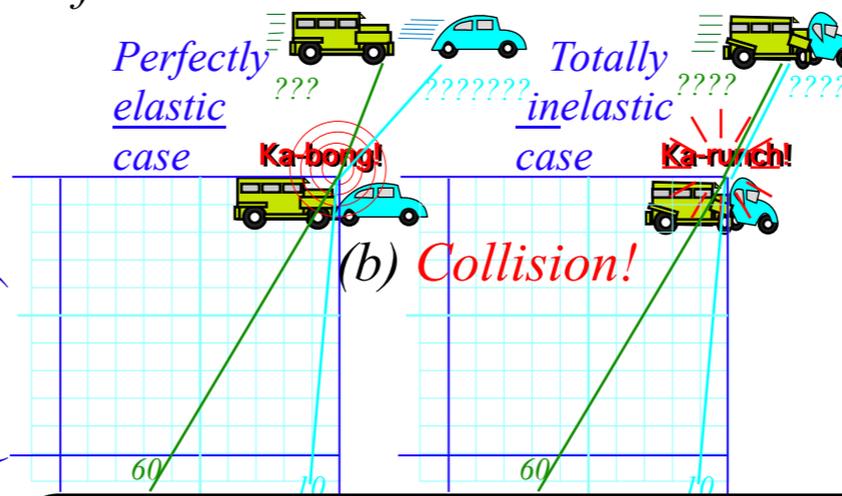
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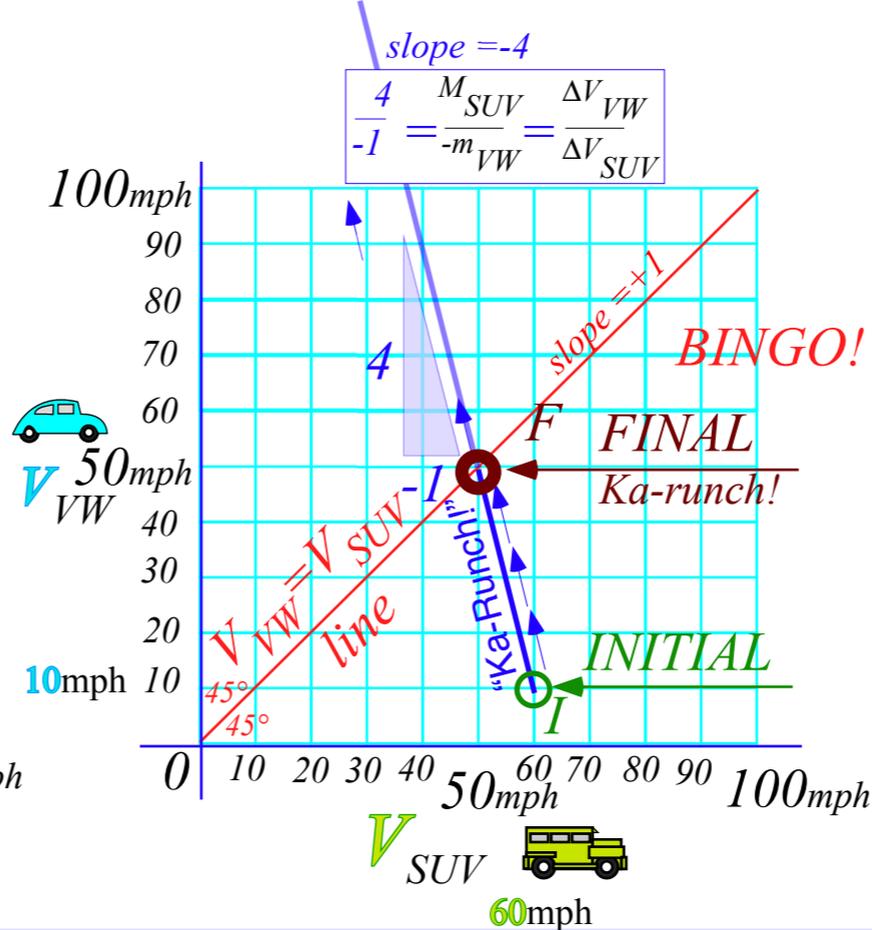
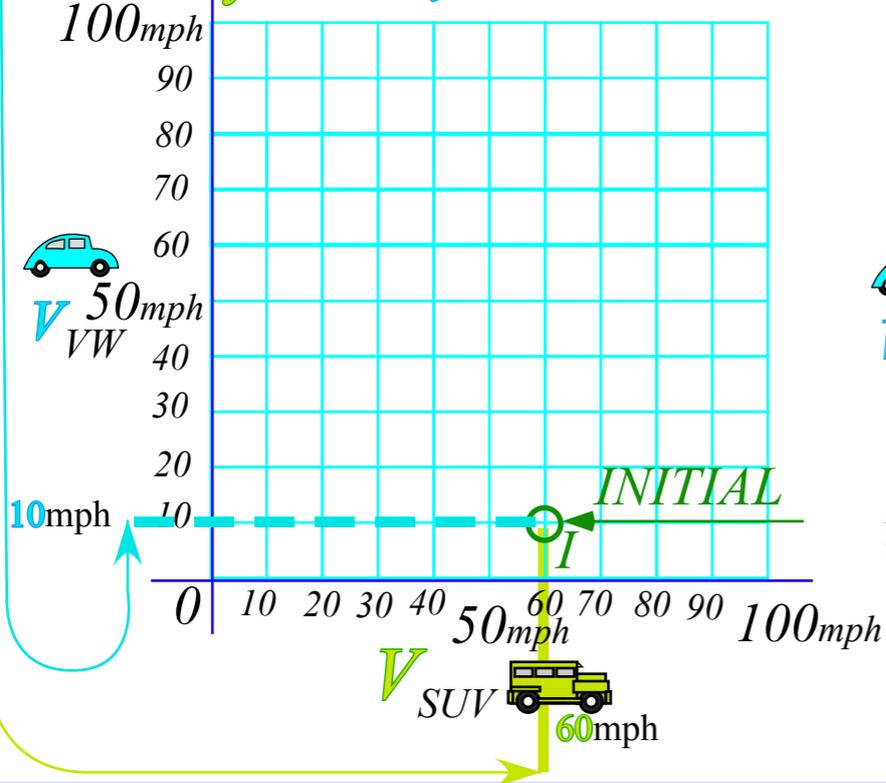
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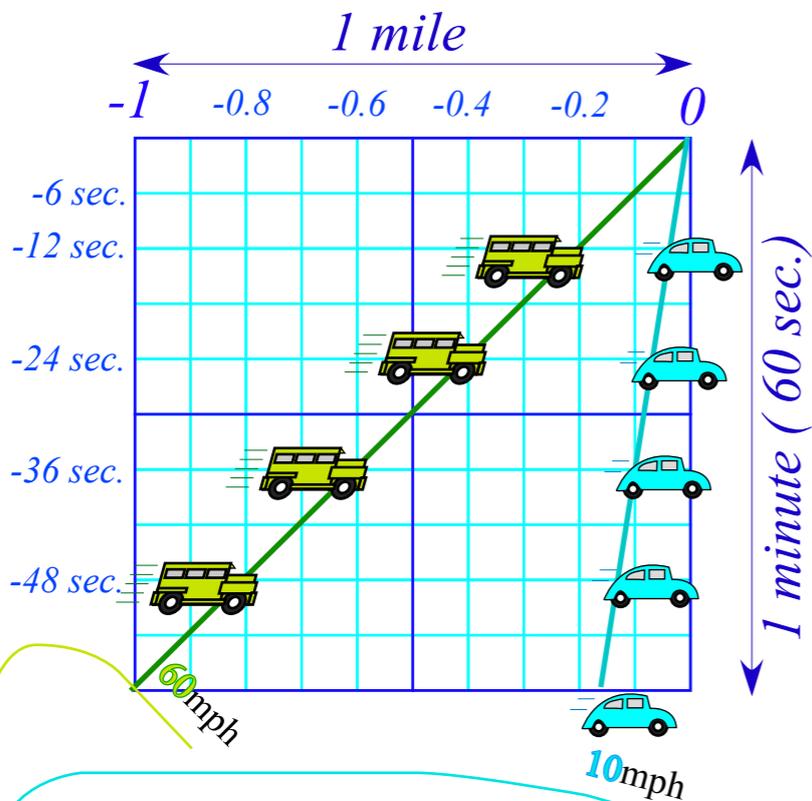
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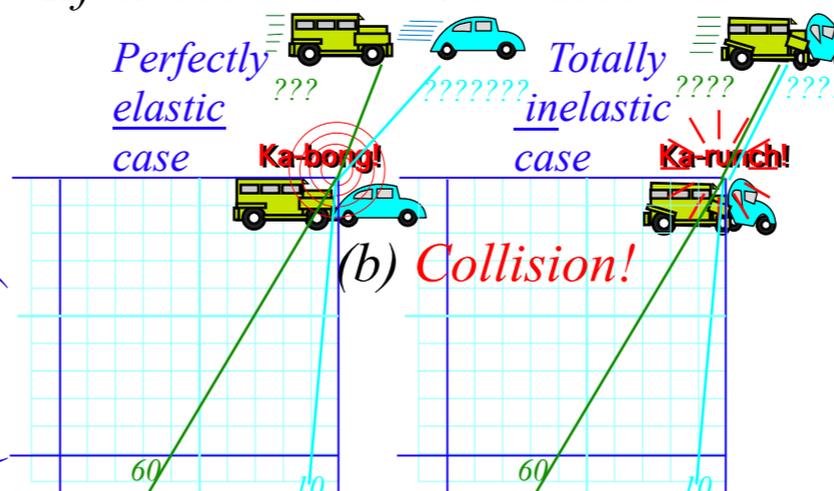
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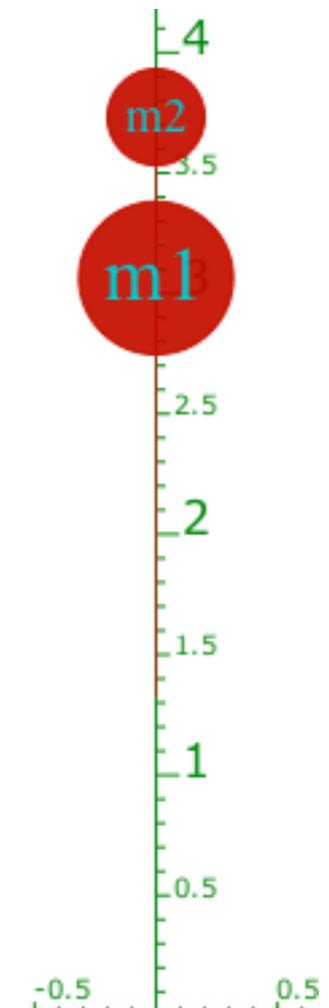
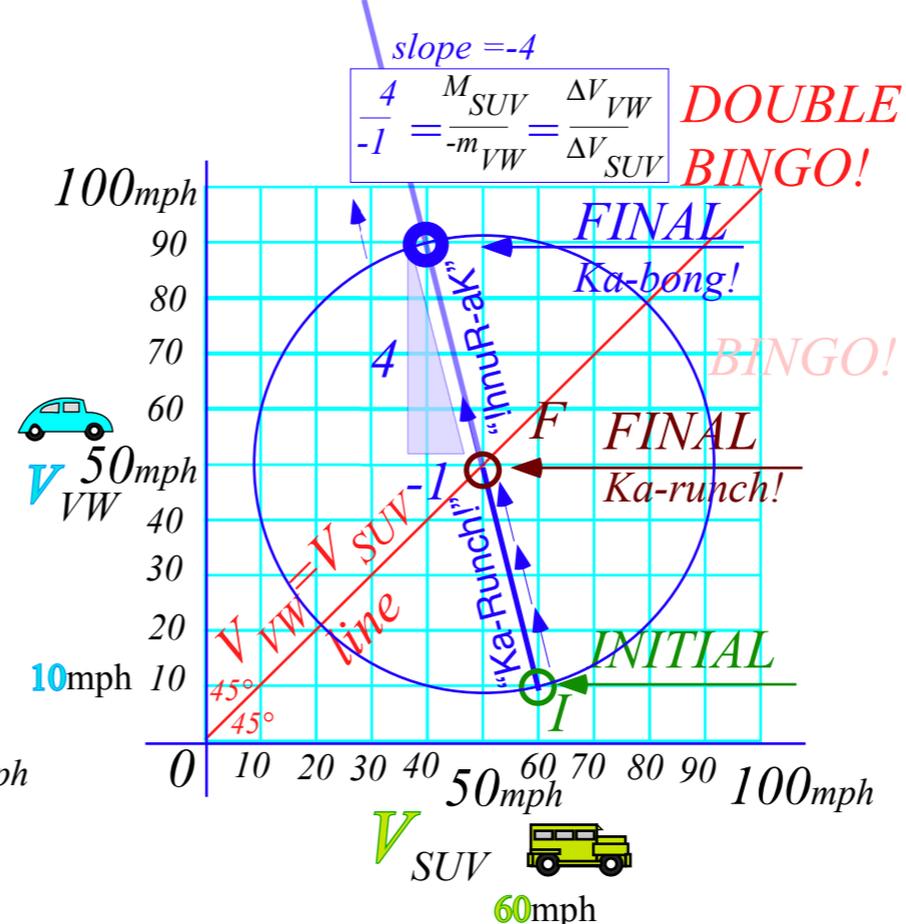
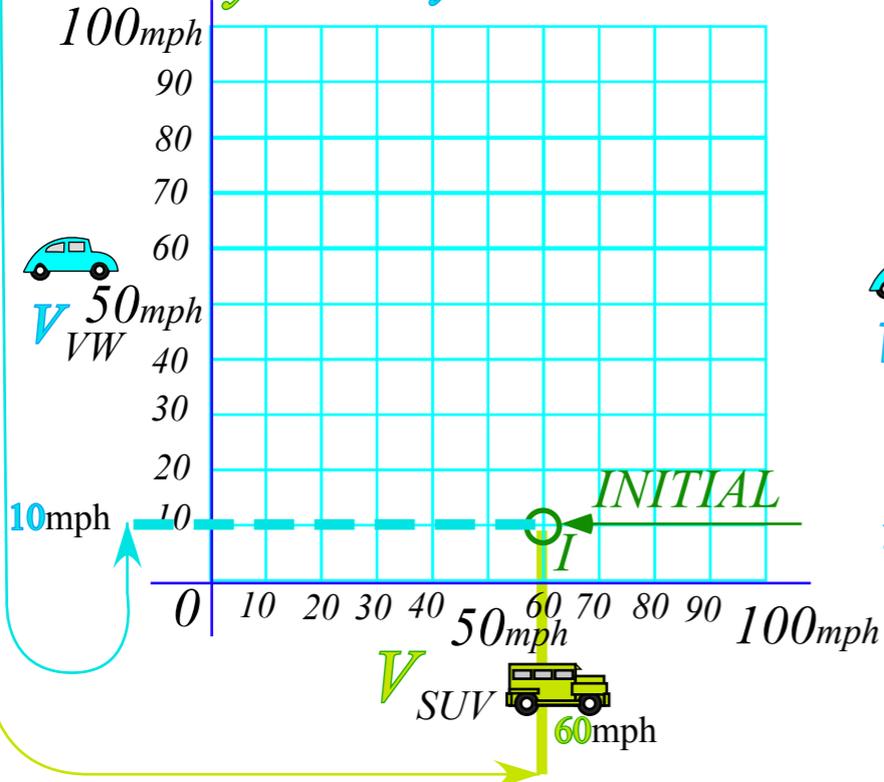
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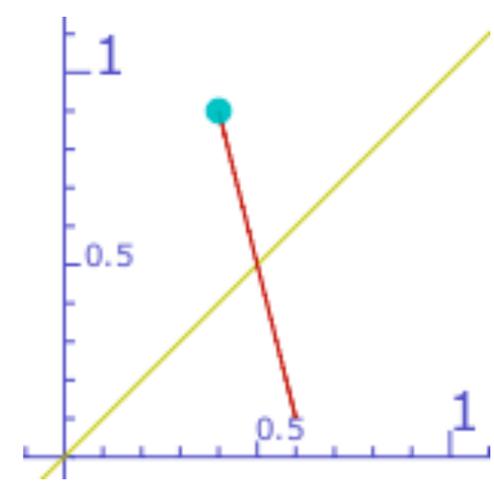
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Velocity-velocity Plot

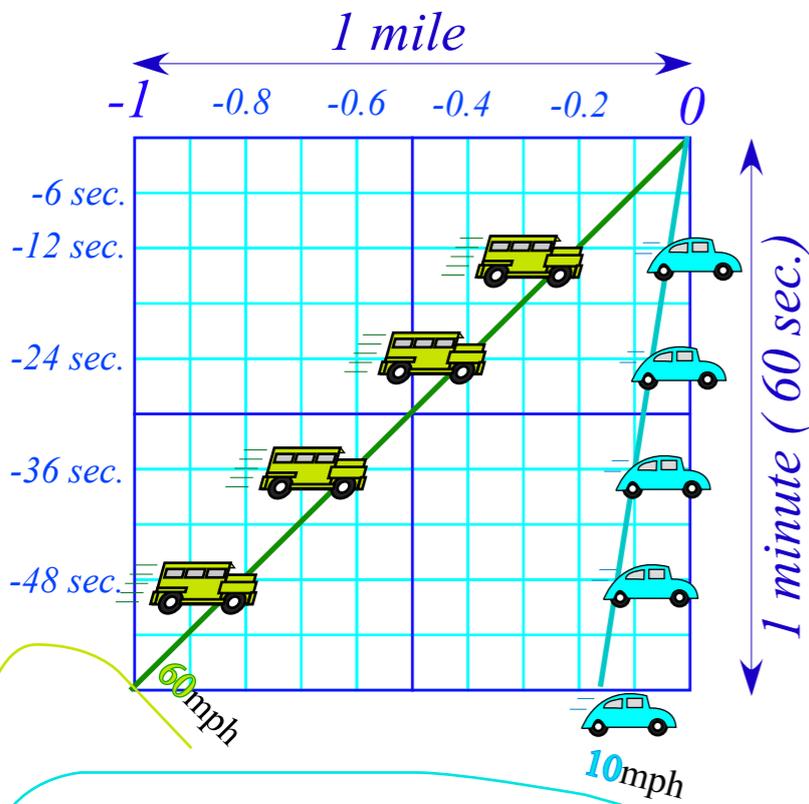


Superball Collision Simulator

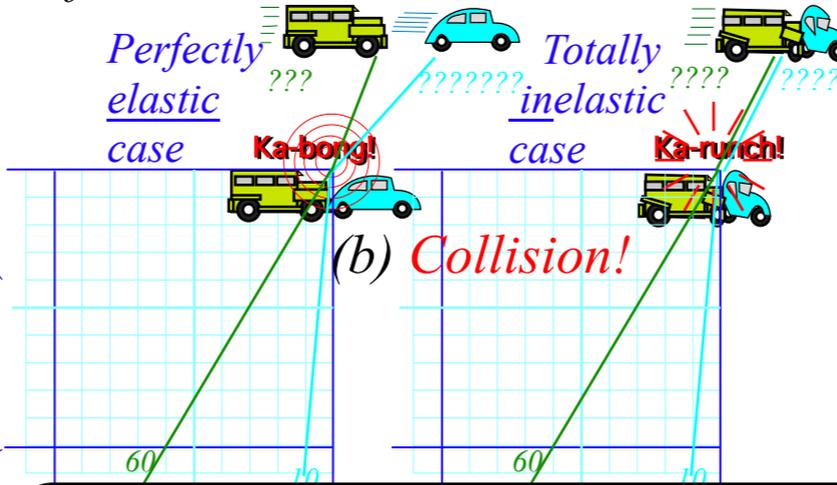


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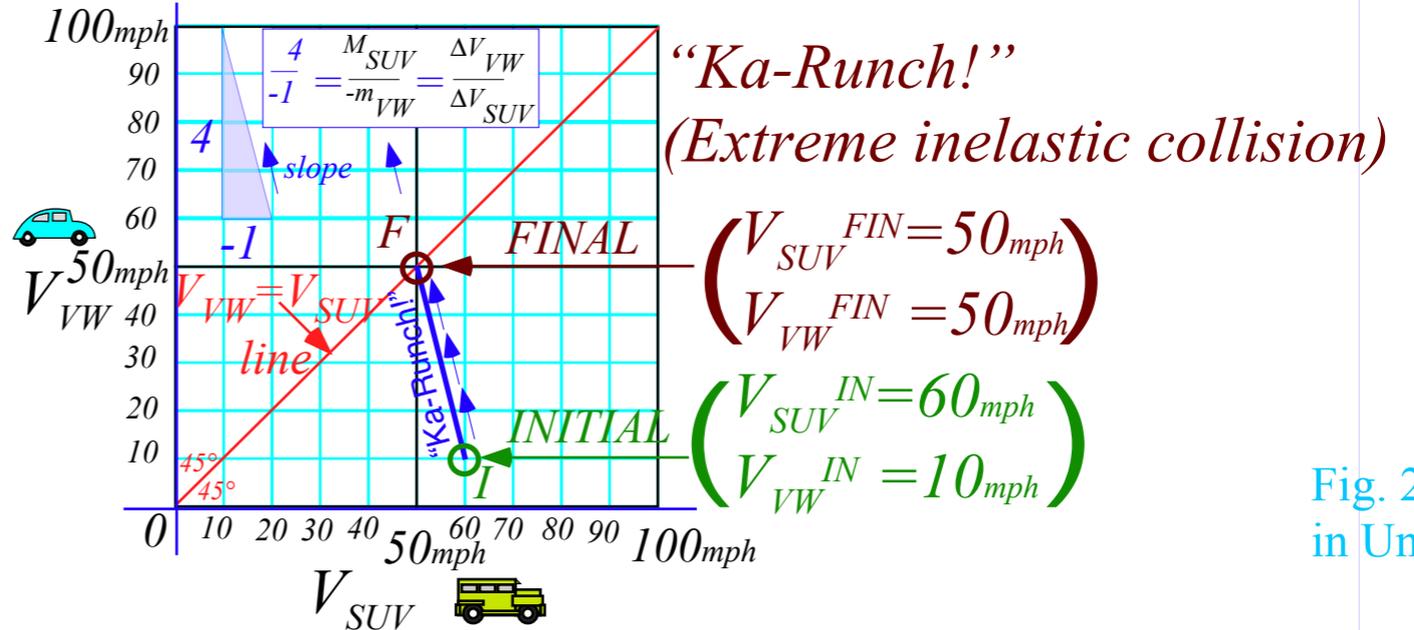
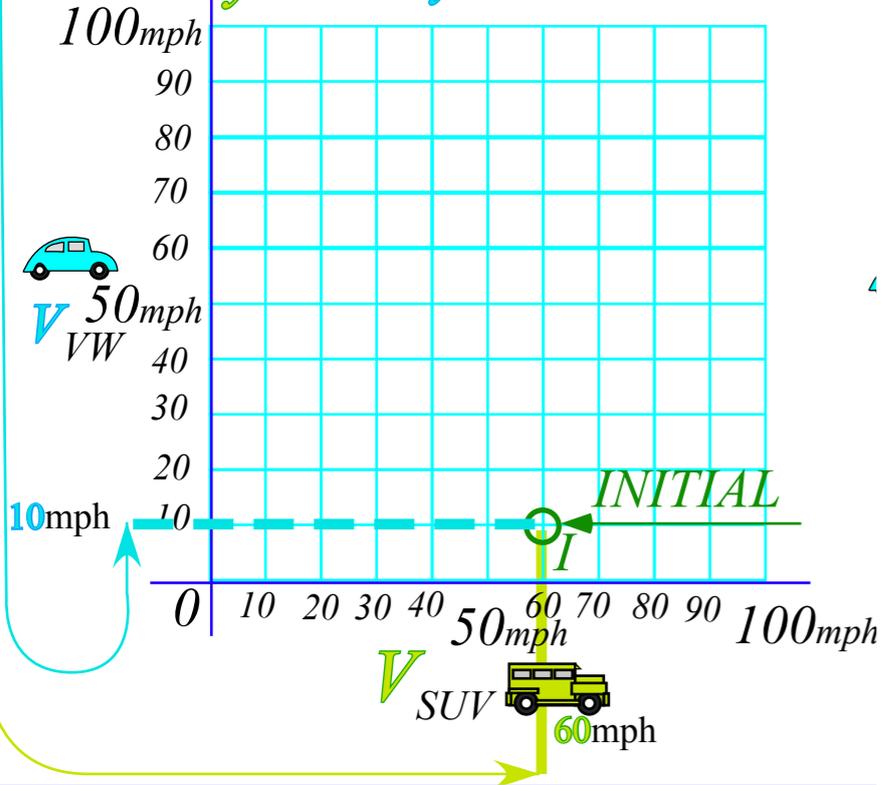
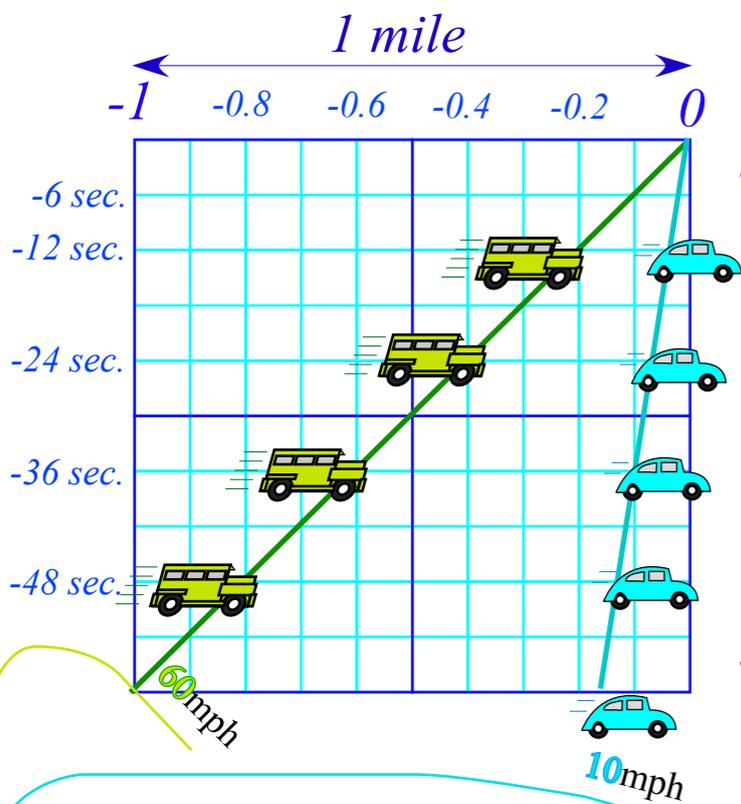


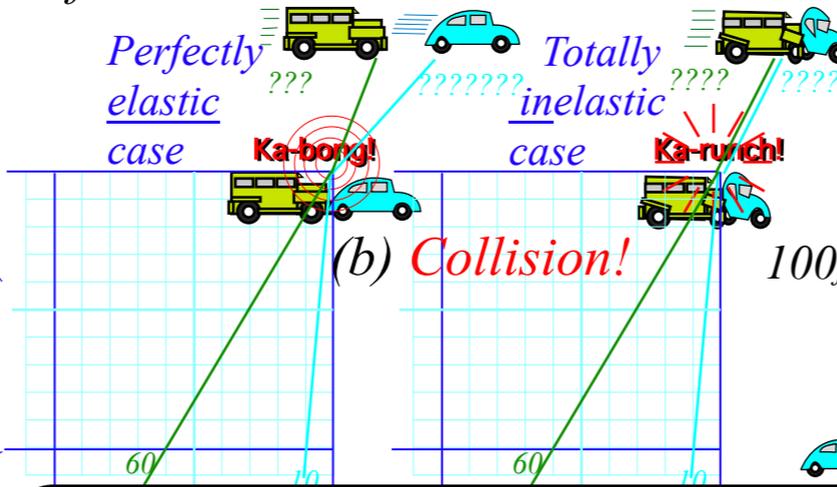
Fig. 2.1 in Unit 1

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After collision...what velocities?



