

Electromagnetic Lagrangian and charge-field mechanics (Ch. 2.8 of Unit 2)

Charge mechanics in electromagnetic fields

Vector analysis for particle-in- (A, Φ) -potential

Lagrangian for particle-in- (A, Φ) -potential

Hamiltonian for particle-in- (A, Φ) -potential

Canonical momentum in (A, Φ) potential

Hamiltonian formulation

Hamilton's equations

Crossed E and B field mechanics

Classical Hall-effect and cyclotron orbit orbit equations

Vector theory vs. complex variable theory

Mechanical analog of cyclotron and FBI rule

Cycloidal ruler&compass geometry

Cycloidal geometry of flying levers

Practical poolhall application



This mechanical analog of (E_x, B_z) field mimics \mathbf{A} -field with tabletop v-field

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- *Vector analysis for particle-in- (A, Φ) -potential*
- Lagrangian for particle-in- (A, Φ) -potential*
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Vector analysis for particle-in-(A,Φ)-potential

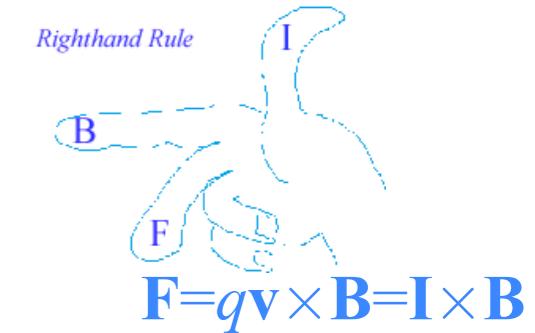
So-called *pondermotive* form for Newton's $F=ma$ equation for a mass m of charge e .

$$m \frac{d\mathbf{v}}{dt} = \mathbf{F} = e(\mathbf{E} + \mathbf{v} \times \mathbf{B})$$

Electric field \mathbf{E} and magnetic field \mathbf{B}
scalar potential field $\Phi = \Phi(\mathbf{r}, t)$
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electronic charge:
 $e = -1.602176 \cdot 10^{-19}$ Coulombs

$$\mathbf{E} = -\nabla\Phi - \frac{\partial\mathbf{A}}{\partial t}$$
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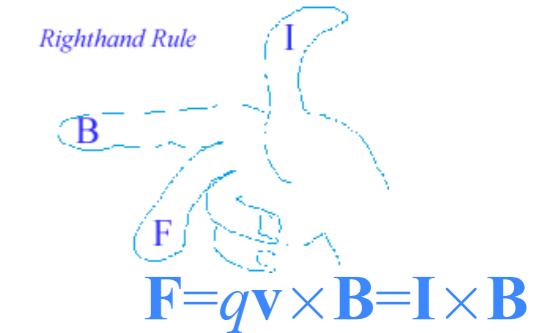
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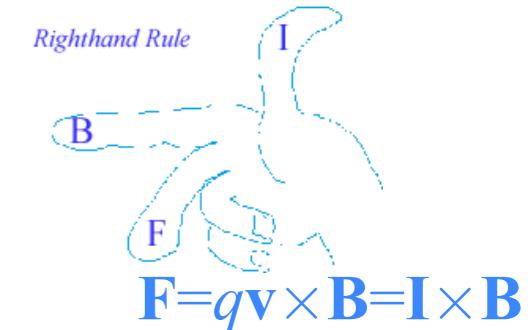
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$$\varepsilon_{ijk}\text{-Tensor analysis of } \mathbf{v} \times (\nabla \times \mathbf{A}) \quad [\mathbf{v} \times (\nabla \times \mathbf{A})]_k = \varepsilon_{kij} v_i (\nabla \times \mathbf{A})_j$$



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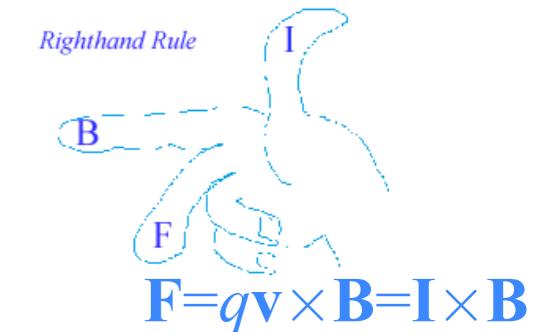
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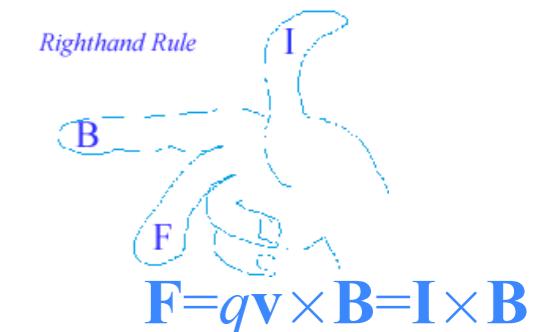
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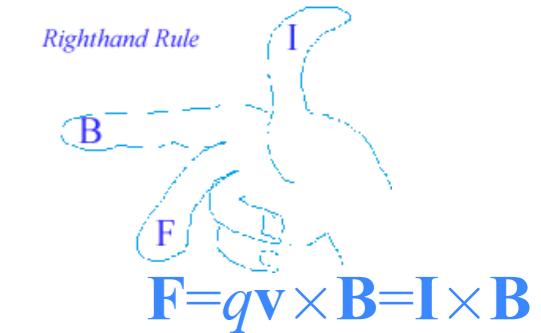
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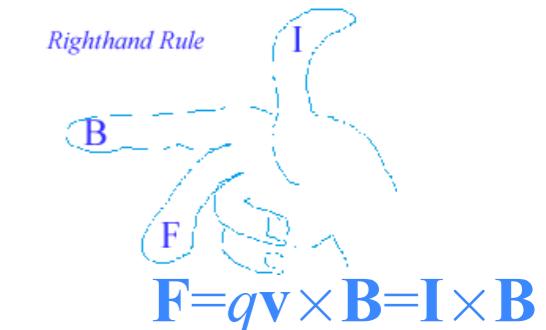
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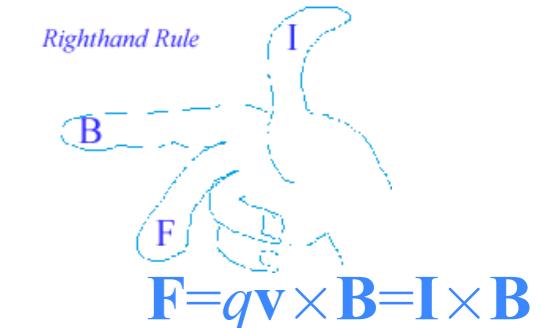
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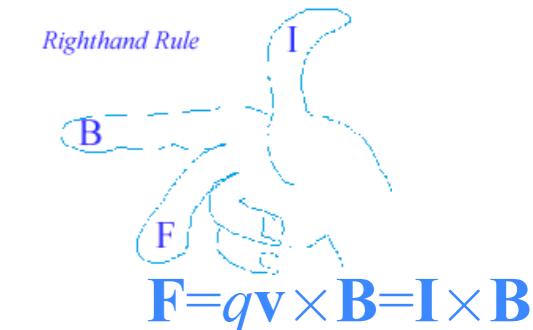
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