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slope = -4

Notice "Ka-Bong"
Figure 2.2 scaling
(ft./min. is more realistic)

"Ka-Bong!" (Ideal elastic collision)

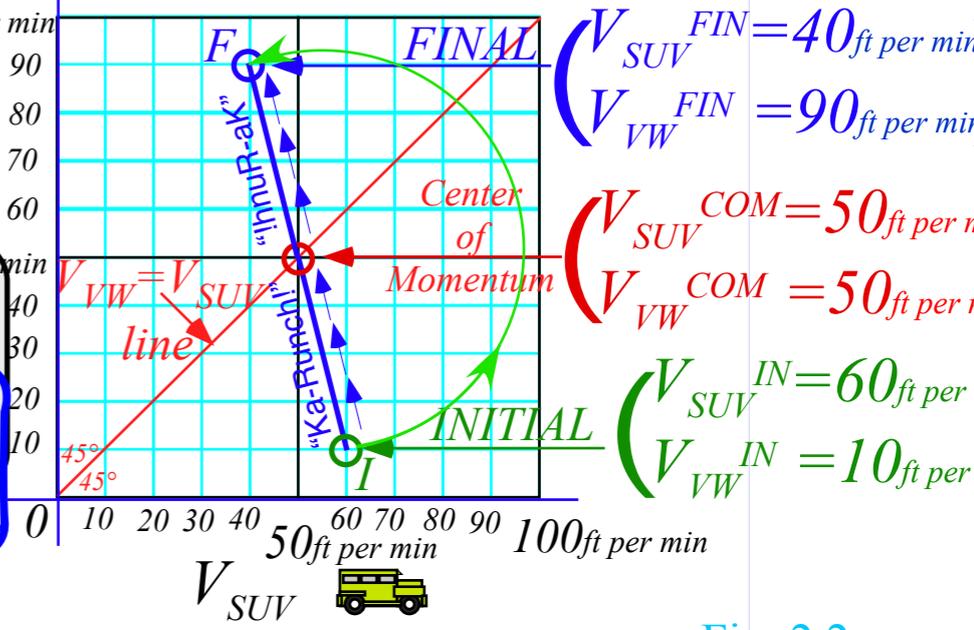
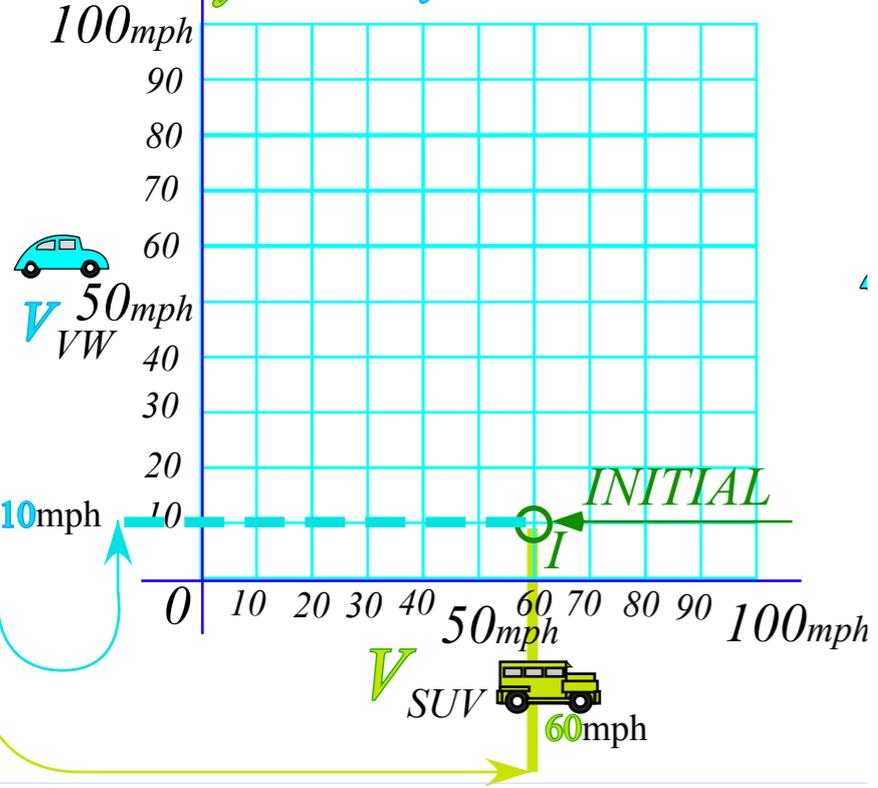


Fig. 2.2 in Unit 1

Velocity-velocity Plot



"Ka-Runch!"
(Extreme inelastic collision)

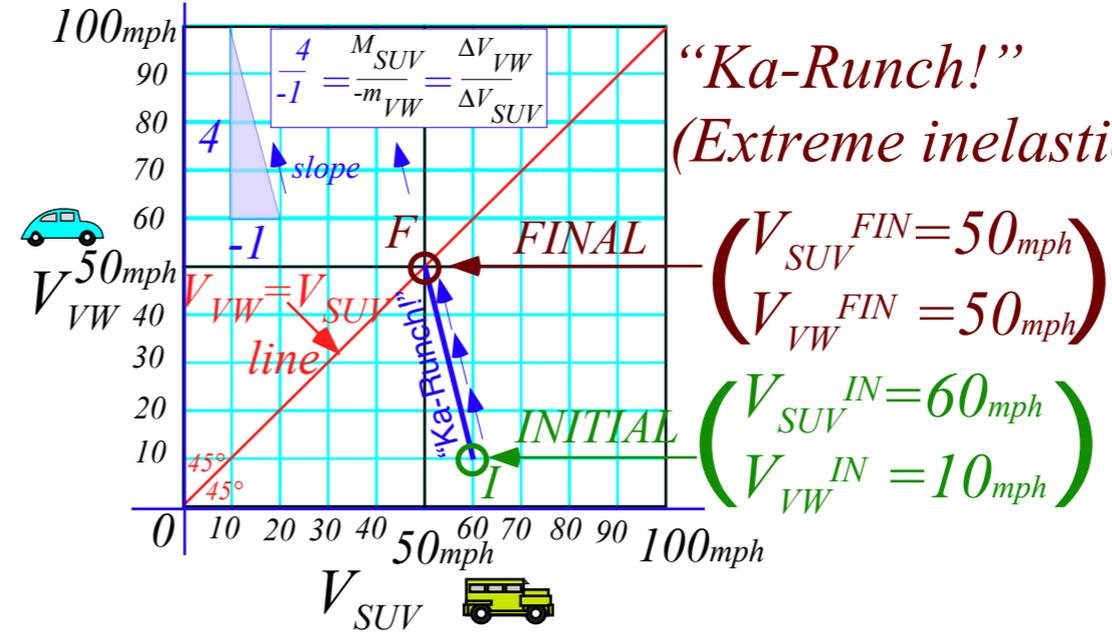


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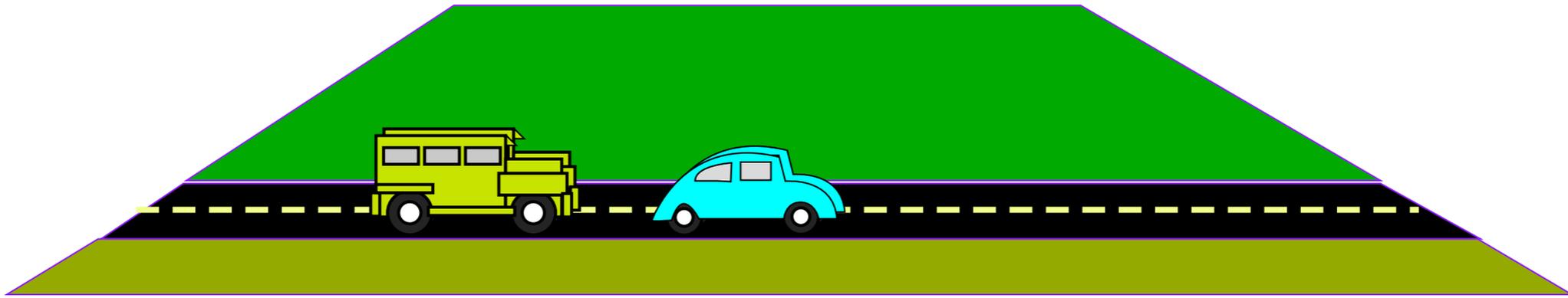
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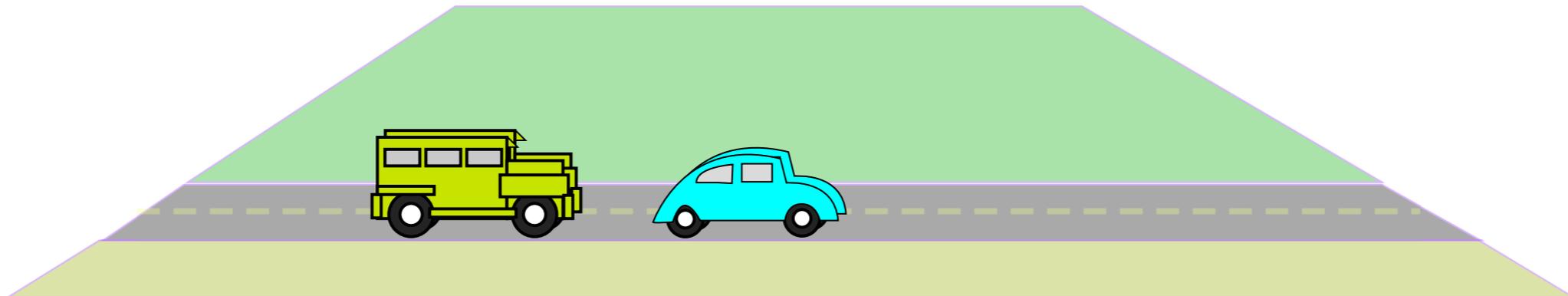
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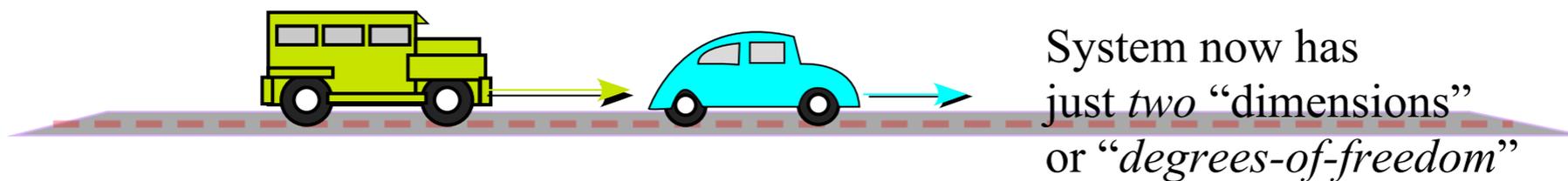
The SUV and VW *Idealized* thought experiments



Idealization 1. Ignore background.
(No rolling friction, air resistance, etc.)



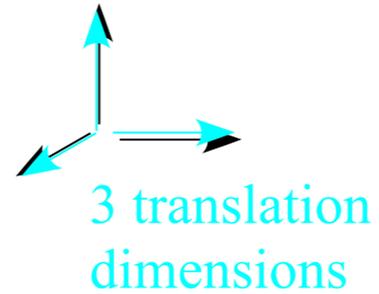
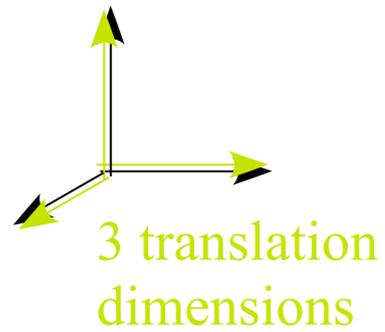
Idealization 2. Make each 1-dimensional.
(Cars “constrained” to ride on frictionless rail)



Landscape 1.1 Idealized model for collision model and thought experiments

Summary of Classical Mechanical Degrees of Freedom

Translation (Each body has 3 translational degrees of freedom) (Introduced in Units 1 and 2)



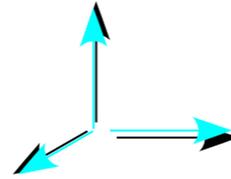
6 translational degrees of freedom for SUV and VW.

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3 translation dimensions



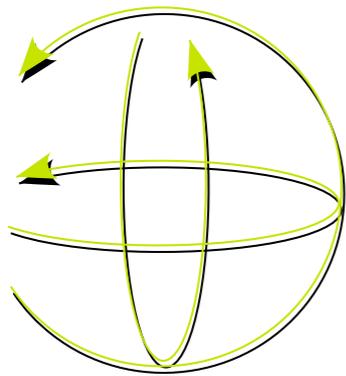
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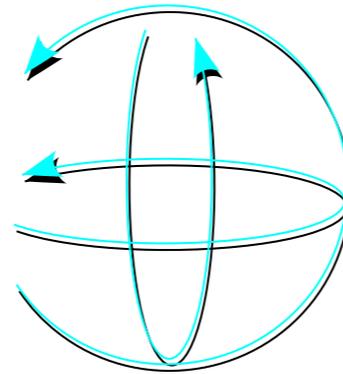
Rotation (Each body has 3 rotational degrees of freedom)

(Introduced in Units 3 and 7)



3 rotational dimensions

yaw-pitch-roll Euler angles



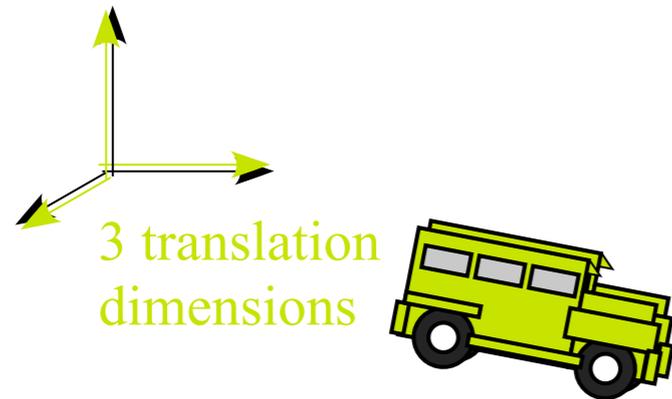
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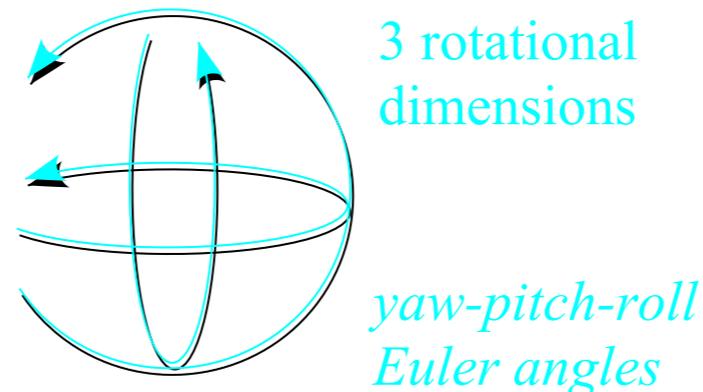
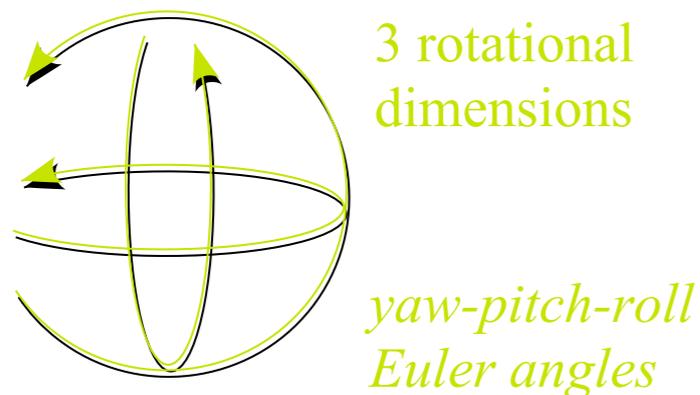
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Rotation (Each body has 3 rotational degrees of freedom) (Introduced in Units 3 and 7)

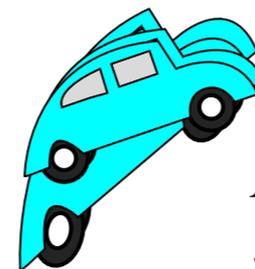
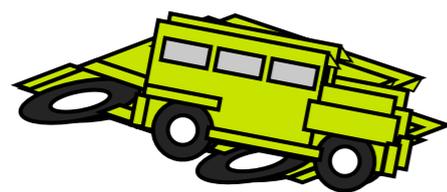


6 rotational degrees of freedom for *SUV* and *VW*.

SUV and VW system involves 12 rigid-body degrees of freedom

Vibration (Each body has many vibrational degrees of freedom) (Introduced in Units 3-8)

Generalized Curvilinear Coordinates (GCC) introduced in Unit 1 Chapters 10-12



An N-atom molecule has $3N-6$ vibrational degrees of freedom

Geometry of Galilean translation symmetry



45° shift in (V_1, V_2) -space

Time reversal symmetry

...of COM collisions

A problem in *space-time* : (60mph Cell-faxing 4ton SUV rear-ends 10mph 1ton VW)

Geometry of Galilean translation (A *symmetry transformation*)

If you increase your velocity by 50 mph,...

(In some direction x, y , or $z...$)

...the rest of the world appears to be 50 mph **slower** (In that direction...)

(a) Galileo transforms to *COM* frame

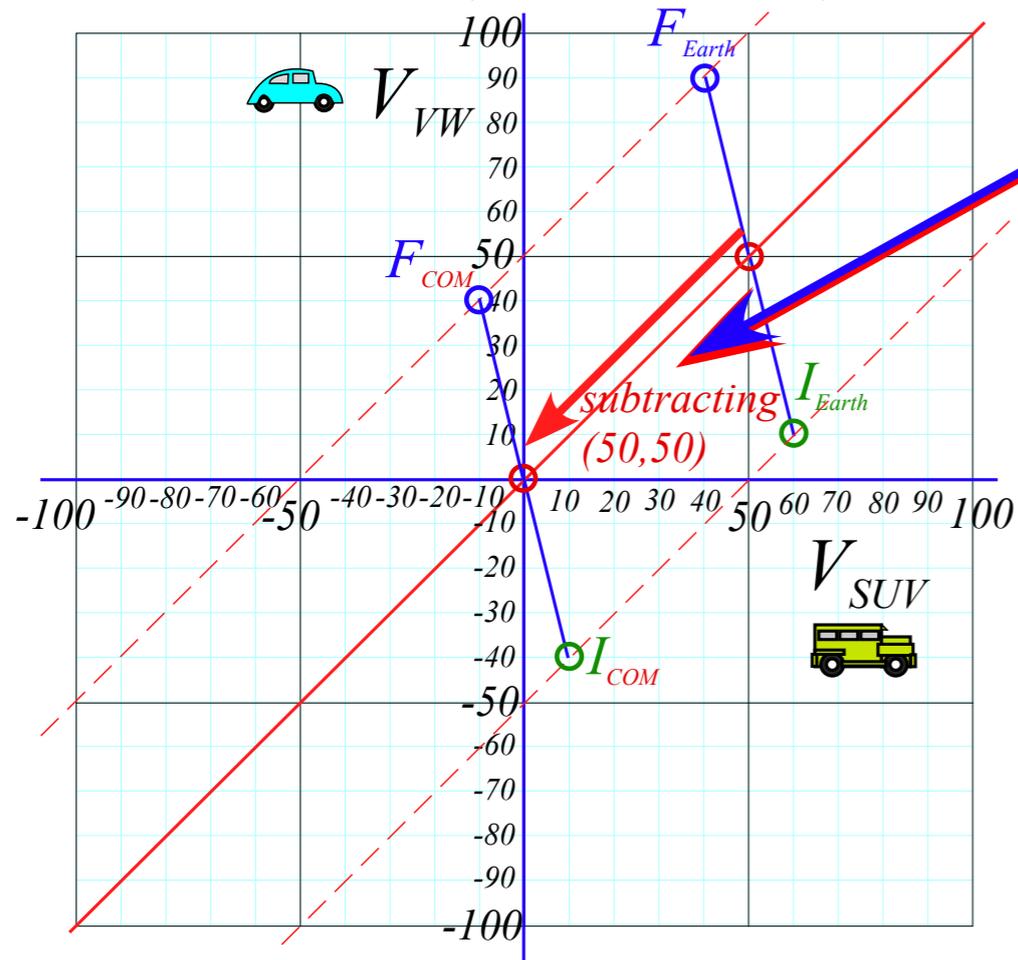


Fig. 2.5a
in Unit 1

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Geometry of Galilean translation (A *symmetry transformation*)

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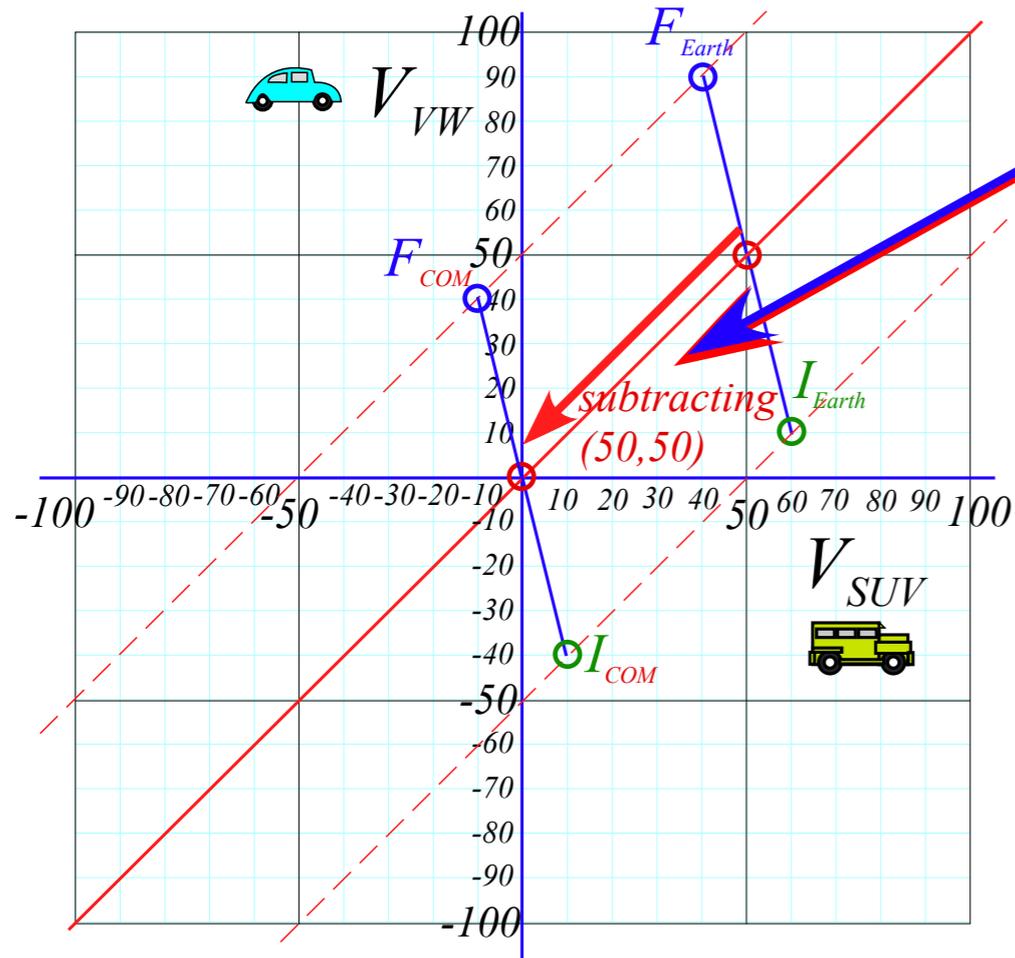


Fig. 2.5a
in Unit 1

(b) ... and to five or six other reference frames

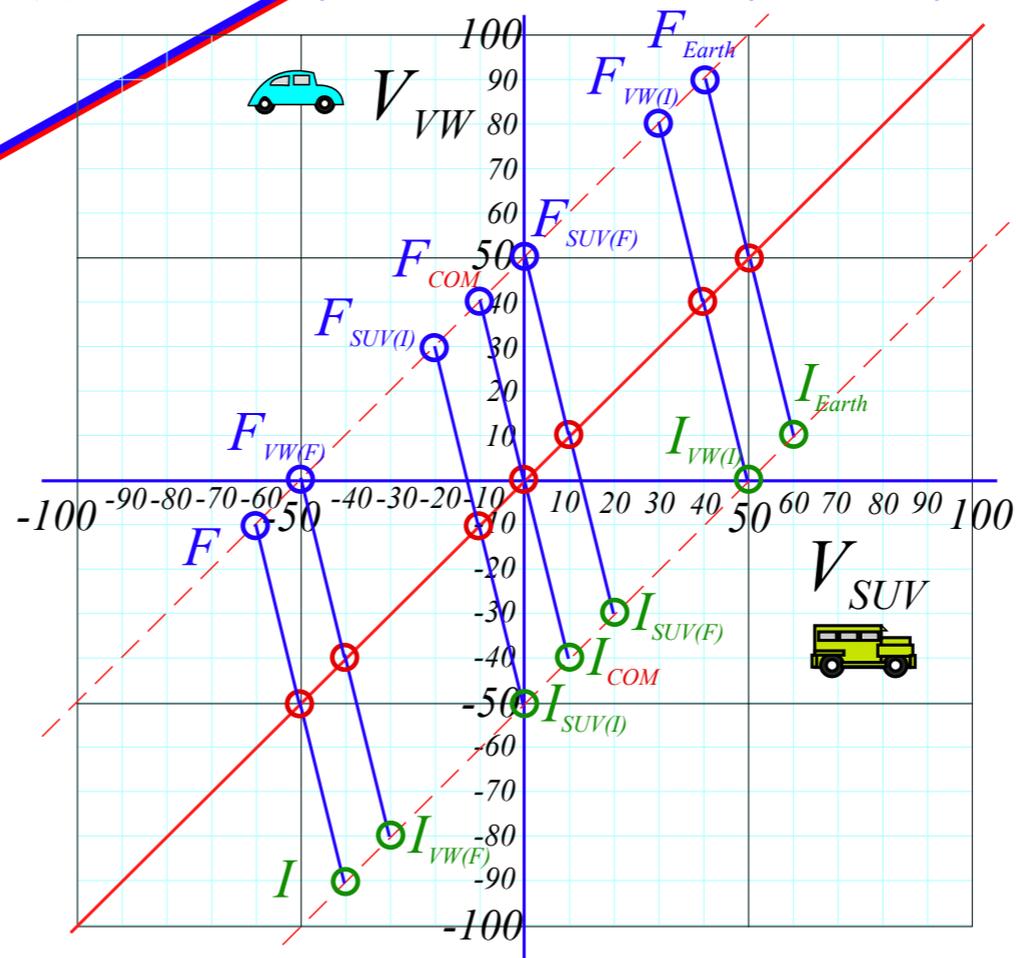


Fig. 2.5b
in Unit 1

Geometry of Galilean translation symmetry

45° shift in (V_1, V_2) -space

Time reversal symmetry

...of COM collisions



A problem in *space-time* : (60mph Cell-faxing 4ton SUV rear-ends 10mph 1ton VW)

Final F and Initial I trade places ...

Geometry of Galilean translation (A symmetry transformation)

If you increase your velocity by 50 mph,...

...the rest of the world appears to be 50 mph slower

Time-reversal (F-I) symmetry pairs (Four examples)

(a) Galileo transforms to COM frame

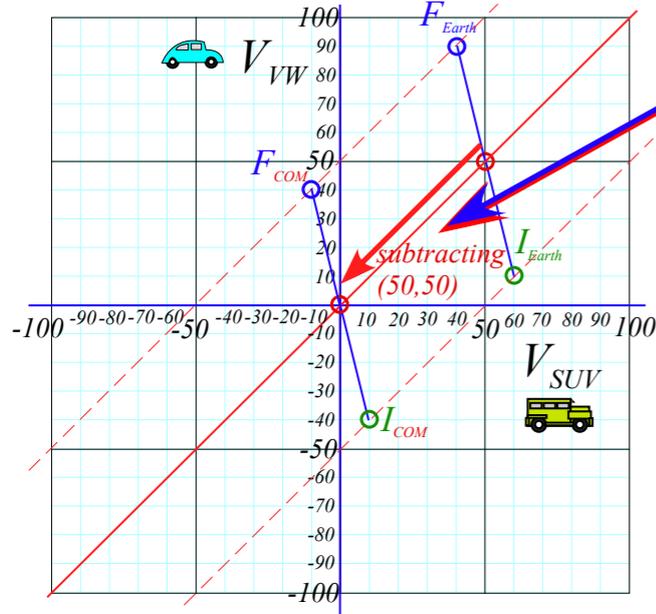


Fig. 2.5a
in Unit 1

(b) ... and to five or six other reference frames

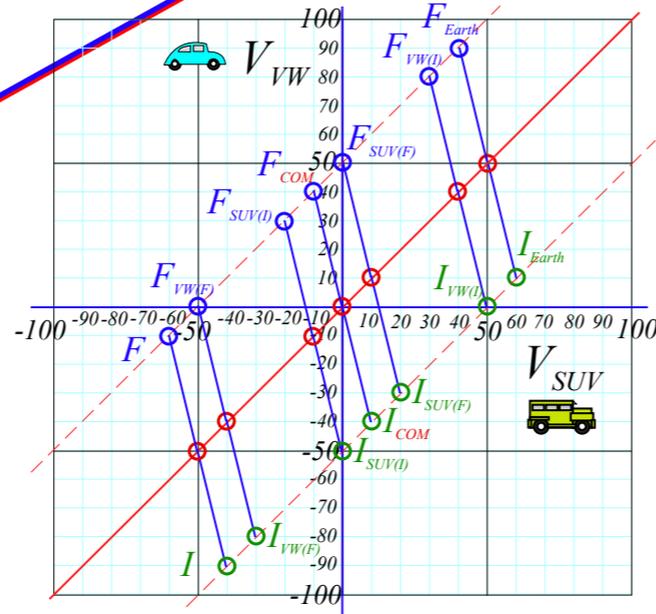
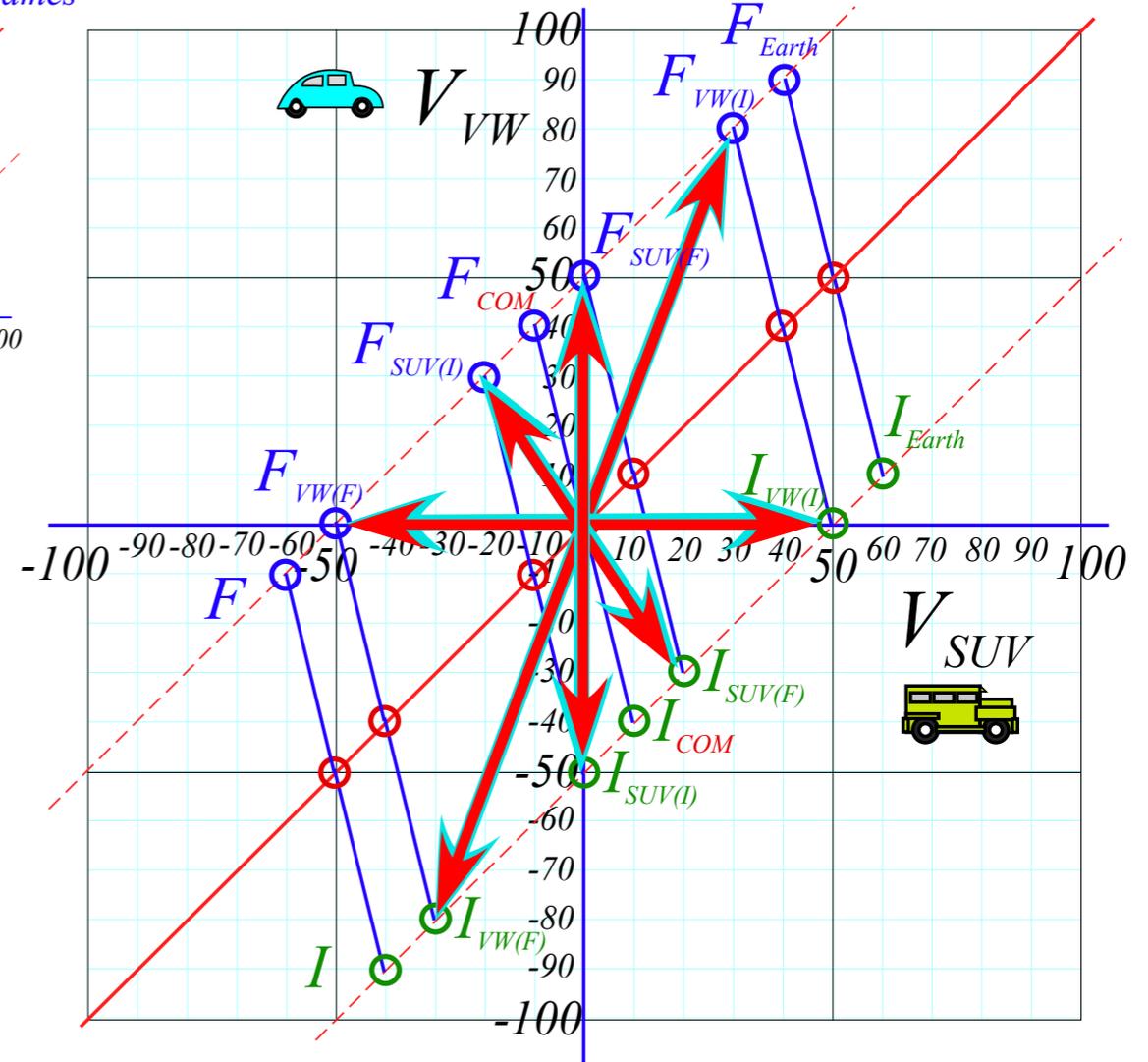


Fig. 2.5b
in Unit 1



Time-reversal means flip t to $-t$... (Run a movie backwards)

A problem in *space-time* : (60mph Cell-faxing 4ton SUV rear-ends 10mph 1ton VW)

Final F and Initial I trade places ...

Geometry of Galilean translation (A symmetry transformation)

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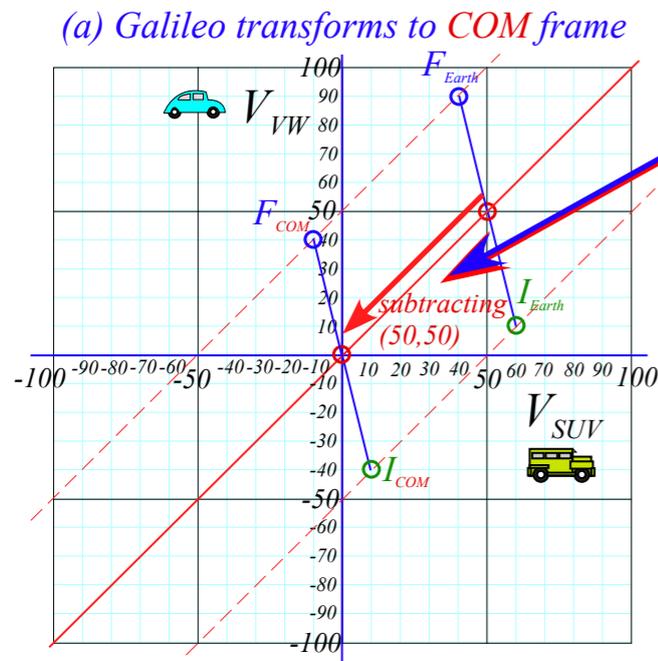


Fig. 2.5a
in Unit 1

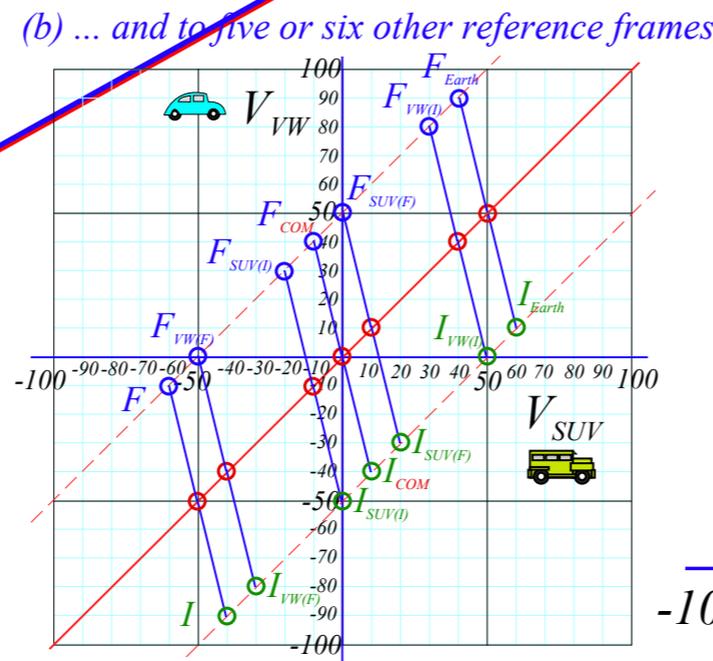
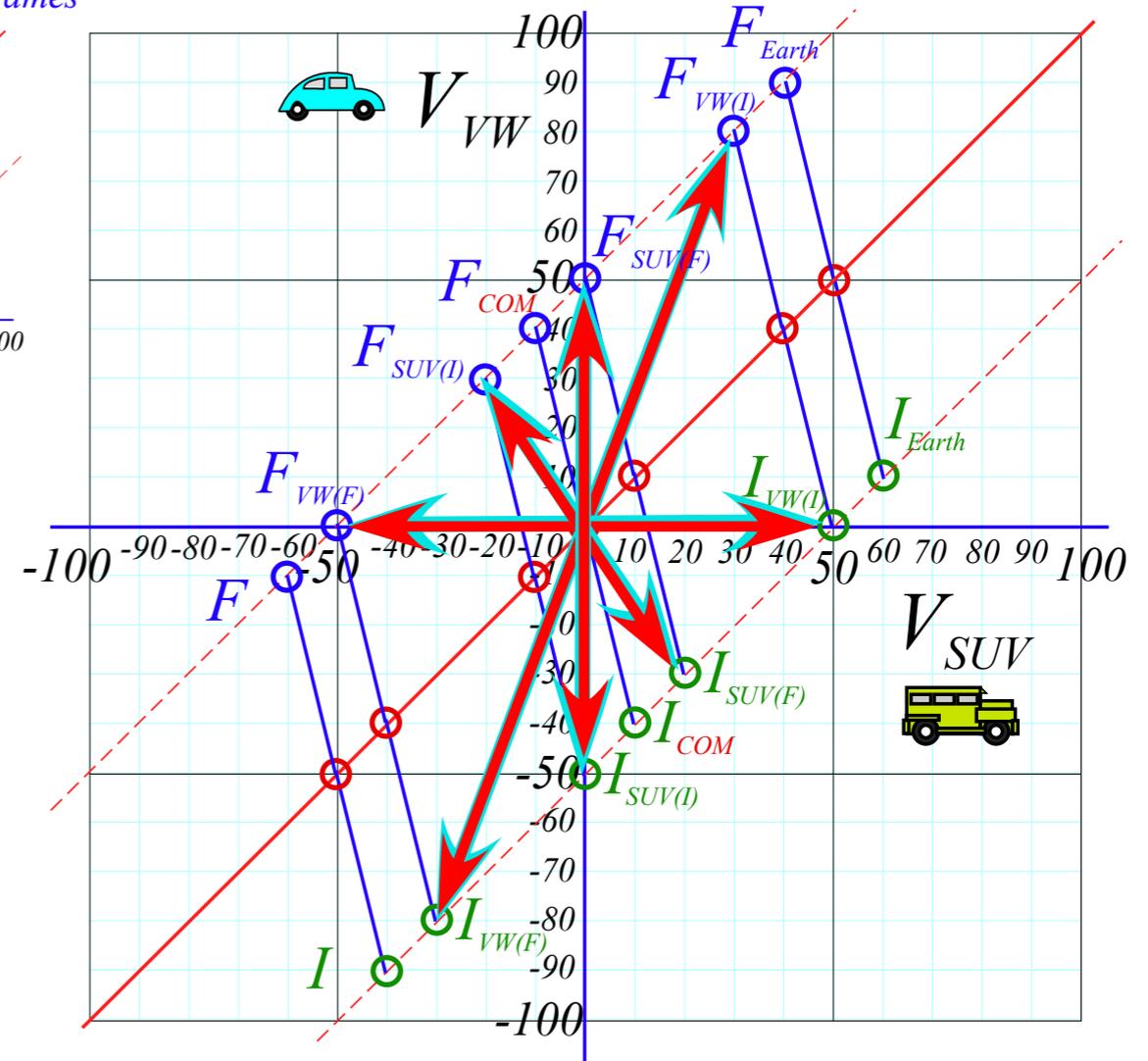


Fig. 2.5b
in Unit 1



*Time-reversal means flip t to $-t$...
(Run a movie backwards)*

*That means you flip Velocity V to $-V$...
(Everything goes backwards)*

Geometry of Galilean translation symmetry

45° shift in (V_1, V_2) -space

Time reversal symmetry

...of COM collisions



A problem in *space-time* : (60mph Cell-faxing 4ton SUV rear-ends 10mph 1ton VW)

Geometry of Galilean translation (A symmetry transformation)

If you increase your velocity by 50 mph,...

...the rest of the world appears to be 50 mph slower

THE
COM Time-reversal
symmetry pair
(Just 1 case)

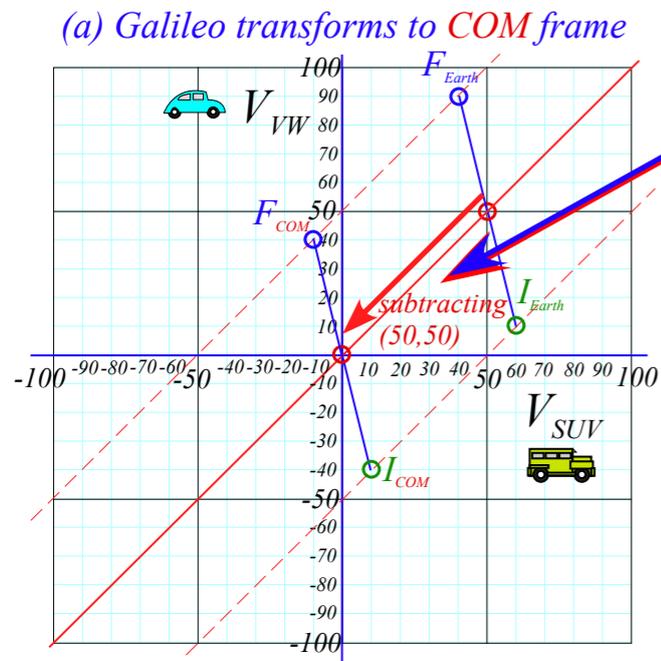


Fig. 2.5a
in Unit 1

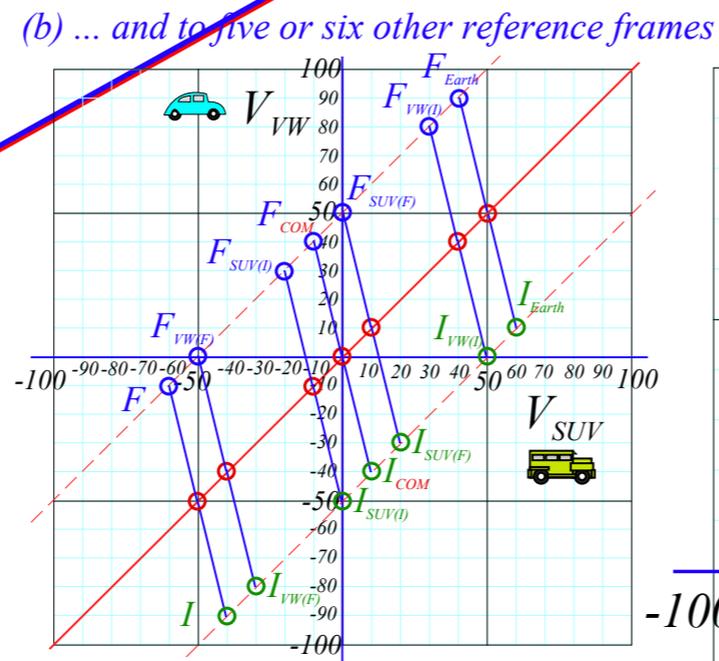
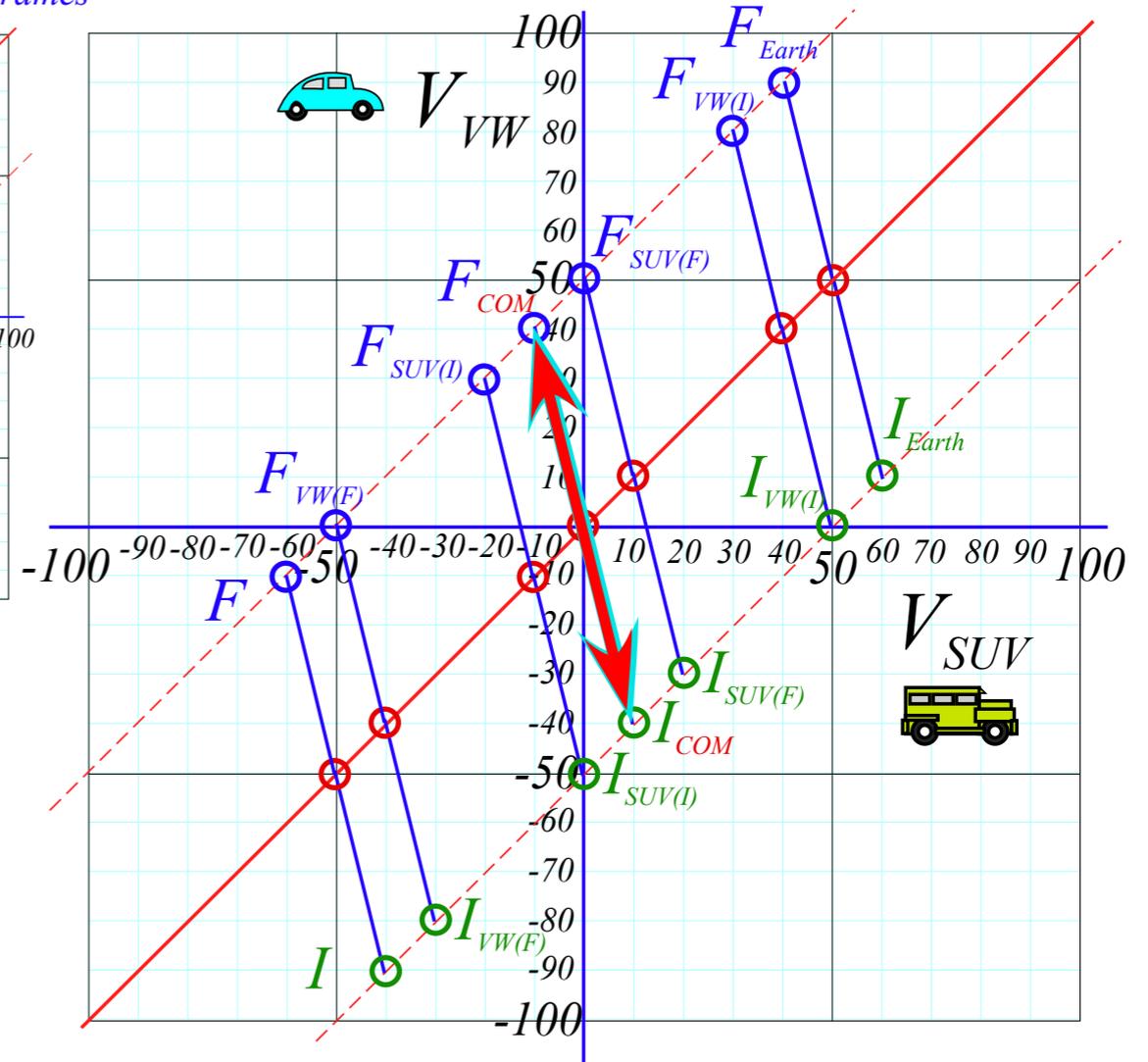


Fig. 2.5b
in Unit 1



*There is just one velocity frame
in which the time-reversed collision
looks just like the original collision*

*That is the
Center-of-Momentum
(COM)-frame*

*Time-reversal means flip t to $-t$...
(Run a movie backwards)*

*That means you flip Velocity V to $-V$...
(Everything goes backwards)*

Algebra, Geometry, and Physics of momentum conservation axiom

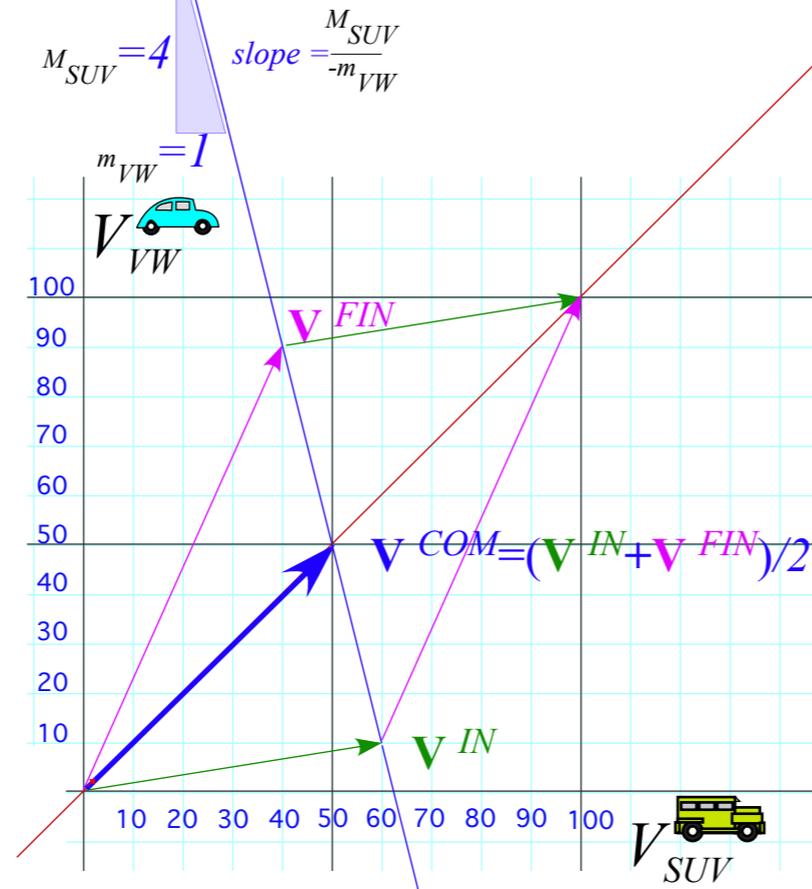
- *Vector algebra of collisions*
- Matrix or tensor algebra of collisions*
- Deriving Energy Conservation Theorem*
- Energy Ellipse geometry*

Algebra, Geometry, and Physics of Momentum Conservation Axiom

Conservation of momentum line: \rightarrow

$$(M_{SUV} + M_{VW})V^{COM} = M_{SUV}V_{SUV}^{IN} + M_{VW}V_{VW}^{IN} = M_{SUV}V_{SUV}^{FIN} + M_{VW}V_{VW}^{FIN}$$

Wow! This is constant!
(Says the axiom)



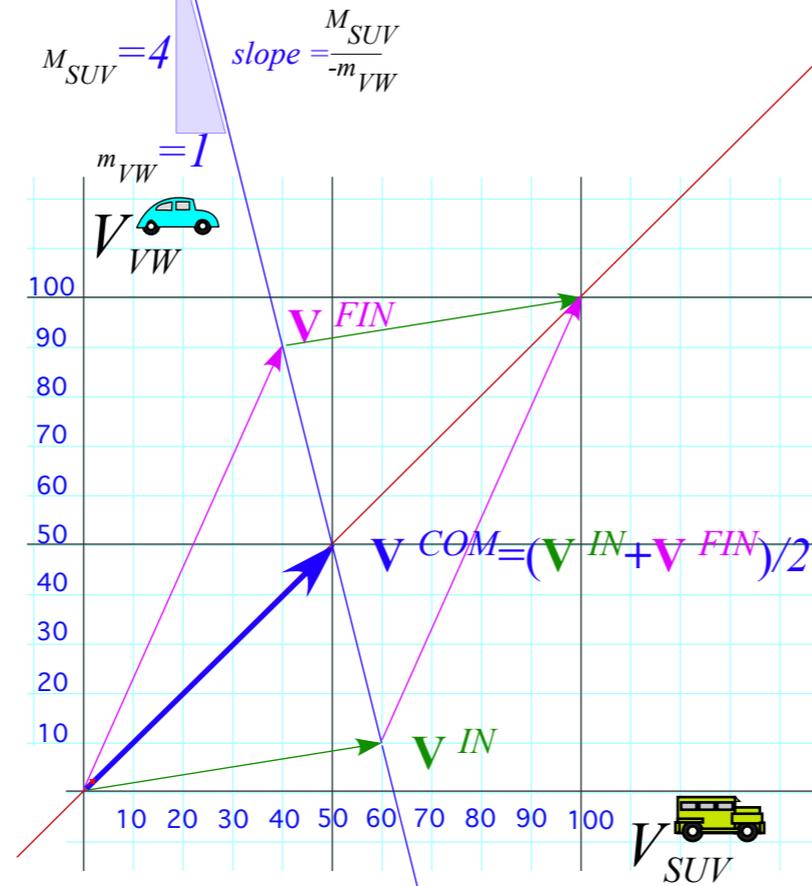
Developing
Conservation-of-Momentum
The key axiom of mechanics

Algebra, Geometry, and Physics of Momentum Conservation Axiom

Conservation of momentum line:

$$(M_{SUV} + M_{VW}) V^{COM} = M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN} = M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}$$

Wow! This is constant!
(Says the axiom)



Developing Conservation-of-Momentum The key axiom of mechanics

Define velocity vector points

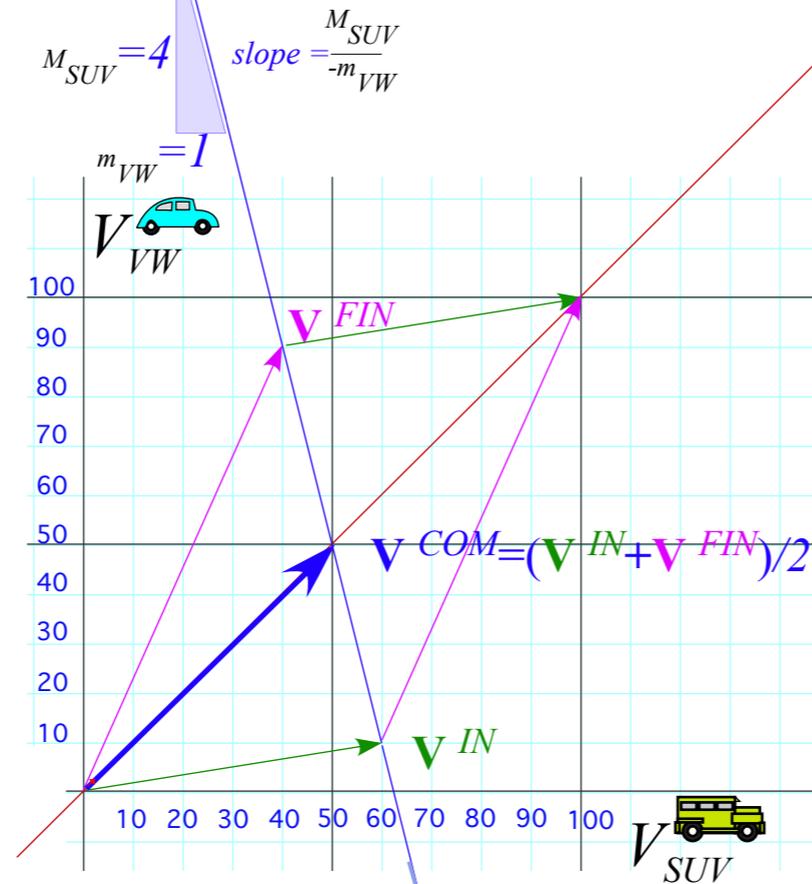
$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix}, \quad \mathbf{V}^{COM} = \begin{pmatrix} V_{SUV}^{COM} \\ V_{VW}^{COM} \end{pmatrix}, \quad \mathbf{V}^{IN} = \begin{pmatrix} V_{SUV}^{IN} \\ V_{VW}^{IN} \end{pmatrix}$$

Algebra, Geometry, and Physics of Momentum Conservation Axiom

Conservation of momentum line:

$$(M_{SUV} + M_{VW}) V^{COM} = M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN} = M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}$$

Wow! This is constant!
(Says the axiom)



Developing Conservation-of-Momentum The key axiom of mechanics

Define velocity vector points

$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix}, \quad \mathbf{V}^{COM} = \begin{pmatrix} V_{SUV}^{COM} \\ V_{VW}^{COM} \end{pmatrix}, \quad \mathbf{V}^{IN} = \begin{pmatrix} V_{SUV}^{IN} \\ V_{VW}^{IN} \end{pmatrix}$$

Points of vectors

\mathbf{V}^{FIN} and \mathbf{V}^{COM} and \mathbf{V}^{IN}

all lie on

momentum - conservation line

Algebra, Geometry, and Physics of Momentum Conservation Axiom

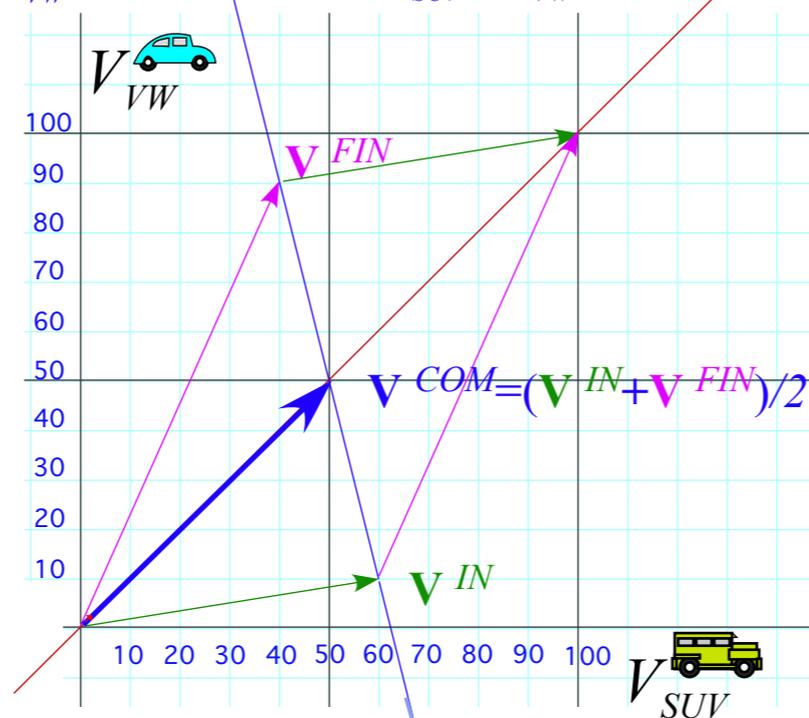
Conservation of momentum line: \rightarrow

$$(M_{SUV} + M_{VW}) V^{COM} = M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN} = M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}$$

Mass weighted average velocity at anytime is Center of Mass velocity V^{COM} :

$$const. = V^{COM} = \frac{M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN}}{(M_{SUV} + M_{VW})} = \frac{M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}}{(M_{SUV} + M_{VW})}$$

Wow! This is constant!
(Says the axiom)



Developing Conservation-of-Momentum The key axiom of mechanics

Define velocity vector points

$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix}, \quad \mathbf{V}^{COM} = \begin{pmatrix} V_{SUV}^{COM} \\ V_{VW}^{COM} \end{pmatrix}, \quad \mathbf{V}^{IN} = \begin{pmatrix} V_{SUV}^{IN} \\ V_{VW}^{IN} \end{pmatrix}$$

Points of vectors

\mathbf{V}^{FIN} and \mathbf{V}^{COM} and \mathbf{V}^{IN}

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Algebra, Geometry, and Physics of Momentum Conservation Axiom

Conservation of momentum line: \rightarrow

$$(M_{SUV} + M_{VW}) V^{COM} = M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN} = M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}$$

Mass weighted average velocity at anytime is Center of Mass velocity V^{COM} :

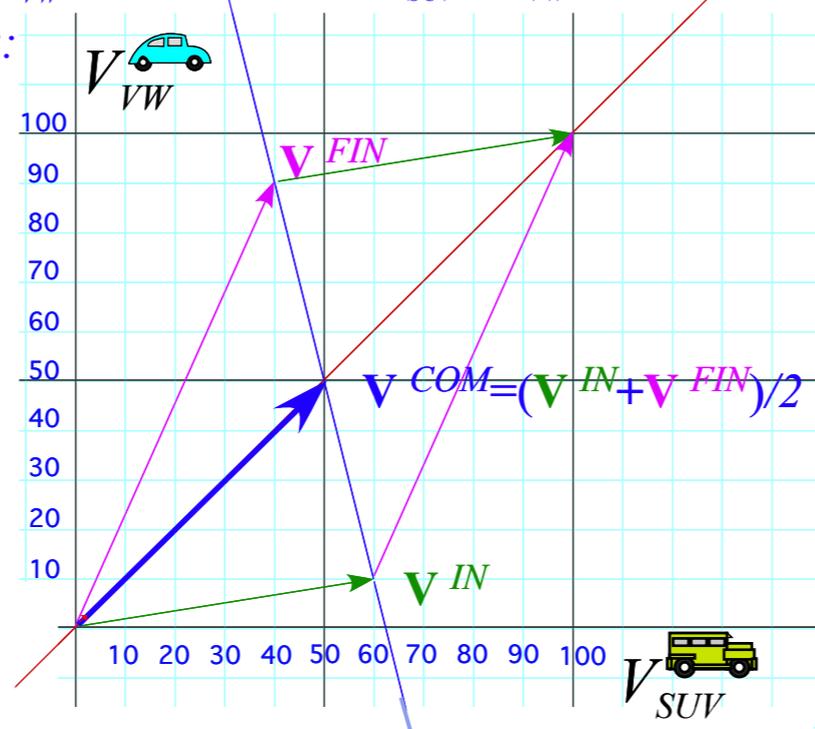
$$const. = V^{COM} = \frac{M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN}}{(M_{SUV} + M_{VW})} = \frac{M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}}{(M_{SUV} + M_{VW})}$$

Express this using velocity vectors:

$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix} = \begin{pmatrix} 40 \\ 90 \end{pmatrix}$$

$$\mathbf{V}^{IN} = \begin{pmatrix} V_{SUV}^{IN} \\ V_{VW}^{IN} \end{pmatrix} = \begin{pmatrix} 60 \\ 10 \end{pmatrix}$$

$$\mathbf{V}^{COM} = \begin{pmatrix} V^{COM} \\ V^{COM} \end{pmatrix} = V^{COM} \begin{pmatrix} 1 \\ 1 \end{pmatrix}$$



Developing Conservation-of-Momentum The key axiom of mechanics

Define velocity vector points

$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix}, \quad \mathbf{V}^{COM} = \begin{pmatrix} V_{SUV}^{COM} \\ V_{VW}^{COM} \end{pmatrix}, \quad \mathbf{V}^{IN} = \begin{pmatrix} V_{SUV}^{IN} \\ V_{VW}^{IN} \end{pmatrix}$$

Points of vectors

\mathbf{V}^{FIN} and \mathbf{V}^{COM} and \mathbf{V}^{IN}

all lie on

momentum - conservation line

Algebra, Geometry, and Physics of Momentum Conservation Axiom

Conservation of momentum line: \rightarrow

$$(M_{SUV} + M_{VW}) V^{COM} = M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN} = M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}$$

Mass weighted average velocity at anytime is Center of Mass velocity V^{COM} :

$$const. = V^{COM} = \frac{M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN}}{(M_{SUV} + M_{VW})} = \frac{M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}}{(M_{SUV} + M_{VW})}$$

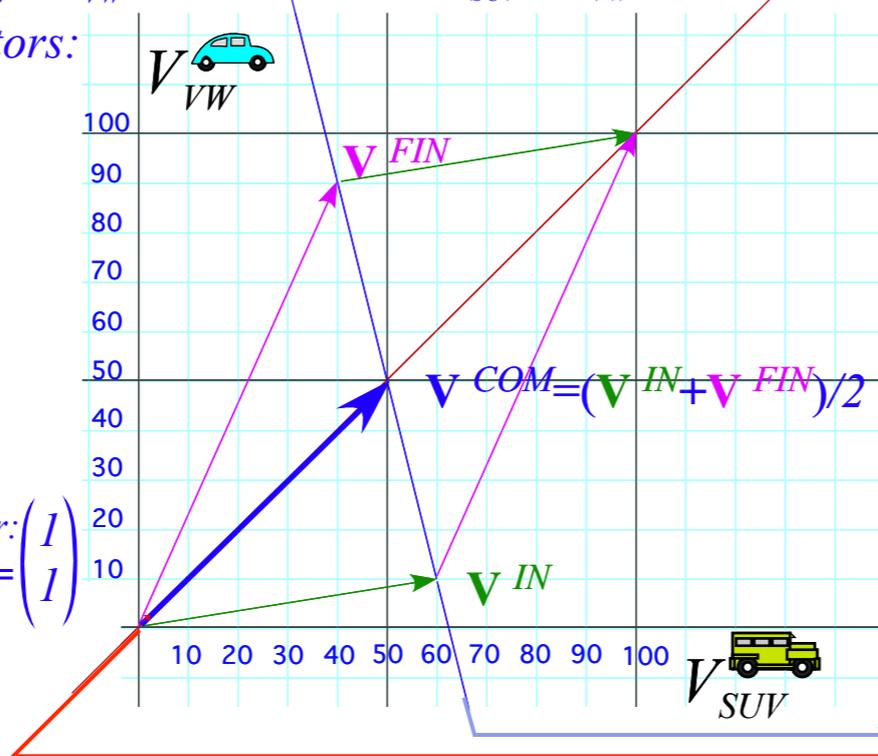
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$$\mathbf{V}^{COM} = \begin{pmatrix} V^{COM} \\ V^{COM} \end{pmatrix} = V^{COM} \begin{pmatrix} 1 \\ 1 \end{pmatrix}$$

$$= V^{COM} \mathbf{u} \quad \text{Define funny-unit vector: } \mathbf{u} = \begin{pmatrix} 1 \\ 1 \end{pmatrix}$$



Developing Conservation-of-Momentum The key axiom of mechanics

Define velocity vector points

$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix}, \quad \mathbf{V}^{COM} = \begin{pmatrix} V_{SUV}^{COM} \\ V_{VW}^{COM} \end{pmatrix}, \quad \mathbf{V}^{IN} = \begin{pmatrix} V_{SUV}^{IN} \\ V_{VW}^{IN} \end{pmatrix}$$

Points of vectors

\mathbf{V}^{FIN} and \mathbf{V}^{COM} and \mathbf{V}^{IN}
all lie on

momentum - conservation line

Vector \mathbf{V}^{COM} is along *45° line*

Define funny-unit vector : $\mathbf{u} = \begin{pmatrix} 1 \\ 1 \end{pmatrix}$

Algebra, Geometry, and Physics of momentum conservation axiom

Vector algebra of collisions

 *Matrix or tensor algebra of collisions*

Deriving Energy Conservation Theorem

Energy Ellipse geometry

Algebra, Geometry, and Physics of Momentum Conservation Axiom

Conservation of momentum line: \rightarrow

$$(M_{SUV} + M_{VW}) V^{COM} = M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN} = M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}$$

Mass weighted average velocity at anytime is Center of Mass velocity V^{COM} :

$$const. = V^{COM} = \frac{M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN}}{(M_{SUV} + M_{VW})} = \frac{M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}}{(M_{SUV} + M_{VW})}$$

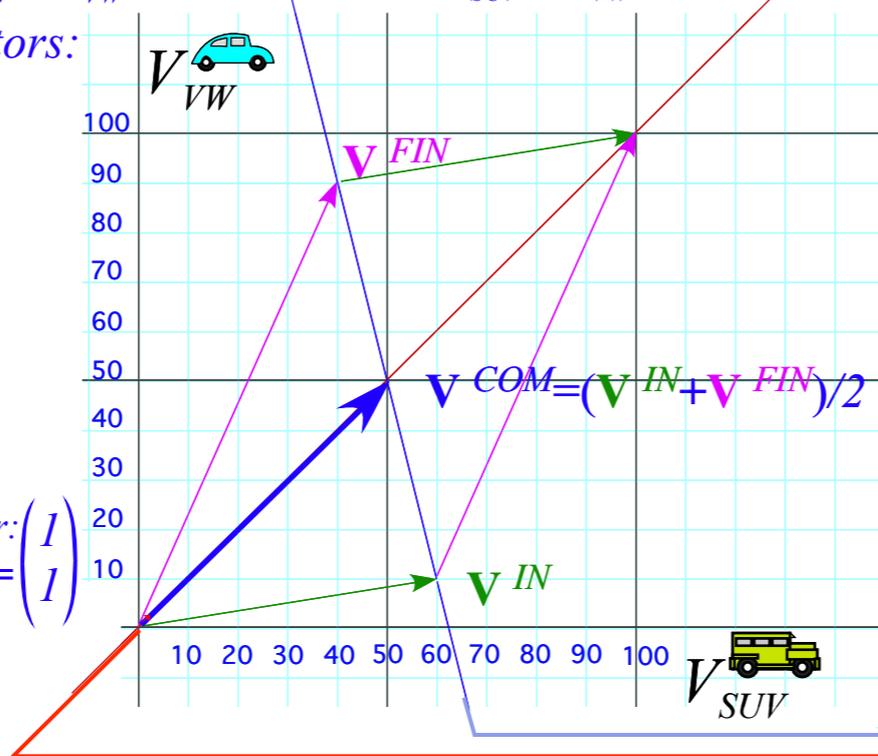
Express this using velocity vectors:

$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix} = \begin{pmatrix} 40 \\ 90 \end{pmatrix}$$

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Developing Conservation-of-Momentum The key axiom of mechanics

Define velocity vector points

$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix}, \quad \mathbf{V}^{COM} = \begin{pmatrix} V_{SUV}^{COM} \\ V_{VW}^{COM} \end{pmatrix}, \quad \mathbf{V}^{IN} = \begin{pmatrix} V_{SUV}^{IN} \\ V_{VW}^{IN} \end{pmatrix}$$

Points of vectors

\mathbf{V}^{FIN} and \mathbf{V}^{COM} and \mathbf{V}^{IN}
all lie on

momentum - conservation line

Vector \mathbf{V}^{COM} is along *45° line*

Define funny-unit vector : $\mathbf{u} = \begin{pmatrix} 1 \\ 1 \end{pmatrix}$

Algebra, Geometry, and Physics of Momentum Conservation Axiom

Conservation of momentum line: \rightarrow

$$(M_{SUV} + M_{VW}) V^{COM} = M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN} = M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}$$

Mass weighted average velocity at anytime is Center of Mass velocity V^{COM} :

$$const. = V^{COM} = \frac{M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN}}{(M_{SUV} + M_{VW})} = \frac{M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}}{(M_{SUV} + M_{VW})}$$

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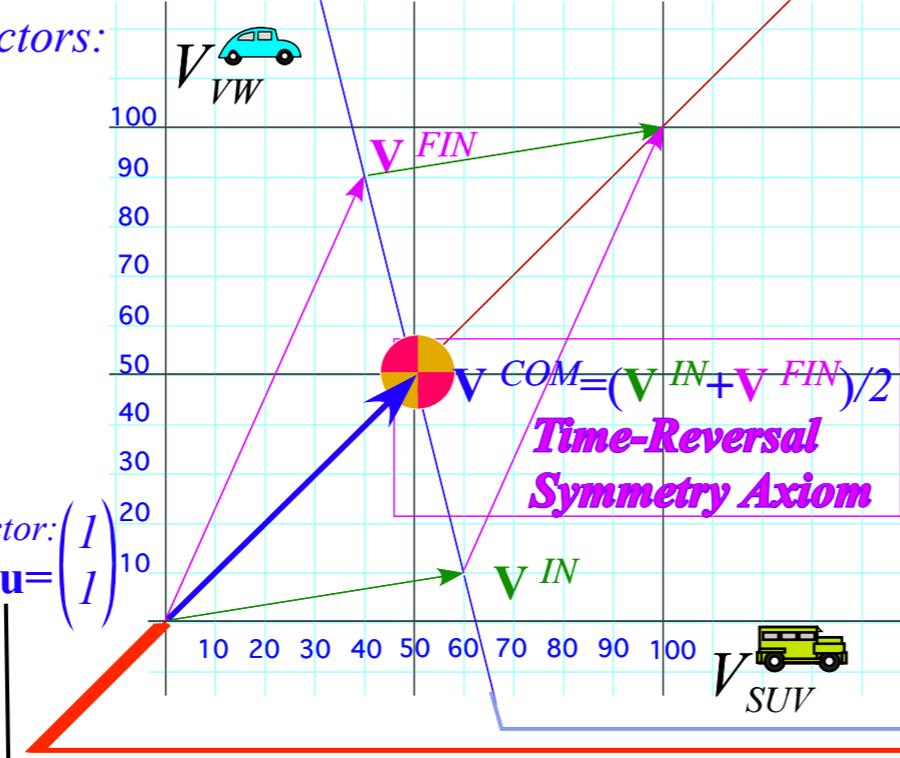
...and matrix operators:

$$\mathbf{M} = \begin{pmatrix} M_{SUV} & 0 \\ 0 & M_{VW} \end{pmatrix}$$

...that give momentum vector:

$$\mathbf{P} = \mathbf{M} \cdot \mathbf{V} = \begin{pmatrix} M_{SUV} & 0 \\ 0 & M_{VW} \end{pmatrix} \begin{pmatrix} V_{SUV} \\ V_{VW} \end{pmatrix} = \begin{pmatrix} P_{SUV} \\ P_{VW} \end{pmatrix} = \begin{pmatrix} M_{SUV} V_{SUV} \\ M_{VW} V_{VW} \end{pmatrix}$$

Define funny-unit vector: $\mathbf{u} = \begin{pmatrix} 1 \\ 1 \end{pmatrix}$



Developing Conservation-of-Momentum The key axiom of mechanics

Define velocity vector points

$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix}, \quad \mathbf{V}^{COM} = \begin{pmatrix} V_{SUV}^{COM} \\ V_{VW}^{COM} \end{pmatrix}, \quad \mathbf{V}^{IN} = \begin{pmatrix} V_{SUV}^{IN} \\ V_{VW}^{IN} \end{pmatrix}$$

Points of vectors

\mathbf{V}^{FIN} and \mathbf{V}^{COM} and \mathbf{V}^{IN}

all lie on

momentum - conservation line

Vector \mathbf{V}^{COM} is along *45° line*

Algebra, Geometry, and Physics of Momentum Conservation Axiom

Conservation of momentum line: \rightarrow

$$(M_{SUV} + M_{VW}) V^{COM} = M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN} = M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}$$

Mass weighted average velocity at anytime is Center of Mass velocity V^{COM} :

$$const. = V^{COM} = \frac{M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN}}{(M_{SUV} + M_{VW})} = \frac{M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}}{(M_{SUV} + M_{VW})}$$

Express this using velocity vectors:

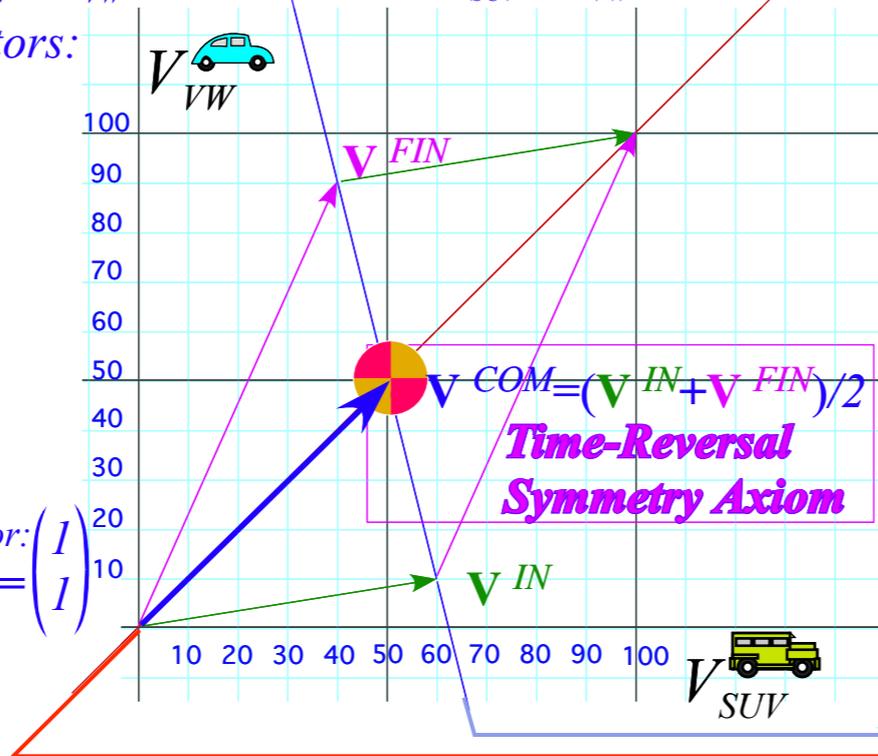
$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix} = \begin{pmatrix} 40 \\ 90 \end{pmatrix}$$

$$\mathbf{V}^{IN} = \begin{pmatrix} V_{SUV}^{IN} \\ V_{VW}^{IN} \end{pmatrix} = \begin{pmatrix} 60 \\ 10 \end{pmatrix}$$

$$\mathbf{V}^{COM} = \begin{pmatrix} V^{COM} \\ V^{COM} \end{pmatrix} = V^{COM} \begin{pmatrix} 1 \\ 1 \end{pmatrix}$$

$= V^{COM} \mathbf{u}$ Define funny-unit vector: $\mathbf{u} = \begin{pmatrix} 1 \\ 1 \end{pmatrix}$
 ...and matrix operators:

$$\mathbf{M} = \begin{pmatrix} M_{SUV} & 0 \\ 0 & M_{VW} \end{pmatrix}$$



...that give momentum vector: $\mathbf{P} = \mathbf{M} \cdot \mathbf{V} = \begin{pmatrix} M_{SUV} & 0 \\ 0 & M_{VW} \end{pmatrix} \begin{pmatrix} V_{SUV} \\ V_{VW} \end{pmatrix} = \begin{pmatrix} P_{SUV} \\ P_{VW} \end{pmatrix} = \begin{pmatrix} M_{SUV} V_{SUV} \\ M_{VW} V_{VW} \end{pmatrix}$
 whose sum of components is constant.

$$const. = \mathbf{u} \cdot \mathbf{P} = P_{SUV} + P_{VW} = M_{SUV} V_{SUV} + M_{VW} V_{VW} = \mathbf{u} \cdot \mathbf{M} \cdot \mathbf{V} = \mathbf{u} \cdot \mathbf{M} \cdot \mathbf{V}^{IN} = \mathbf{u} \cdot \mathbf{M} \cdot \mathbf{V}^{FIN}$$

Define funny-unit vector: $\mathbf{u} = \begin{pmatrix} 1 \\ 1 \end{pmatrix}$

Developing Conservation-of-Momentum The key axiom of mechanics

Define velocity vector points

$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix}, \quad \mathbf{V}^{COM} = \begin{pmatrix} V_{SUV}^{COM} \\ V_{VW}^{COM} \end{pmatrix}, \quad \mathbf{V}^{IN} = \begin{pmatrix} V_{SUV}^{IN} \\ V_{VW}^{IN} \end{pmatrix}$$

Points of vectors

\mathbf{V}^{FIN} and \mathbf{V}^{COM} and \mathbf{V}^{IN}
all lie on

momentum - conservation line

Vector \mathbf{V}^{COM} is along *45° line*

Algebra, Geometry, and Physics of Momentum Conservation Axiom

Conservation of momentum line: \rightarrow

$$(M_{SUV} + M_{VW}) V^{COM} = M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN} = M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}$$

Mass weighted average velocity at anytime is Center of Mass velocity V^{COM} :

$$const. = V^{COM} = \frac{M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN}}{(M_{SUV} + M_{VW})} = \frac{M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}}{(M_{SUV} + M_{VW})}$$

Express this using velocity vectors:

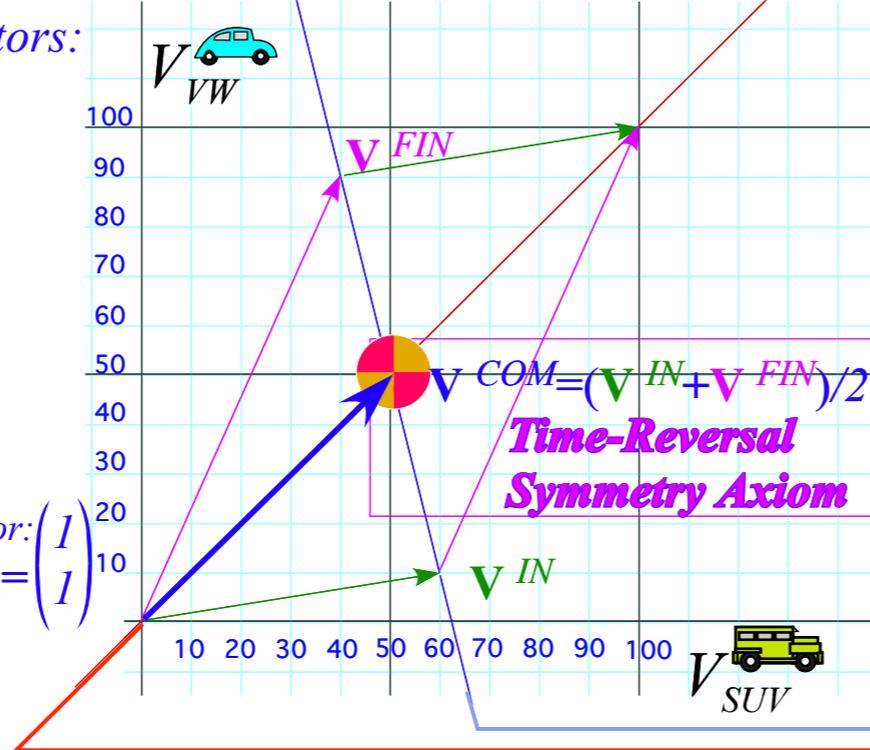
$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix} = \begin{pmatrix} 40 \\ 90 \end{pmatrix}$$

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 ...and matrix operators:

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Developing Conservation-of-Momentum The key axiom of mechanics

Define velocity vector points

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Points of vectors

\mathbf{V}^{FIN} and \mathbf{V}^{COM} and \mathbf{V}^{IN}

all lie on

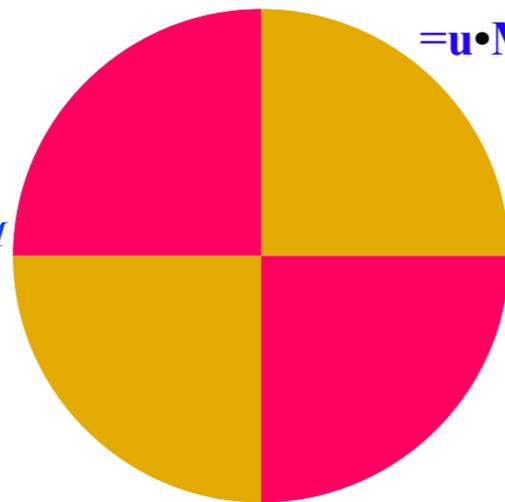
momentum - conservation line

Vector \mathbf{V}^{COM} is along *45° line*

...that give momentum vector: $\mathbf{P} = \mathbf{M} \cdot \mathbf{V} = \begin{pmatrix} M_{SUV} & 0 \\ 0 & M_{VW} \end{pmatrix} \begin{pmatrix} V_{SUV} \\ V_{VW} \end{pmatrix} = \begin{pmatrix} P_{SUV} \\ P_{VW} \end{pmatrix} = \begin{pmatrix} M_{SUV} V_{SUV} \\ M_{VW} V_{VW} \end{pmatrix}$
 whose sum of components is constant.
 (by $\mathbf{u} \cdot$ product)

$$const. = \mathbf{u} \cdot \mathbf{P} = P_{SUV} + P_{VW} = M_{SUV} V_{SUV} + M_{VW} V_{VW} = \mathbf{u} \cdot \mathbf{M} \cdot \mathbf{V} = \mathbf{u} \cdot \mathbf{M} \cdot \mathbf{V}^{IN} = \mathbf{u} \cdot \mathbf{M} \cdot \mathbf{V}^{FIN}$$

Denote Center of Momentum \mathbf{V}^{COM} with engineer's centering symbol



Algebra, Geometry, and Physics of Momentum Conservation Axiom

Conservation of momentum line: \rightarrow

$$(M_{SUV} + M_{VW}) V^{COM} = M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN} = M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}$$

Mass weighted average velocity at anytime is Center of Mass velocity V^{COM} :

$$const. = V^{COM} = \frac{M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN}}{(M_{SUV} + M_{VW})} = \frac{M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}}{(M_{SUV} + M_{VW})}$$

Express this using velocity vectors:

$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix} = \begin{pmatrix} 40 \\ 90 \end{pmatrix}$$

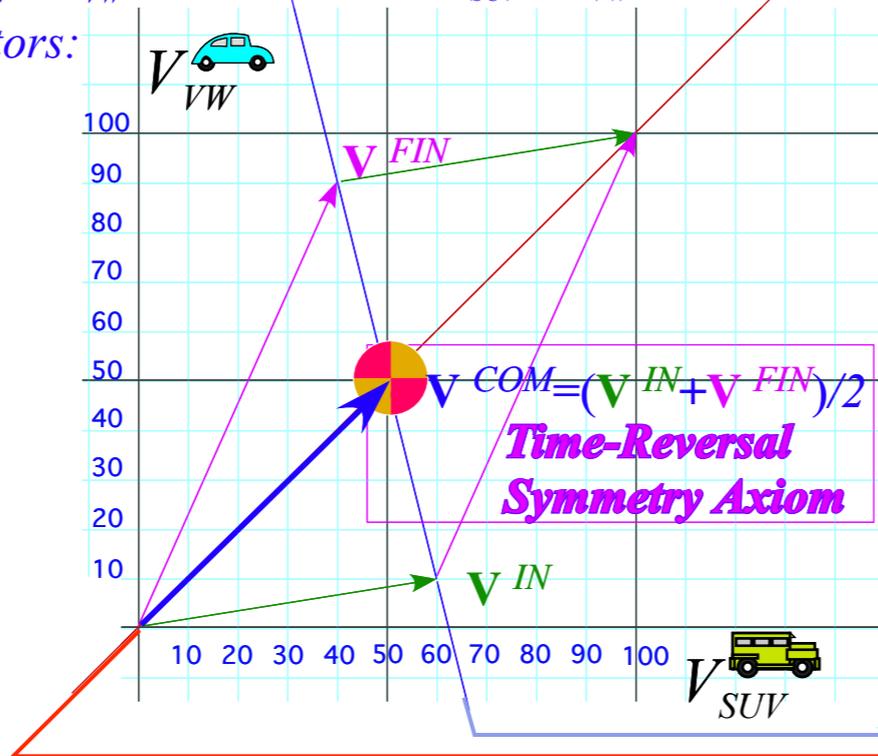
$$\mathbf{V}^{IN} = \begin{pmatrix} V_{SUV}^{IN} \\ V_{VW}^{IN} \end{pmatrix} = \begin{pmatrix} 60 \\ 10 \end{pmatrix}$$

$$\mathbf{V}^{COM} = \begin{pmatrix} V^{COM} \\ V^{COM} \end{pmatrix} = V^{COM} \begin{pmatrix} 1 \\ 1 \end{pmatrix}$$

$$= V^{COM} \mathbf{u}$$

...and matrix operators:

$$\mathbf{M} = \begin{pmatrix} M_{SUV} & 0 \\ 0 & M_{VW} \end{pmatrix}$$



...that give momentum vector: $\mathbf{P} = \mathbf{M} \cdot \mathbf{V} = \begin{pmatrix} M_{SUV} & 0 \\ 0 & M_{VW} \end{pmatrix} \begin{pmatrix} V_{SUV} \\ V_{VW} \end{pmatrix} = \begin{pmatrix} P_{SUV} \\ P_{VW} \end{pmatrix} = \begin{pmatrix} M_{SUV} V_{SUV} \\ M_{VW} V_{VW} \end{pmatrix}$
 whose sum of components is constant.
 (by $\mathbf{u} \cdot \mathbf{p}$ product)

$$const. = \mathbf{u} \cdot \mathbf{P} = P_{SUV} + P_{VW} = M_{SUV} V_{SUV} + M_{VW} V_{VW} = \mathbf{u} \cdot \mathbf{M} \cdot \mathbf{V} = \mathbf{u} \cdot \mathbf{M} \cdot \mathbf{V}^{IN} = \mathbf{u} \cdot \mathbf{M} \cdot \mathbf{V}^{FIN}$$

Then: $\mathbf{V}^{COM} = V^{COM} \mathbf{u}$ gives:

$$\mathbf{V}^{COM} \cdot \mathbf{M} \cdot \mathbf{V}^{COM} = \mathbf{V}^{COM} \cdot \mathbf{M} \cdot \mathbf{V}^{IN} = \mathbf{V}^{COM} \cdot \mathbf{M} \cdot \mathbf{V}^{FIN}$$

Developing Conservation-of-Momentum The key axiom of mechanics

Define velocity vector points

$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix}, \quad \mathbf{V}^{COM} = \begin{pmatrix} V_{SUV}^{COM} \\ V_{VW}^{COM} \end{pmatrix}, \quad \mathbf{V}^{IN} = \begin{pmatrix} V_{SUV}^{IN} \\ V_{VW}^{IN} \end{pmatrix}$$

Points of vectors

\mathbf{V}^{FIN} and \mathbf{V}^{COM} and \mathbf{V}^{IN}

all lie on

momentum - conservation line

Vector \mathbf{V}^{COM} is along *45° line*

Algebra, Geometry, and Physics of momentum conservation axiom

Vector algebra of collisions

Matrix or tensor algebra of collisions

 *Deriving Energy Conservation Theorem*

Energy Ellipse geometry

Algebra, Geometry, and Physics of Momentum Conservation Axiom

Conservation of momentum line: \rightarrow

$$(M_{SUV} + M_{VW}) V^{COM} = M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN} = M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}$$

Mass weighted average velocity at anytime is Center of Mass velocity V^{COM} :

$$const. = V^{COM} = \frac{M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN}}{(M_{SUV} + M_{VW})} = \frac{M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}}{(M_{SUV} + M_{VW})}$$

Express this using velocity vectors:

$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix} = \begin{pmatrix} 40 \\ 90 \end{pmatrix}$$

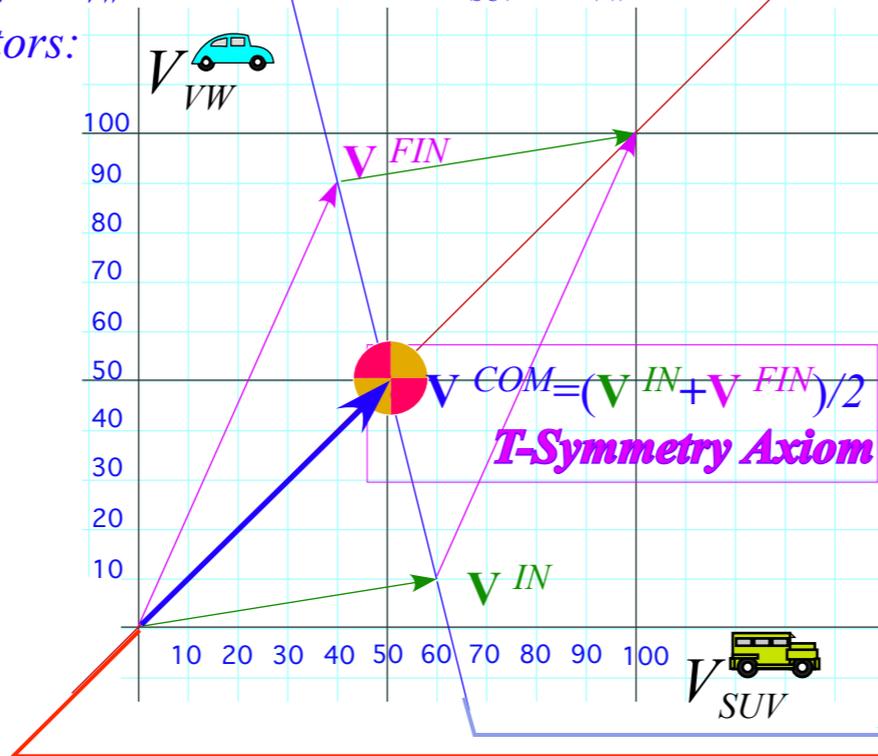
$$\mathbf{V}^{IN} = \begin{pmatrix} V_{SUV}^{IN} \\ V_{VW}^{IN} \end{pmatrix} = \begin{pmatrix} 60 \\ 10 \end{pmatrix}$$

$$\mathbf{V}^{COM} = \begin{pmatrix} V^{COM} \\ V^{COM} \end{pmatrix} = V^{COM} \begin{pmatrix} 1 \\ 1 \end{pmatrix}$$

$$= V^{COM} \mathbf{u}$$

...and matrix operators:

$$\mathbf{M} = \begin{pmatrix} M_{SUV} & 0 \\ 0 & M_{VW} \end{pmatrix}$$



...that give momentum vector: $\mathbf{P} = \mathbf{M} \cdot \mathbf{V} = \begin{pmatrix} M_{SUV} & 0 \\ 0 & M_{VW} \end{pmatrix} \begin{pmatrix} V_{SUV} \\ V_{VW} \end{pmatrix} = \begin{pmatrix} P_{SUV} \\ P_{VW} \end{pmatrix} = \begin{pmatrix} M_{SUV} V_{SUV} \\ M_{VW} V_{VW} \end{pmatrix}$
 whose sum of components is constant.
 (by $\mathbf{u} \cdot \mathbf{p}$ product)

$$const. = \mathbf{u} \cdot \mathbf{P} = P_{SUV} + P_{VW} = M_{SUV} V_{SUV} + M_{VW} V_{VW} = \mathbf{u} \cdot \mathbf{M} \cdot \mathbf{V} = \mathbf{u} \cdot \mathbf{M} \cdot \mathbf{V}^{IN} = \mathbf{u} \cdot \mathbf{M} \cdot \mathbf{V}^{FIN}$$

Then: $\mathbf{V}^{COM} = V^{COM} \mathbf{u}$ gives:

$$\mathbf{V}^{COM} \cdot \mathbf{M} \cdot \mathbf{V}^{COM} = \mathbf{V}^{COM} \cdot \mathbf{M} \cdot \mathbf{V}^{IN} = \mathbf{V}^{COM} \cdot \mathbf{M} \cdot \mathbf{V}^{FIN}$$

By **T-Symmetry Axiom**: $\mathbf{V}^{COM} = 1/2(\mathbf{V}^{IN} + \mathbf{V}^{FIN})$.

Developing Conservation-of-Momentum The key axiom of mechanics

Define velocity vector points

$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix}, \quad \mathbf{V}^{COM} = \begin{pmatrix} V_{SUV}^{COM} \\ V_{VW}^{COM} \end{pmatrix}, \quad \mathbf{V}^{IN} = \begin{pmatrix} V_{SUV}^{IN} \\ V_{VW}^{IN} \end{pmatrix}$$

Points of vectors

\mathbf{V}^{FIN} and \mathbf{V}^{COM} and \mathbf{V}^{IN}
all lie on

momentum - conservation line

Vector \mathbf{V}^{COM} is along **45° line**

Algebra, Geometry, and Physics of Momentum Conservation Axiom

Conservation of momentum line: \rightarrow

$$(M_{SUV} + M_{VW}) V^{COM} = M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN} = M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}$$

Mass weighted average velocity at anytime is Center of Mass velocity V^{COM} :

$$const. = V^{COM} = \frac{M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN}}{(M_{SUV} + M_{VW})} = \frac{M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}}{(M_{SUV} + M_{VW})}$$

Express this using velocity vectors:

$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix} = \begin{pmatrix} 40 \\ 90 \end{pmatrix}$$

$$\mathbf{V}^{IN} = \begin{pmatrix} V_{SUV}^{IN} \\ V_{VW}^{IN} \end{pmatrix} = \begin{pmatrix} 60 \\ 10 \end{pmatrix}$$

$$\mathbf{V}^{COM} = \begin{pmatrix} V^{COM} \\ V^{COM} \end{pmatrix} = V^{COM} \begin{pmatrix} 1 \\ 1 \end{pmatrix}$$

$$= V^{COM} \mathbf{u}$$

...and matrix operators:

$$\mathbf{M} = \begin{pmatrix} M_{SUV} & 0 \\ 0 & M_{VW} \end{pmatrix} = \mathbf{M}^{Transpose}$$

M-symmetry $\mathbf{M} = \mathbf{M}^T$

...that give momentum vector: $\mathbf{P} = \mathbf{M} \cdot \mathbf{V} = \begin{pmatrix} M_{SUV} & 0 \\ 0 & M_{VW} \end{pmatrix} \begin{pmatrix} V_{SUV} \\ V_{VW} \end{pmatrix} = \begin{pmatrix} P_{SUV} \\ P_{VW} \end{pmatrix} = \begin{pmatrix} M_{SUV} V_{SUV} \\ M_{VW} V_{VW} \end{pmatrix}$

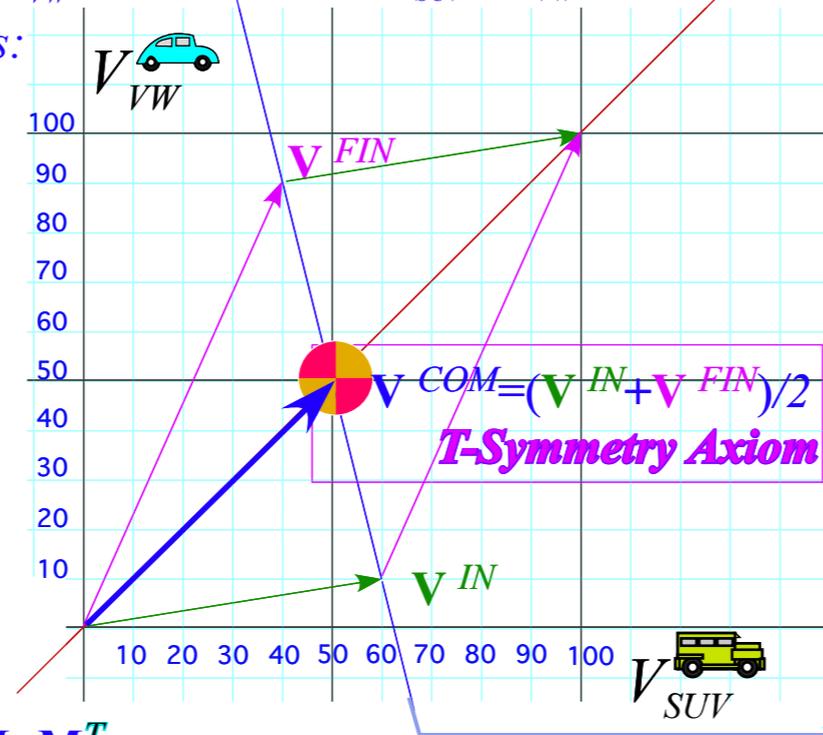
whose sum of components is constant.
(by $\mathbf{u} \cdot \mathbf{p}$ product)

$$const. = \mathbf{u} \cdot \mathbf{P} = P_{SUV} + P_{VW} = M_{SUV} V_{SUV} + M_{VW} V_{VW} = \mathbf{u} \cdot \mathbf{M} \cdot \mathbf{V} = \mathbf{u} \cdot \mathbf{M} \cdot \mathbf{V}^{IN} = \mathbf{u} \cdot \mathbf{M} \cdot \mathbf{V}^{FIN}$$

Then: $\mathbf{V}^{COM} = V^{COM} \mathbf{u}$ gives:

$$\mathbf{V}^{COM} \cdot \mathbf{M} \cdot \mathbf{V}^{COM} = \mathbf{V}^{COM} \cdot \mathbf{M} \cdot \mathbf{V}^{IN} = \mathbf{V}^{COM} \cdot \mathbf{M} \cdot \mathbf{V}^{FIN}$$

By **T-Symmetry Axiom**: $\mathbf{V}^{COM} = 1/2(\mathbf{V}^{IN} + \mathbf{V}^{FIN})$.



Developing Conservation-of-Momentum The key axiom of mechanics

Define velocity vector points

$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix}, \quad \mathbf{V}^{COM} = \begin{pmatrix} V_{SUV}^{COM} \\ V_{VW}^{COM} \end{pmatrix}, \quad \mathbf{V}^{IN} = \begin{pmatrix} V_{SUV}^{IN} \\ V_{VW}^{IN} \end{pmatrix}$$

Points of vectors

\mathbf{V}^{FIN} and \mathbf{V}^{COM} and \mathbf{V}^{IN}

all lie on

momentum - conservation line

Vector \mathbf{V}^{COM} is along **45° line**

Algebra, Geometry, and Physics of Momentum Conservation Axiom

Conservation of momentum line: \rightarrow

$$(M_{SUV} + M_{VW}) V^{COM} = M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN} = M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}$$

Mass weighted average velocity at anytime is Center of Mass velocity V^{COM} :

$$const. = V^{COM} = \frac{M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN}}{(M_{SUV} + M_{VW})} = \frac{M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}}{(M_{SUV} + M_{VW})}$$

Express this using velocity vectors:

$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix} = \begin{pmatrix} 40 \\ 90 \end{pmatrix}$$

$$\mathbf{V}^{IN} = \begin{pmatrix} V_{SUV}^{IN} \\ V_{VW}^{IN} \end{pmatrix} = \begin{pmatrix} 60 \\ 10 \end{pmatrix}$$

$$\mathbf{V}^{COM} = \begin{pmatrix} V^{COM} \\ V^{COM} \end{pmatrix} = V^{COM} \begin{pmatrix} 1 \\ 1 \end{pmatrix}$$

$$= V^{COM} \mathbf{u}$$

...and matrix operators:

$$\mathbf{M} = \begin{pmatrix} M_{SUV} & 0 \\ 0 & M_{VW} \end{pmatrix} = \mathbf{M}^{Transpose}$$

M-symmetry $\mathbf{M} = \mathbf{M}^T$

...that give **momentum vector**: $\mathbf{P} = \mathbf{M} \cdot \mathbf{V} = \begin{pmatrix} M_{SUV} & 0 \\ 0 & M_{VW} \end{pmatrix} \begin{pmatrix} V_{SUV} \\ V_{VW} \end{pmatrix} = \begin{pmatrix} P_{SUV} \\ P_{VW} \end{pmatrix} = \begin{pmatrix} M_{SUV} V_{SUV} \\ M_{VW} V_{VW} \end{pmatrix}$
 whose sum of components is constant.
 (by $\mathbf{u} \cdot \mathbf{p}$ product)

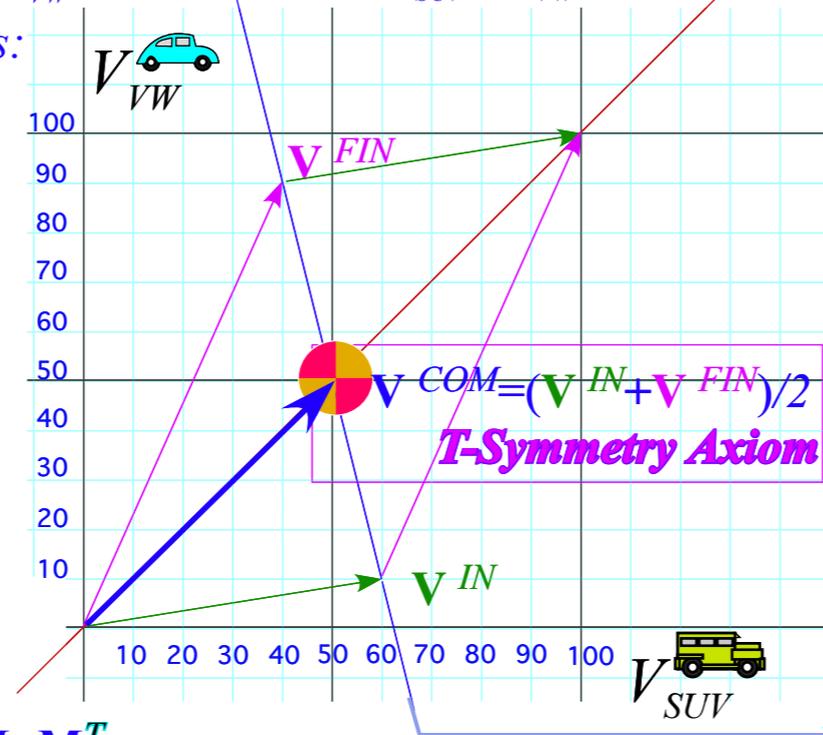
$$const. = \mathbf{u} \cdot \mathbf{P} = P_{SUV} + P_{VW} = M_{SUV} V_{SUV} + M_{VW} V_{VW} = \mathbf{u} \cdot \mathbf{M} \cdot \mathbf{V} = \mathbf{u} \cdot \mathbf{M} \cdot \mathbf{V}^{IN} = \mathbf{u} \cdot \mathbf{M} \cdot \mathbf{V}^{FIN}$$

Then: $\mathbf{V}^{COM} = V^{COM} \mathbf{u}$ gives:

$$\mathbf{V}^{COM} \cdot \mathbf{M} \cdot \mathbf{V}^{COM} = \mathbf{V}^{COM} \cdot \mathbf{M} \cdot \mathbf{V}^{IN} = \mathbf{V}^{COM} \cdot \mathbf{M} \cdot \mathbf{V}^{FIN}$$

By **T-Symmetry Axiom**: $\mathbf{V}^{COM} = 1/2(\mathbf{V}^{IN} + \mathbf{V}^{FIN})$. Substituting:

$$\mathbf{V}^{COM} \cdot \mathbf{M} \cdot \mathbf{V}^{COM} = 1/2(\mathbf{V}^{IN} + \mathbf{V}^{FIN}) \cdot \mathbf{M} \cdot \mathbf{V}^{IN} = 1/2(\mathbf{V}^{IN} + \mathbf{V}^{FIN}) \cdot \mathbf{M} \cdot \mathbf{V}^{FIN}$$



Developing Conservation-of-Momentum

The key axiom of mechanics

Define velocity vector points

$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix}, \quad \mathbf{V}^{COM} = \begin{pmatrix} V_{SUV}^{COM} \\ V_{VW}^{COM} \end{pmatrix}, \quad \mathbf{V}^{IN} = \begin{pmatrix} V_{SUV}^{IN} \\ V_{VW}^{IN} \end{pmatrix}$$

Points of vectors

\mathbf{V}^{FIN} and \mathbf{V}^{COM} and \mathbf{V}^{IN}

all lie on

momentum - conservation line

Vector \mathbf{V}^{COM} is along **45° line**

Algebra, Geometry, and Physics of Momentum Conservation Axiom

Conservation of momentum line: \rightarrow

$$(M_{SUV} + M_{VW}) V^{COM} = M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN} = M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}$$

Mass weighted average velocity at anytime is Center of Mass velocity V^{COM} :

$$const. = V^{COM} = \frac{M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN}}{(M_{SUV} + M_{VW})} = \frac{M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}}{(M_{SUV} + M_{VW})}$$

Express this using velocity vectors:

$$\mathbf{V}^{IN} = \begin{pmatrix} V_{SUV}^{IN} \\ V_{VW}^{IN} \end{pmatrix}$$

$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix}$$

$$\mathbf{V}^{COM} = \begin{pmatrix} V^{COM} \\ V^{COM} \end{pmatrix} = V^{COM} \begin{pmatrix} 1 \\ 1 \end{pmatrix}$$

$$= V^{COM} \mathbf{u}$$

...and matrix operators:

$$\mathbf{M} = \begin{pmatrix} M_{SUV} & 0 \\ 0 & M_{VW} \end{pmatrix} = \mathbf{M}^{Transpose}$$

M-symmetry $\mathbf{M} = \mathbf{M}^T$

...that give momentum vector: $\mathbf{P} = \mathbf{M} \cdot \mathbf{V} = \begin{pmatrix} M_{SUV} & 0 \\ 0 & M_{VW} \end{pmatrix} \begin{pmatrix} V_{SUV} \\ V_{VW} \end{pmatrix} = \begin{pmatrix} P_{SUV} \\ P_{VW} \end{pmatrix} = \begin{pmatrix} M_{SUV} V_{SUV} \\ M_{VW} V_{VW} \end{pmatrix}$

whose sum of components is constant.

(by $\mathbf{u} \cdot$ product)

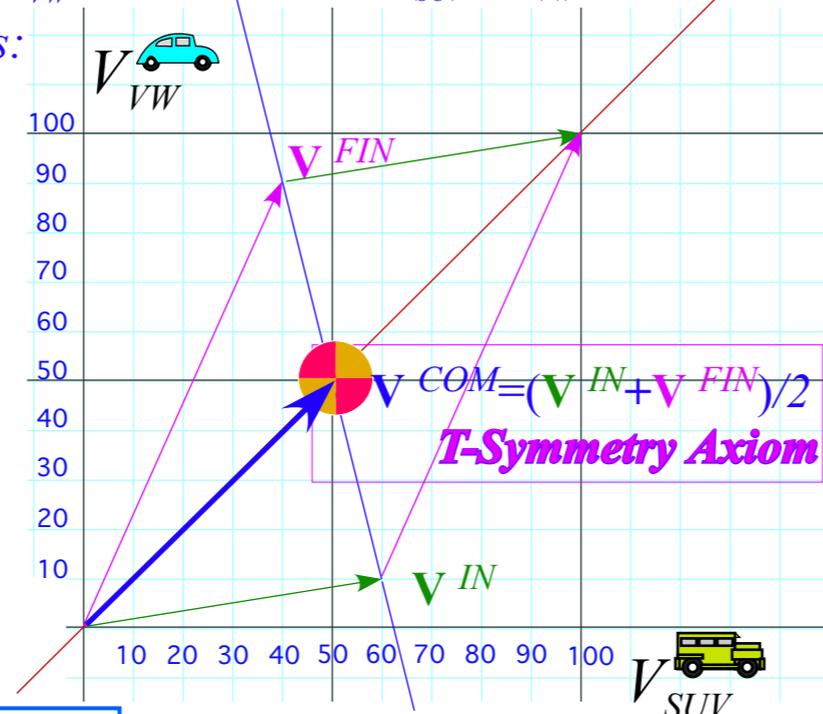
$$const. = \mathbf{u} \cdot \mathbf{P} = P_{SUV} + P_{VW} = M_{SUV} V_{SUV} + M_{VW} V_{VW} = \mathbf{u} \cdot \mathbf{M} \cdot \mathbf{V}$$

Then: $\mathbf{V}^{COM} = V^{COM} \mathbf{u}$ gives:

$$\mathbf{V}^{COM} \cdot \mathbf{M} \cdot \mathbf{V}^{COM} = V^{COM} \cdot \mathbf{M} \cdot V_{SUV}^{IN} = V^{COM} \cdot \mathbf{M} \cdot V_{VW}^{FIN}$$

By **T-Symmetry Axiom**: $\mathbf{V}^{COM} = 1/2(\mathbf{V}^{IN} + \mathbf{V}^{FIN})$. Substituting:

$$\mathbf{V}^{COM} \cdot \mathbf{M} \cdot \mathbf{V}^{COM} = 1/2(\mathbf{V}^{IN} + \mathbf{V}^{FIN}) \cdot \mathbf{M} \cdot V_{SUV}^{IN} = 1/2(\mathbf{V}^{IN} + \mathbf{V}^{FIN}) \cdot \mathbf{M} \cdot V_{VW}^{FIN}$$



Developing Conservation-of-Momentum The key axiom of mechanics

Define velocity vector points

$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix}, \quad \mathbf{V}^{COM} = \begin{pmatrix} V_{SUV}^{COM} \\ V_{VW}^{COM} \end{pmatrix}, \quad \mathbf{V}^{IN} = \begin{pmatrix} V_{SUV}^{IN} \\ V_{VW}^{IN} \end{pmatrix}$$

By **M-symmetry $\mathbf{M} = \mathbf{M}^T$** : $\mathbf{V}^{FIN} \cdot \mathbf{M} \cdot \mathbf{V}^{IN} = \mathbf{V}^{IN} \cdot \mathbf{M} \cdot \mathbf{V}^{FIN}$
this becomes:

$$\mathbf{V}^{COM} \cdot \mathbf{M} \cdot \mathbf{V}^{COM} - 1/2 \mathbf{V}^{FIN} \cdot \mathbf{M} \cdot \mathbf{V}^{IN} = 1/2 \mathbf{V}^{IN} \cdot \mathbf{M} \cdot \mathbf{V}^{IN} - 1/2 \mathbf{V}^{FIN} \cdot \mathbf{M} \cdot \mathbf{V}^{FIN}$$

Algebra, Geometry, and Physics of momentum conservation axiom

Vector algebra of collisions

Matrix or tensor algebra of collisions

 *Completing derivation of Energy Conservation Theorem*

Energy Ellipse geometry

Algebra, Geometry, and Physics of Momentum Conservation Axiom

Conservation of momentum line: \rightarrow

$$(M_{SUV} + M_{VW}) V^{COM} = M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN} = M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}$$

Mass weighted average velocity at anytime is Center of Mass velocity V^{COM} :

$$const. = V^{COM} = \frac{M_{SUV} V_{SUV}^{IN} + M_{VW} V_{VW}^{IN}}{(M_{SUV} + M_{VW})} = \frac{M_{SUV} V_{SUV}^{FIN} + M_{VW} V_{VW}^{FIN}}{(M_{SUV} + M_{VW})}$$

Express this using velocity vectors:

$$\mathbf{V}^{IN} = \begin{pmatrix} V_{SUV}^{IN} \\ V_{VW}^{IN} \end{pmatrix}$$

$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix}$$

$$\mathbf{V}^{COM} = \begin{pmatrix} V^{COM} \\ V^{COM} \end{pmatrix} = V^{COM} \begin{pmatrix} 1 \\ 1 \end{pmatrix}$$

$$= V^{COM} \mathbf{u}$$

...and matrix operators:

$$\mathbf{M} = \begin{pmatrix} M_{SUV} & 0 \\ 0 & M_{VW} \end{pmatrix} = \mathbf{M}^{Transpose}$$

M-symmetry $\mathbf{M} = \mathbf{M}^T$

...that give momentum vector: $\mathbf{P} = \mathbf{M} \cdot \mathbf{V} = \begin{pmatrix} M_{SUV} & 0 \\ 0 & M_{VW} \end{pmatrix} \begin{pmatrix} V_{SUV} \\ V_{VW} \end{pmatrix} = \begin{pmatrix} P_{SUV} \\ P_{VW} \end{pmatrix} = \begin{pmatrix} M_{SUV} V_{SUV} \\ M_{VW} V_{VW} \end{pmatrix}$

whose sum of components is constant.
(by $\mathbf{u} \cdot$ product)

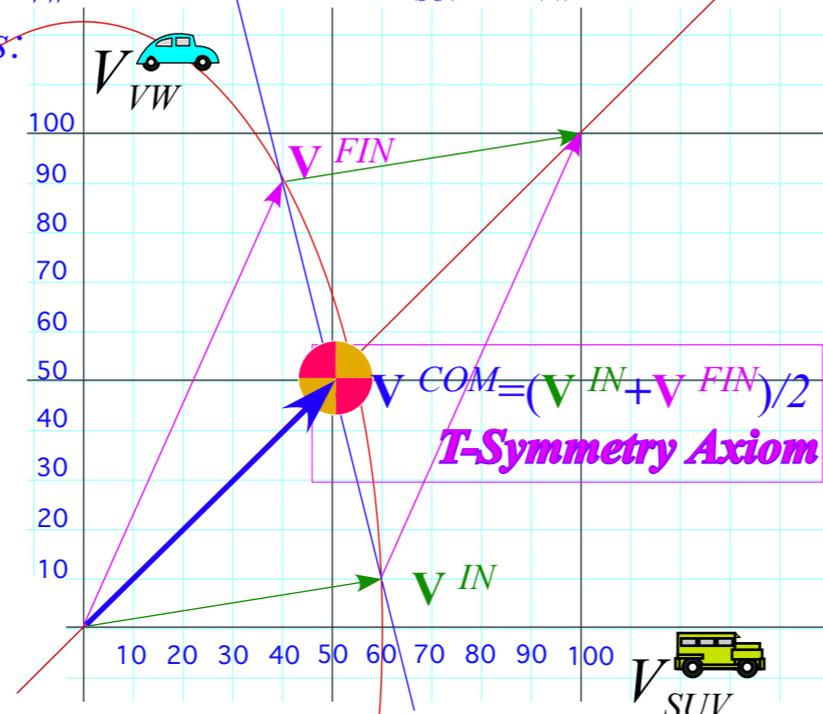
$$const. = \mathbf{u} \cdot \mathbf{P} = P_{SUV} + P_{VW} = M_{SUV} V_{SUV} + M_{VW} V_{VW} = \mathbf{u} \cdot \mathbf{M} \cdot \mathbf{V}$$

Then: $\mathbf{V}^{COM} = V^{COM} \mathbf{u}$ gives:

$$\mathbf{V}^{COM} \cdot \mathbf{M} \cdot \mathbf{V}^{COM} = \mathbf{V}^{COM} \cdot \mathbf{M} \cdot \mathbf{V}^{IN} = \mathbf{V}^{COM} \cdot \mathbf{M} \cdot \mathbf{V}^{FIN}$$

By **T-Symmetry Axiom**: $\mathbf{V}^{COM} = 1/2(\mathbf{V}^{IN} + \mathbf{V}^{FIN})$. Substituting:

$$\mathbf{V}^{COM} \cdot \mathbf{M} \cdot \mathbf{V}^{COM} = 1/2(\mathbf{V}^{IN} + \mathbf{V}^{FIN}) \cdot \mathbf{M} \cdot \mathbf{V}^{IN} = 1/2(\mathbf{V}^{IN} + \mathbf{V}^{FIN}) \cdot \mathbf{M} \cdot \mathbf{V}^{FIN}$$



Developing Conservation-of-Momentum

The key axiom of mechanics

leading to

Conservation-of-Energy Theorem

Define velocity vector points

$$\mathbf{V}^{FIN} = \begin{pmatrix} V_{SUV}^{FIN} \\ V_{VW}^{FIN} \end{pmatrix}, \quad \mathbf{V}^{COM} = \begin{pmatrix} V_{SUV}^{COM} \\ V_{VW}^{COM} \end{pmatrix}, \quad \mathbf{V}^{IN} = \begin{pmatrix} V_{SUV}^{IN} \\ V_{VW}^{IN} \end{pmatrix}$$

By **M-symmetry** $\mathbf{M} = \mathbf{M}^T$: $\mathbf{V}^{FIN} \cdot \mathbf{M} \cdot \mathbf{V}^{IN} = \mathbf{V}^{IN} \cdot \mathbf{M} \cdot \mathbf{V}^{FIN}$

this becomes:

$$\mathbf{V}^{COM} \cdot \mathbf{M} \cdot \mathbf{V}^{COM} - 1/2 \mathbf{V}^{FIN} \cdot \mathbf{M} \cdot \mathbf{V}^{IN} = 1/2 \mathbf{V}^{IN} \cdot \mathbf{M} \cdot \mathbf{V}^{IN} = 1/2 \mathbf{V}^{FIN} \cdot \mathbf{M} \cdot \mathbf{V}^{FIN}$$

These are equations for energy conservation ellipse:

$$\begin{aligned} const. &= 1/2 M_{SUV} V_{SUV}^2 + 1/2 M_{VW} V_{VW}^2 \\ &= 1/2 M_{SUV} V_{SUV}^2 + 1/2 M_{VW} V_{VW}^2 \\ &= \text{Kinetic Energy} = KE \text{ is now defined} \\ &\text{and proved a constant under T-Symmetry} \end{aligned}$$

Algebra, Geometry, and Physics of momentum conservation axiom

Vector algebra of collisions

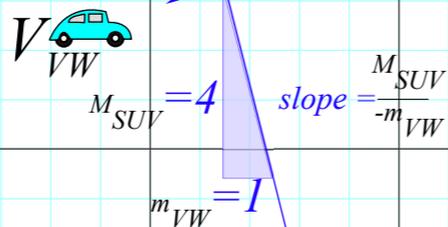
Matrix or tensor algebra of collisions

Deriving Energy Conservation Theorem

 *Energy Ellipse geometry*

Algebra, Geometry, and Physics of Momentum Conservation Axiom

Conservation of momentum line: \rightarrow (...one of ∞ -many...)



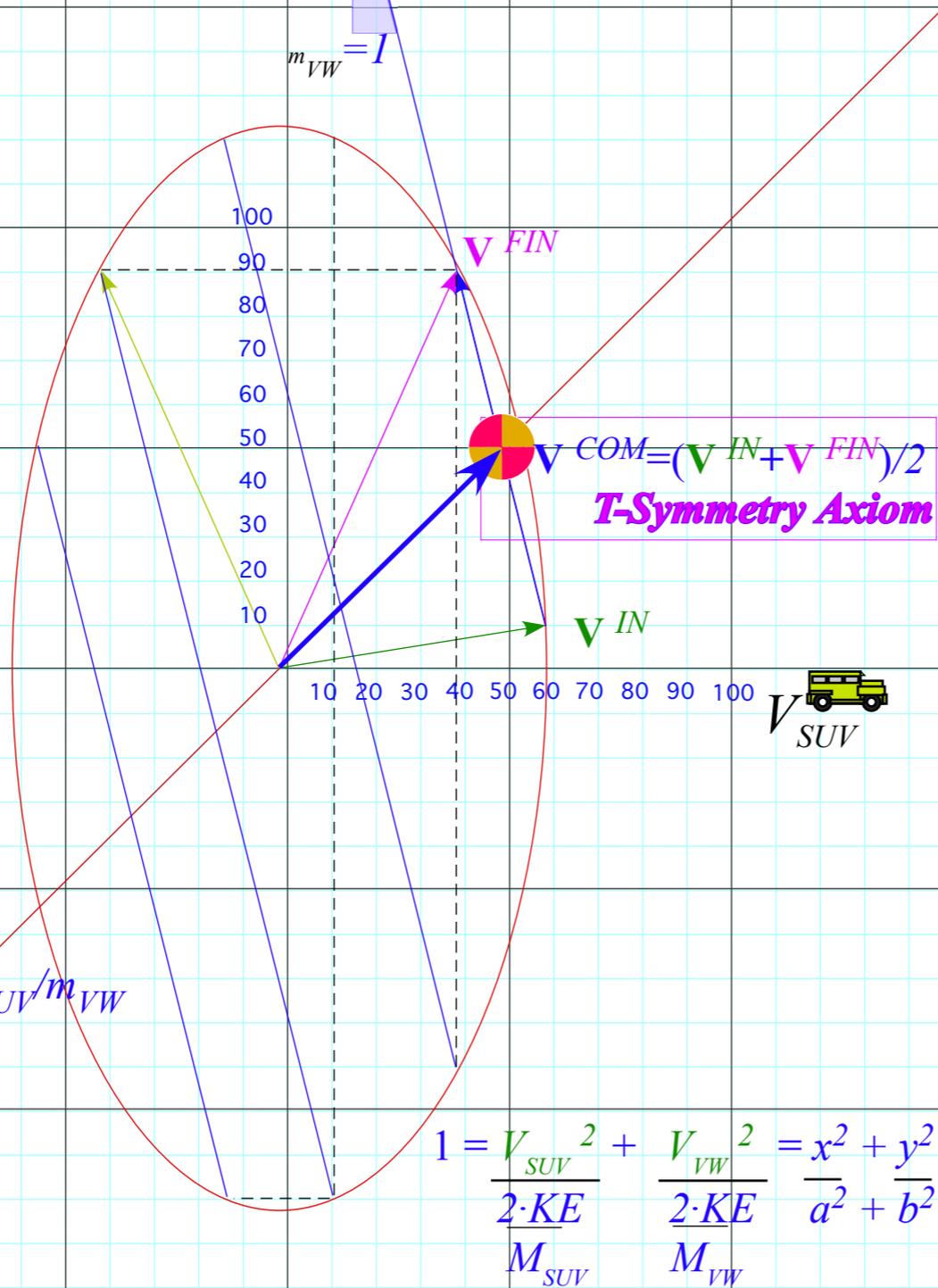
Momentum Conservation Axiom

plus

T-Symmetry Axiom
($M=M^T$ implied)

gives

Kinetic Energy Conservation Theorem



All lines of slope $-M_{SUV}/m_{VW}$
...are bisected by the
(slope=1)-COM line

$$1 = \frac{V_{SUV}^2}{\frac{2 \cdot KE}{M_{SUV}}} + \frac{V_{VW}^2}{\frac{2 \cdot KE}{M_{VW}}} = \frac{x^2}{a^2} + \frac{y^2}{b^2}$$

Developing
Conservation-of-Momentum
The key axiom of mechanics
leading to
Conservation-of-Energy Theorem

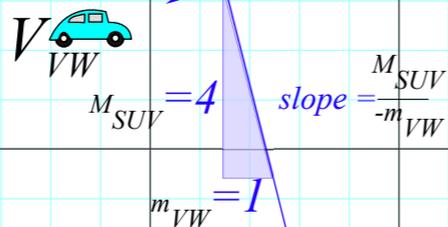
$$\mathbf{V}^{COM} \cdot \mathbf{M} \cdot \mathbf{V}^{COM} - 1/2 \mathbf{V}^{FIN} \cdot \mathbf{M} \cdot \mathbf{V}^{IN} = 1/2 \mathbf{V}^{IN} \cdot \mathbf{M} \cdot \mathbf{V}^{IN} = 1/2 \mathbf{V}^{FIN} \cdot \mathbf{M} \cdot \mathbf{V}^{FIN}$$

These are equations for energy conservation ellipse:

$$KE = 1/2 M_{SUV} V_{SUV}^2 + 1/2 M_{VW} V_{VW}^2$$

Algebra, Geometry, and Physics of Momentum Conservation Axiom

Conservation of momentum line: \rightarrow (...one of ∞ -many...)



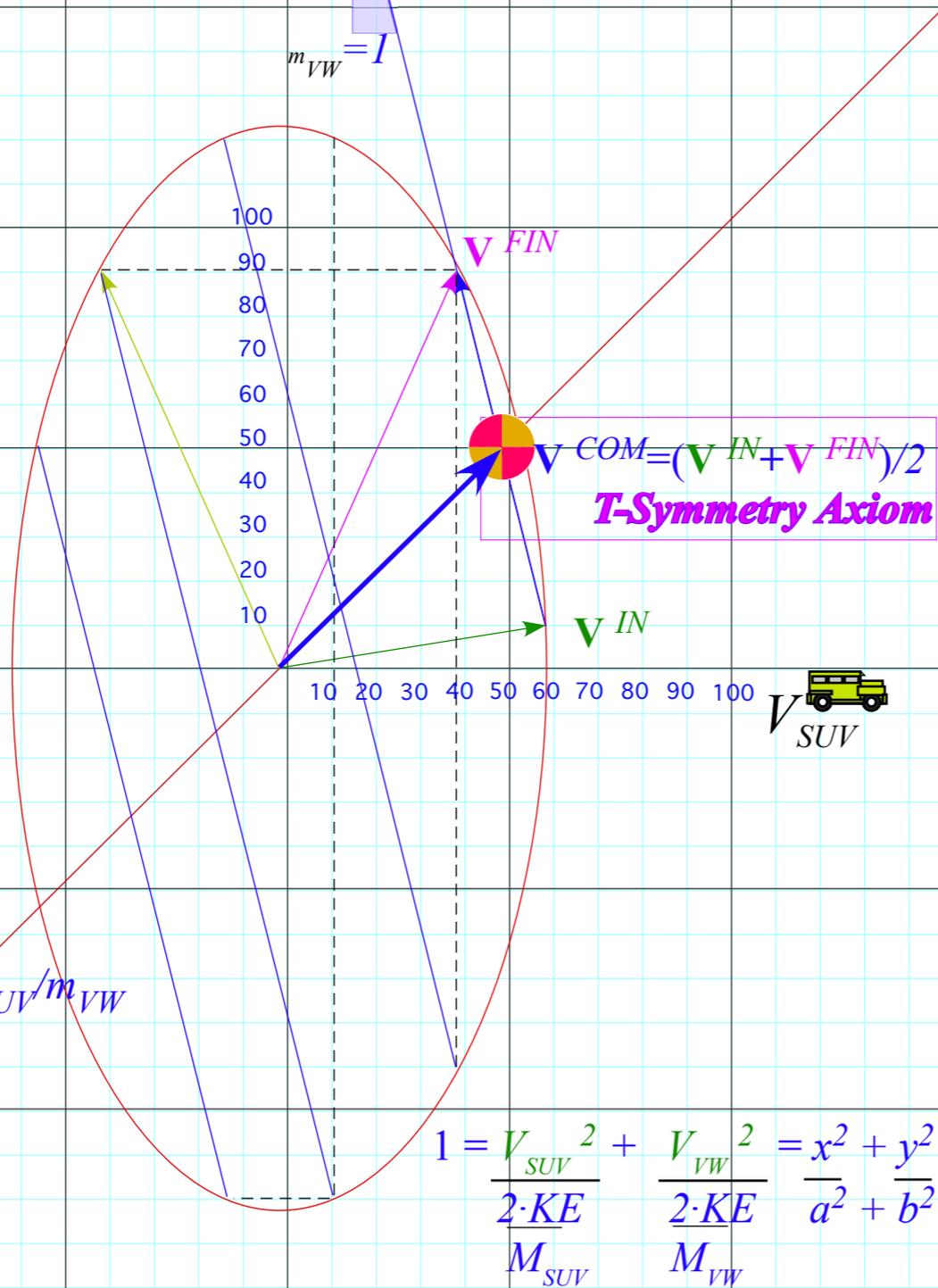
Momentum Conservation Axiom

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All lines of slope $-M_{SUV}/m_{VW}$
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$$1 = \frac{V_{SUV}^2}{\frac{2 \cdot KE}{M_{SUV}}} + \frac{V_{VW}^2}{\frac{2 \cdot KE}{M_{VW}}} = \frac{x^2}{a^2} + \frac{y^2}{b^2}$$

Developing
Conservation-of-Momentum
The key axiom of mechanics
leading to
Conservation-of-Energy Theorem

If and only if...
there is **T-Symmetry**

$$\mathbf{V}^{COM} \cdot \mathbf{M} \cdot \mathbf{V}^{COM} - 1/2 \mathbf{V}^{FIN} \cdot \mathbf{M} \cdot \mathbf{V}^{IN} = 1/2 \mathbf{V}^{IN} \cdot \mathbf{M} \cdot \mathbf{V}^{IN} = 1/2 \mathbf{V}^{FIN} \cdot \mathbf{M} \cdot \mathbf{V}^{FIN}$$

These are equations for energy conservation ellipse:

$$KE = 1/2 M_{SUV} V_{SUV}^2 + 1/2 M_{VW} V_{VW}^2$$

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If and only if...
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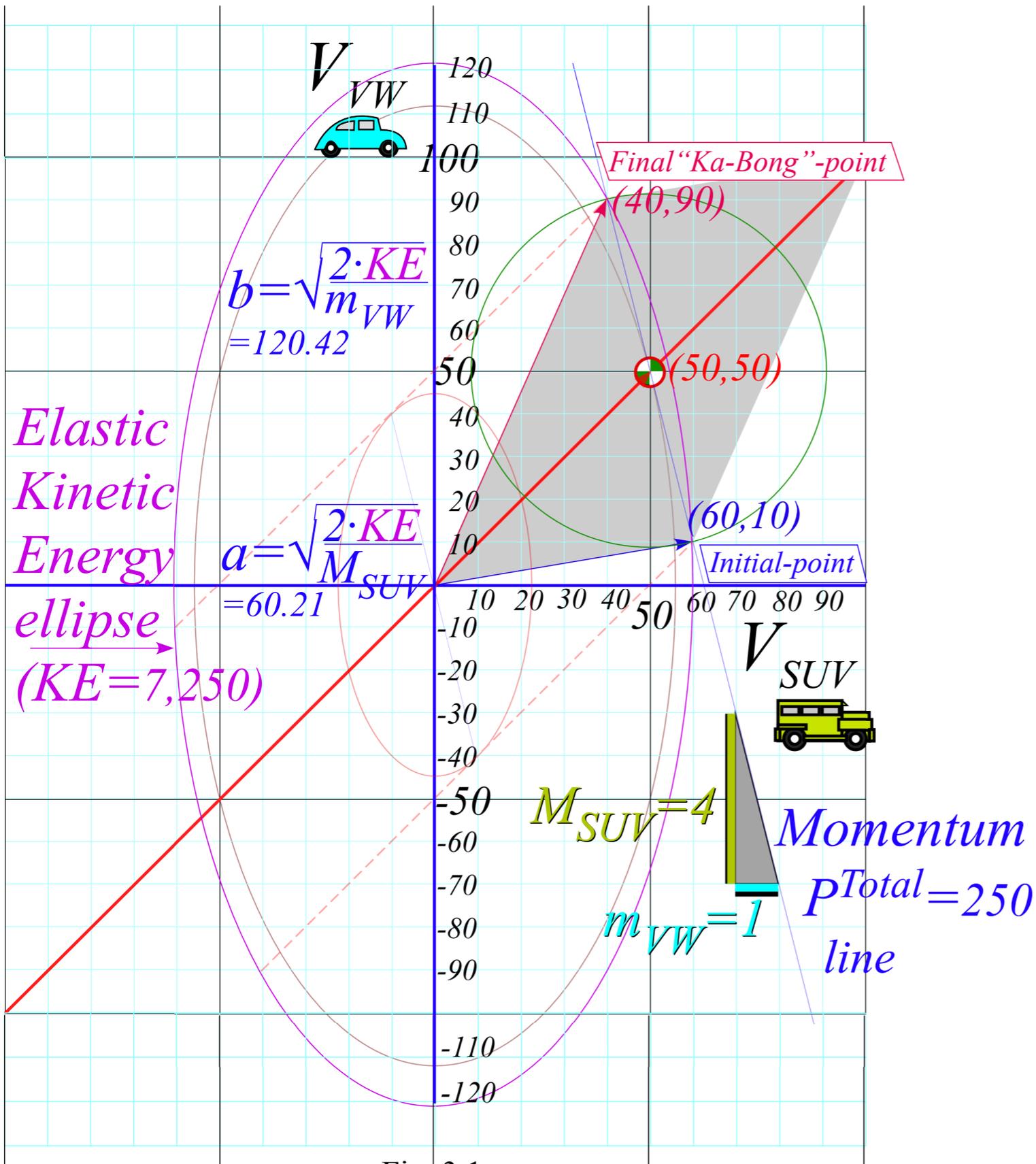


Fig. 3.1 a
 in Unit 1

Fig. 3.1

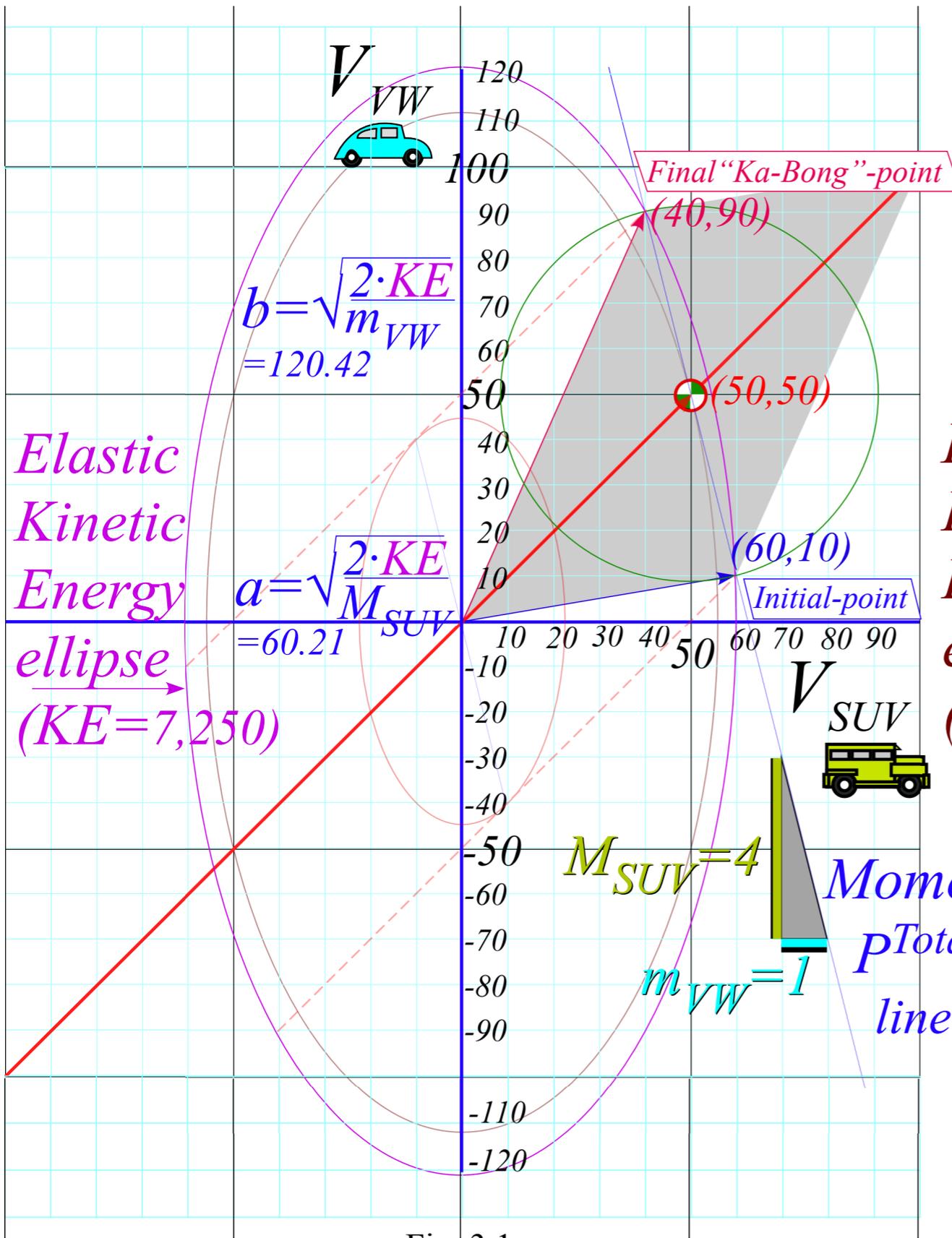


Fig. 3.1 a
in Unit 1

Inelastic
Kinetic
Energy
ellipse
($IE = 6,250$)

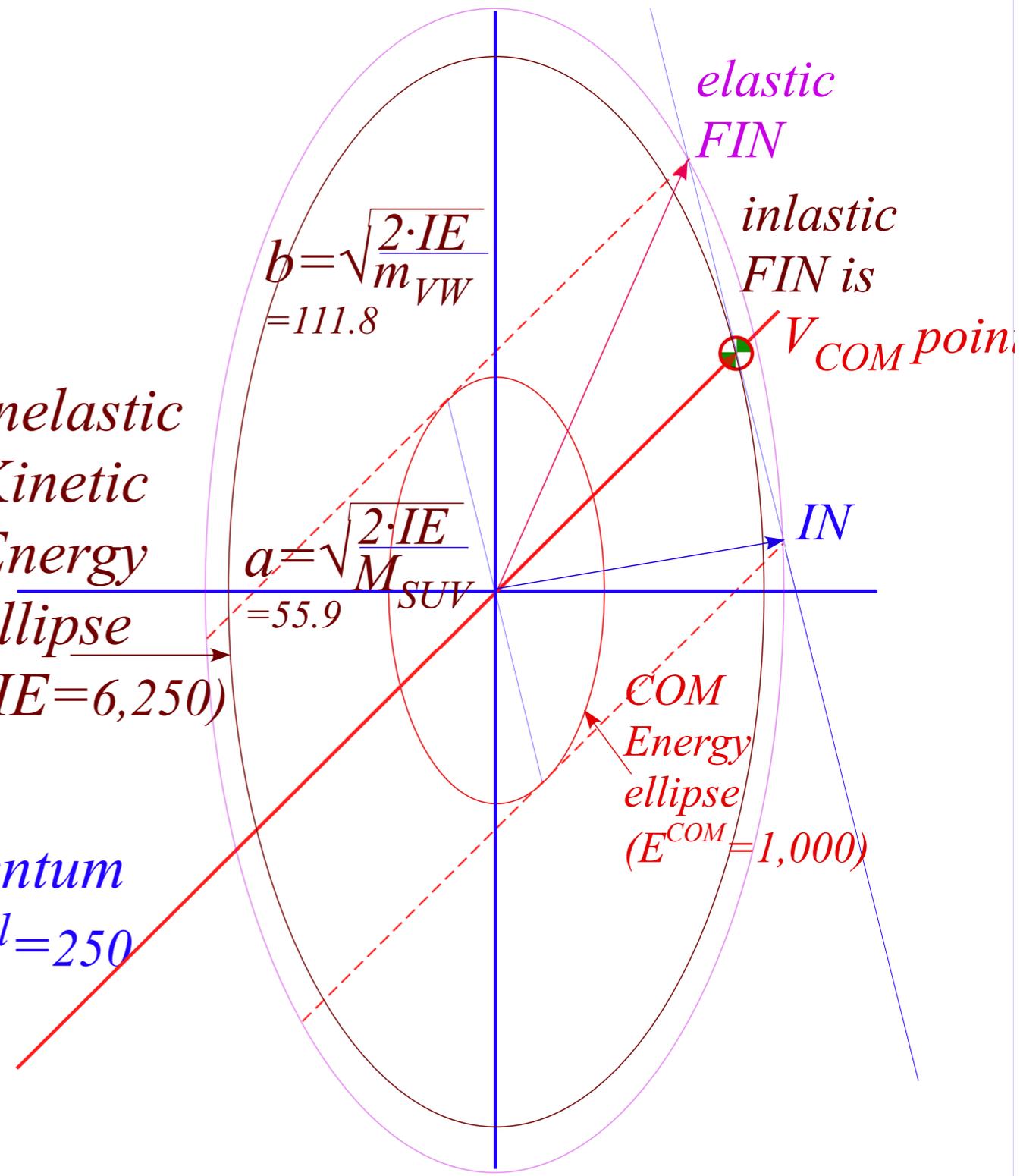


Fig. 3.1 b
in Unit 1

Fig. 3.1

As usual in physics, opposite extremes are easier to analyze than the generic “real(er) world” in between!

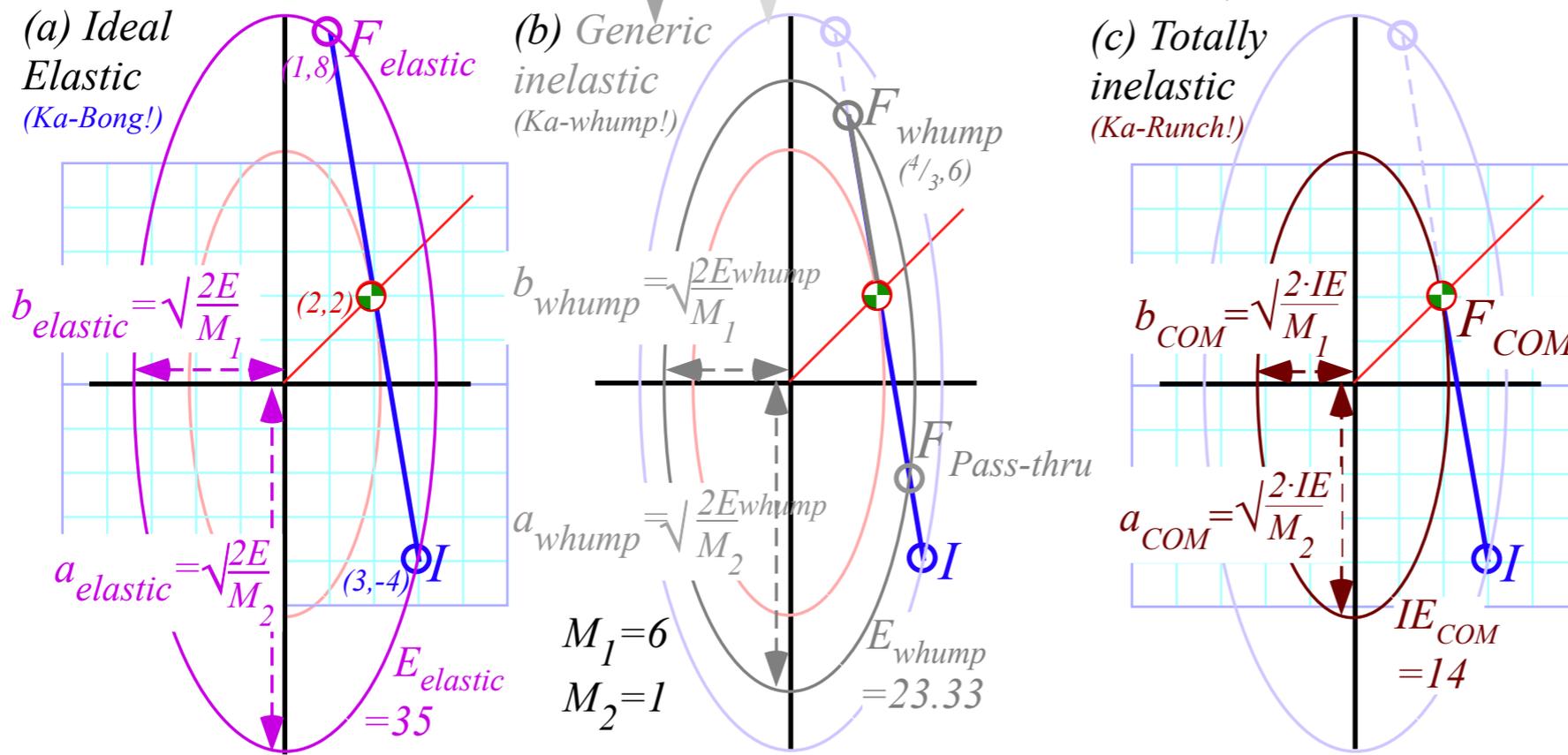


Fig. 3.2 *(This case has Bush era requisite SUV mass of the 6 ton “Hummer”)*
in Unit 1

Next: **The X-2 pen-launcher**

Here *T-Symmetry* is best

Here *T-Symmetry* is less

Here *T-Symmetry* is least

Numerical details of collision tensor algebra

General Inertia Tensor \mathbf{M} or inertia matrix of n^2 coefficients M_{jk} for dimension $n=2, 3, \dots$

$$\left. \begin{aligned} P_1 &= M_{11}V_1 + M_{12}V_2 \\ P_2 &= M_{21}V_1 + M_{22}V_2 \end{aligned} \right\} \text{denoted: } \vec{\mathbf{P}} = \vec{\mathbf{M}} \cdot \vec{\mathbf{V}} \quad \text{or: } \begin{pmatrix} P_1 \\ P_2 \end{pmatrix} = \begin{pmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{pmatrix} \begin{pmatrix} V_1 \\ V_2 \end{pmatrix}$$

With 45° diagonal \mathbf{V}^{COM} so: . $V_1^{COM} = V_2^{COM} \equiv V^{COM}$

$$P_{Total} = M_1 V_1^{IN} + M_2 V_2^{IN} = M_1 V_1^{FIN} + M_2 V_2^{FIN} = M_1 V^{COM} + M_2 V^{COM} = M_{Total} V^{COM}$$

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A product of total momentum P_{Total} and \mathbf{V}^{COM} is expressed by *tensor quadratic forms* $\mathbf{v} \cdot \mathbf{M} \cdot \mathbf{u}$

$$V^{COM} P_{Total} = \vec{\mathbf{V}}^{COM} \cdot \vec{\mathbf{M}} \cdot \vec{\mathbf{V}}^{IN} = \vec{\mathbf{V}}^{COM} \cdot \vec{\mathbf{M}} \cdot \vec{\mathbf{V}}^{FIN} = \vec{\mathbf{V}}^{COM} \cdot \vec{\mathbf{M}} \cdot \vec{\mathbf{V}}^{COM} = V^{COM} M_{Total} V^{COM}$$

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Write this out with the numbers used in Fig. 3.1 where $V^{COM} = 50$. (2 pages back)

$$\begin{aligned} 50 P_{Total} &= \begin{pmatrix} 50 & 50 \end{pmatrix} \cdot \begin{pmatrix} 4 & 0 \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 60 \\ 10 \end{pmatrix} = \begin{pmatrix} 50 & 50 \end{pmatrix} \cdot \begin{pmatrix} 4 & 0 \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 40 \\ 90 \end{pmatrix} = 50 M_{Total} 50 = 12,500 \\ &= 100 \cdot 125 = 100 \cdot 125 = 50 \cdot 250 \end{aligned}$$

General Inertia Tensor M or inertia matrix of n^2 coefficients M_{jk} for dimension $n=2, 3, \dots$

$$\left. \begin{aligned} P_1 &= M_{11}V_1 + M_{12}V_2 \\ P_2 &= M_{21}V_1 + M_{22}V_2 \end{aligned} \right\} \text{denoted: } \vec{\mathbf{P}} = \vec{\mathbf{M}} \cdot \vec{\mathbf{V}} \quad \text{or: } \begin{pmatrix} P_1 \\ P_2 \end{pmatrix} = \begin{pmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{pmatrix} \begin{pmatrix} V_1 \\ V_2 \end{pmatrix}$$

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$P_{Total} = 250$ is the same at **IN**, **FIN**, and **COM**. Now use T -symmetry: $\vec{\mathbf{V}}^{COM} = (\vec{\mathbf{V}}^{FIN} + \vec{\mathbf{V}}^{IN})/2$

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Transpose symmetry ($M_{jk} = M_{kj}$) of the \mathbf{M} -matrix implies: $\vec{\mathbf{V}}^{FIN} \cdot \vec{\mathbf{M}} \cdot \vec{\mathbf{V}}^{IN} = \vec{\mathbf{V}}^{IN} \cdot \vec{\mathbf{M}} \cdot \vec{\mathbf{V}}^{FIN}$

$$\begin{aligned} \begin{pmatrix} 40 & 90 \end{pmatrix} \cdot \begin{pmatrix} 4 & 0 \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 60 \\ 10 \end{pmatrix} &= \begin{pmatrix} 60 & 10 \end{pmatrix} \cdot \begin{pmatrix} 4 & 0 \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 40 \\ 90 \end{pmatrix} \\ &= 100 \cdot 105 = 100 \cdot 105 = 10,500 \end{aligned}$$

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With ($M_{12} = 0 = M_{21}$) kinetic energy $KE_{Elastic} = \frac{1}{2} \vec{V} \cdot \vec{M} \cdot \vec{V}$ is the same at $\mathbf{V} = \mathbf{V}^{IN}$ and $\mathbf{V} = \mathbf{V}^{FIN}$.

$$\begin{aligned} V^{COM} P_{Total} - \frac{\vec{V}^{FIN} \cdot \vec{M} \cdot \vec{V}^{IN}}{2} &= \frac{\vec{V}^{IN} \cdot \vec{M} \cdot \vec{V}^{IN}}{2} = \frac{\vec{V}^{FIN} \cdot \vec{M} \cdot \vec{V}^{FIN}}{2} = KE_{Elastic} \\ 12,500 - \frac{10,500}{2} &= \frac{\begin{pmatrix} 60 & 10 \end{pmatrix} \cdot \begin{pmatrix} 4 & 0 \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 60 \\ 10 \end{pmatrix}}{2} = \frac{\begin{pmatrix} 40 & 90 \end{pmatrix} \cdot \begin{pmatrix} 4 & 0 \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 40 \\ 90 \end{pmatrix}}{2} = KE_{Elastic} \\ 12,500 - 5,250 &= 7,250 = 7,250 \end{aligned}$$

Transpose symmetry ($M_{jk} = M_{kj}$) of the \mathbf{M} -matrix implies:

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Consider kinetic energy $KE_{inelastic} = IE$ when $\mathbf{V} = \mathbf{V}^{COM}$. It is reduced by $1,000$ from $7,250$ to $6,250$.

$$\begin{aligned} KE_{Inelastic} = V^{COM} P_{Total} - \frac{\vec{V}^{COM} \cdot \vec{M} \cdot \vec{V}^{COM}}{2} &= \frac{1}{2} V^{COM} P_{Total} = \frac{\vec{V}^{COM} \cdot \vec{M} \cdot \vec{V}^{COM}}{2} = \frac{\vec{V}^{IN} \cdot \vec{M} \cdot \vec{V}^{IN}}{4} + \frac{\vec{V}^{FIN} \cdot \vec{M} \cdot \vec{V}^{IN}}{4} = \frac{1}{2} KE_{Elastic} + \frac{\vec{V}^{FIN} \cdot \vec{M} \cdot \vec{V}^{IN}}{4} \\ 12,500 - \frac{12,500}{2} &= 6,250 = 6,250 = 3,625 + 2,625 = IE \end{aligned}$$

Transpose symmetry ($M_{jk} = M_{kj}$) of the \mathbf{M} -matrix implies:

$$\begin{aligned} \vec{V}^{FIN} \cdot \vec{M} \cdot \vec{V}^{IN} &= \vec{V}^{IN} \cdot \vec{M} \cdot \vec{V}^{FIN} \\ \begin{pmatrix} 40 & 90 \end{pmatrix} \cdot \begin{pmatrix} 4 & 0 \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 60 \\ 10 \end{pmatrix} &= \begin{pmatrix} 60 & 10 \end{pmatrix} \cdot \begin{pmatrix} 4 & 0 \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 40 \\ 90 \end{pmatrix} \\ &= 100 \cdot 105 = 10,500 \end{aligned}$$

With ($M_{12} = 0 = M_{21}$) kinetic energy $KE_{Elastic} = \frac{1}{2} \vec{V} \cdot \vec{M} \cdot \vec{V}$ is the same at $\mathbf{V} = \mathbf{V}^{IN}$ and $\mathbf{V} = \mathbf{V}^{FIN}$.

$$\begin{aligned} V^{COM} P_{Total} - \frac{\vec{V}^{FIN} \cdot \vec{M} \cdot \vec{V}^{IN}}{2} &= \frac{\vec{V}^{IN} \cdot \vec{M} \cdot \vec{V}^{IN}}{2} = \frac{\vec{V}^{FIN} \cdot \vec{M} \cdot \vec{V}^{FIN}}{2} = KE_{Elastic} \\ 12,500 - \frac{10,500}{2} &= \frac{\begin{pmatrix} 60 & 10 \end{pmatrix} \cdot \begin{pmatrix} 4 & 0 \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 60 \\ 10 \end{pmatrix}}{2} = \frac{\begin{pmatrix} 40 & 90 \end{pmatrix} \cdot \begin{pmatrix} 4 & 0 \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 40 \\ 90 \end{pmatrix}}{2} = KE_{Elastic} \\ 12,500 - 5,250 &= 7,250 = 7,250 \end{aligned}$$

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$$\begin{aligned} KE_{Inelastic} &= V^{COM} P_{Total} - \frac{\vec{V}^{COM} \cdot \vec{M} \cdot \vec{V}^{COM}}{2} = \frac{1}{2} V^{COM} P_{Total} = \frac{\vec{V}^{COM} \cdot \vec{M} \cdot \vec{V}^{COM}}{2} = \frac{\vec{V}^{IN} \cdot \vec{M} \cdot \vec{V}^{IN}}{4} + \frac{\vec{V}^{FIN} \cdot \vec{M} \cdot \vec{V}^{IN}}{4} = \frac{1}{2} KE_{Elastic} + \frac{\vec{V}^{FIN} \cdot \vec{M} \cdot \vec{V}^{IN}}{4} \\ 12,500 - \frac{12,500}{2} &= 6,250 = 6,250 = 3,625 + 2,625 = IE \\ KE_{Inelastic} &= \frac{1}{2} \vec{V}^{COM} \cdot \vec{M} \cdot \vec{V}^{COM} = \frac{1}{2} \begin{pmatrix} 50 & 50 \end{pmatrix} \cdot \begin{pmatrix} 4 & 0 \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 50 \\ 50 \end{pmatrix} = 6,250 \end{aligned}$$

Transpose symmetry ($M_{jk} = M_{kj}$) of the \mathbf{M} -matrix implies:

$$\begin{aligned} \vec{V}^{FIN} \cdot \vec{M} \cdot \vec{V}^{IN} &= \vec{V}^{IN} \cdot \vec{M} \cdot \vec{V}^{FIN} \\ \begin{pmatrix} 40 & 90 \end{pmatrix} \cdot \begin{pmatrix} 4 & 0 \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 60 \\ 10 \end{pmatrix} &= \begin{pmatrix} 60 & 10 \end{pmatrix} \cdot \begin{pmatrix} 4 & 0 \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 40 \\ 90 \end{pmatrix} \\ &= 100 \cdot 105 = 10,500 \end{aligned}$$

With ($M_{12} = 0 = M_{21}$) kinetic energy $KE_{Elastic} = \frac{1}{2} \vec{V} \cdot \vec{M} \cdot \vec{V}$ is the same at $\mathbf{V} = \mathbf{V}^{IN}$ and $\mathbf{V} = \mathbf{V}^{FIN}$.

$$\begin{aligned} V^{COM} P_{Total} - \frac{\vec{V}^{FIN} \cdot \vec{M} \cdot \vec{V}^{IN}}{2} &= \frac{\vec{V}^{IN} \cdot \vec{M} \cdot \vec{V}^{IN}}{2} = \frac{\vec{V}^{FIN} \cdot \vec{M} \cdot \vec{V}^{FIN}}{2} = KE_{Elastic} \\ 12,500 - \frac{10,500}{2} &= \frac{\begin{pmatrix} 60 & 10 \end{pmatrix} \cdot \begin{pmatrix} 4 & 0 \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 60 \\ 10 \end{pmatrix}}{2} = \frac{\begin{pmatrix} 40 & 90 \end{pmatrix} \cdot \begin{pmatrix} 4 & 0 \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 40 \\ 90 \end{pmatrix}}{2} = KE_{Elastic} \\ 12,500 - 5,250 &= 7,250 = 7,250 \end{aligned}$$

Consider kinetic energy $KE_{inelastic} = IE$ when $\mathbf{V} = \mathbf{V}^{COM}$. It is reduced by 1,000 from 7,250 to 6,250.

$$\begin{aligned} KE_{Inelastic} = V^{COM} P_{Total} - \frac{\vec{V}^{COM} \cdot \vec{M} \cdot \vec{V}^{COM}}{2} &= \frac{1}{2} V^{COM} P_{Total} = \frac{\vec{V}^{COM} \cdot \vec{M} \cdot \vec{V}^{COM}}{2} = \frac{\vec{V}^{IN} \cdot \vec{M} \cdot \vec{V}^{IN}}{4} + \frac{\vec{V}^{FIN} \cdot \vec{M} \cdot \vec{V}^{IN}}{4} = \frac{1}{2} KE_{Elastic} + \frac{\vec{V}^{FIN} \cdot \vec{M} \cdot \vec{V}^{IN}}{4} \\ 12,500 - \frac{12,500}{2} &= 6,250 = 6,250 = 3,625 + 2,625 = IE \end{aligned}$$

$$KE_{Inelastic} = \frac{1}{2} \vec{V}^{COM} \cdot \vec{M} \cdot \vec{V}^{COM} = \frac{1}{2} \begin{pmatrix} 50 & 50 \end{pmatrix} \cdot \begin{pmatrix} 4 & 0 \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 50 \\ 50 \end{pmatrix} = 6,250$$

The difference is inelastic “crunch” energy $KE - IE$ or, for elastic cases, potential energy of compression.

$$\begin{aligned} KE_{Elastic} - KE_{Inelastic} &= \frac{\vec{V}^{IN} \cdot \vec{M} \cdot \vec{V}^{IN}}{4} - \frac{\vec{V}^{FIN} \cdot \vec{M} \cdot \vec{V}^{IN}}{4} \\ 1,000 &= 3,625 - 2,625 = KE - IE \end{aligned}$$

Transpose symmetry ($M_{jk} = M_{kj}$) of the \mathbf{M} -matrix implies:

$$\begin{aligned} \vec{V}^{FIN} \cdot \vec{M} \cdot \vec{V}^{IN} &= \vec{V}^{IN} \cdot \vec{M} \cdot \vec{V}^{FIN} \\ \begin{pmatrix} 40 & 90 \end{pmatrix} \cdot \begin{pmatrix} 4 & 0 \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 60 \\ 10 \end{pmatrix} &= \begin{pmatrix} 60 & 10 \end{pmatrix} \cdot \begin{pmatrix} 4 & 0 \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 40 \\ 90 \end{pmatrix} \\ &= 100 \cdot 105 = 10,500 \end{aligned}$$

With ($M_{12} = 0 = M_{21}$) kinetic energy $KE_{Elastic} = \frac{1}{2} \vec{V} \cdot \vec{M} \cdot \vec{V}$ is the same at $\mathbf{V} = \mathbf{V}^{IN}$ and $\mathbf{V} = \mathbf{V}^{FIN}$.

$$\begin{aligned} V^{COM} P_{Total} - \frac{\vec{V}^{FIN} \cdot \vec{M} \cdot \vec{V}^{IN}}{2} &= \frac{\vec{V}^{IN} \cdot \vec{M} \cdot \vec{V}^{IN}}{2} = \frac{\vec{V}^{FIN} \cdot \vec{M} \cdot \vec{V}^{FIN}}{2} = KE_{Elastic} \\ 12,500 - \frac{10,500}{2} &= \frac{\begin{pmatrix} 60 & 10 \end{pmatrix} \cdot \begin{pmatrix} 4 & 0 \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 60 \\ 10 \end{pmatrix}}{2} = \frac{\begin{pmatrix} 40 & 90 \end{pmatrix} \cdot \begin{pmatrix} 4 & 0 \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 40 \\ 90 \end{pmatrix}}{2} = KE_{Elastic} \\ 12,500 - 5,250 &= 7,250 = 7,250 \end{aligned}$$

Consider kinetic energy $KE_{inelastic} = IE$ when $\mathbf{V} = \mathbf{V}^{COM}$. It is reduced by 1,000 from 7,250 to 6,250.

$$\begin{aligned} KE_{Inelastic} = V^{COM} P_{Total} - \frac{\vec{V}^{COM} \cdot \vec{M} \cdot \vec{V}^{COM}}{2} &= \frac{1}{2} V^{COM} P_{Total} = \frac{\vec{V}^{COM} \cdot \vec{M} \cdot \vec{V}^{COM}}{2} = \frac{\vec{V}^{IN} \cdot \vec{M} \cdot \vec{V}^{IN}}{4} + \frac{\vec{V}^{FIN} \cdot \vec{M} \cdot \vec{V}^{IN}}{4} = \frac{1}{2} KE_{Elastic} + \frac{\vec{V}^{FIN} \cdot \vec{M} \cdot \vec{V}^{IN}}{4} \\ 12,500 - \frac{12,500}{2} &= 6,250 = 6,250 = 3,625 + 2,625 = IE \end{aligned}$$

$$KE_{Inelastic} = \frac{1}{2} \vec{V}^{COM} \cdot \vec{M} \cdot \vec{V}^{COM} = \frac{1}{2} \begin{pmatrix} 50 & 50 \end{pmatrix} \cdot \begin{pmatrix} 4 & 0 \\ 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 50 \\ 50 \end{pmatrix} = 6,250$$

The difference is inelastic “crunch” energy $KE - IE$ or, for elastic cases, potential energy of compression.

$$\begin{aligned} KE_{Elastic} - KE_{Inelastic} &= \frac{\vec{V}^{IN} \cdot \vec{M} \cdot \vec{V}^{IN}}{4} - \frac{\vec{V}^{FIN} \cdot \vec{M} \cdot \vec{V}^{IN}}{4} \\ 1,000 &= 3,625 - 2,625 = KE - IE \end{aligned}$$

This difference is the same in all reference frames including COM frame where $KE_{inelastic} = IE$ is zero.

Note “crunch” energy $Elastic KE - inelastic IE = 0.21$ is the same in all frames including COM-frame.

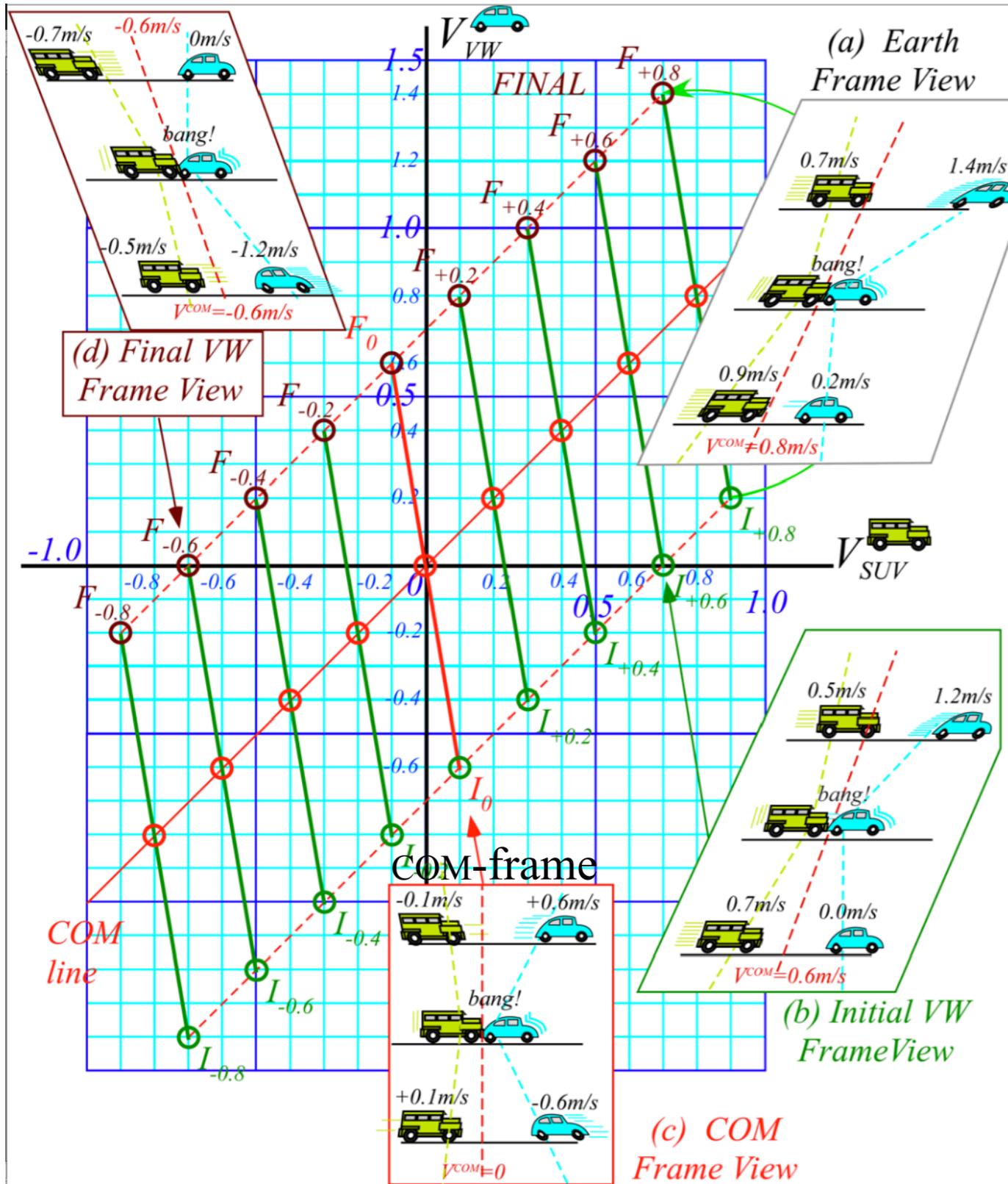


Fig. 3.4 Galilean Frame Views of collision like Fig. 2.5 or Fig. 3.1 with Bush (6:1) SUV.
 (a) Earth frame view (b) Initial VW frame (VW initially fixed)
 (c) COM frame view (d) Final VW frame (VW ends up fixed)

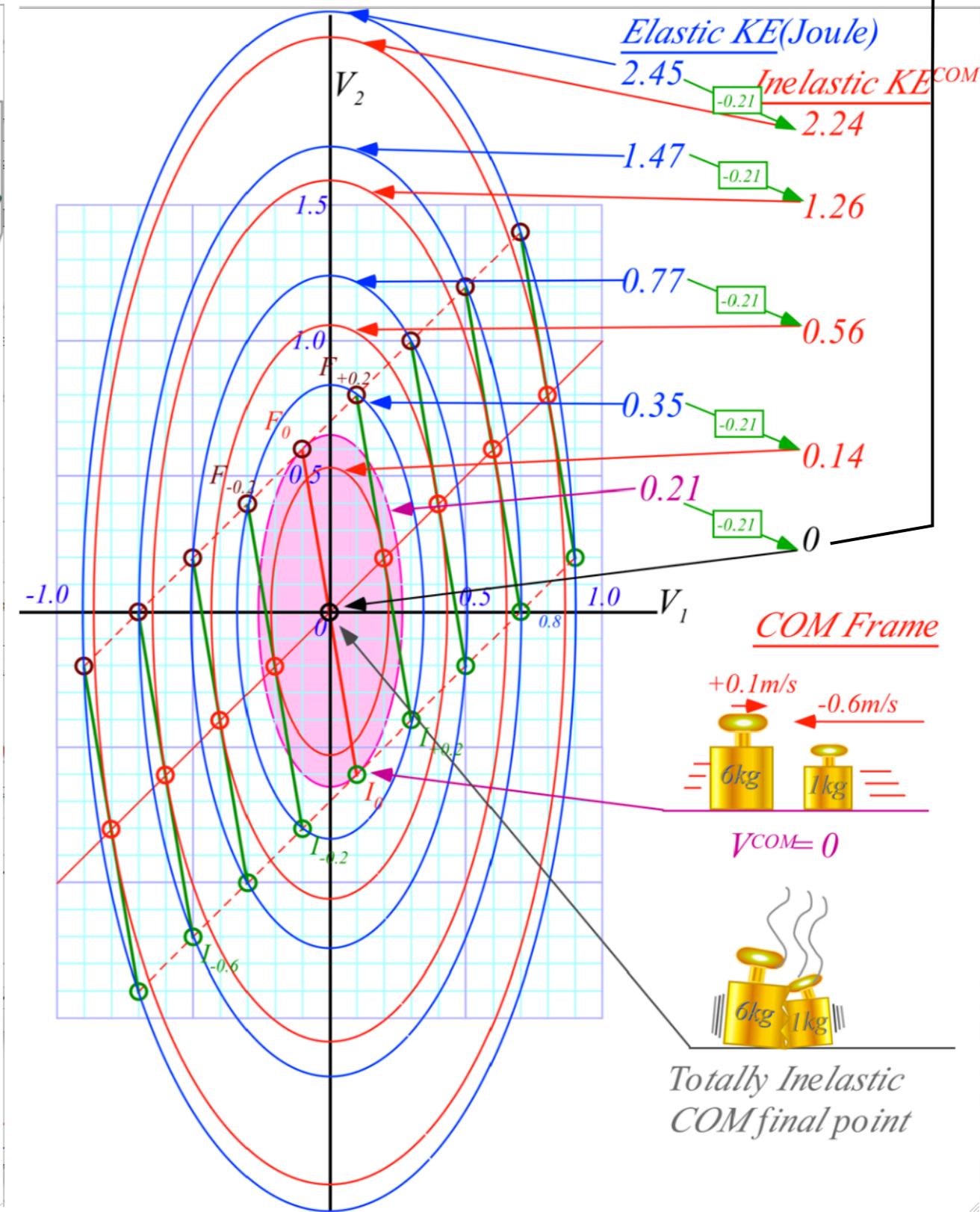


Fig. 3.5 Momentum ($P=const.$)-lines and energy ($KE=const.$)-ellipses appropriate for Fig. 3.4.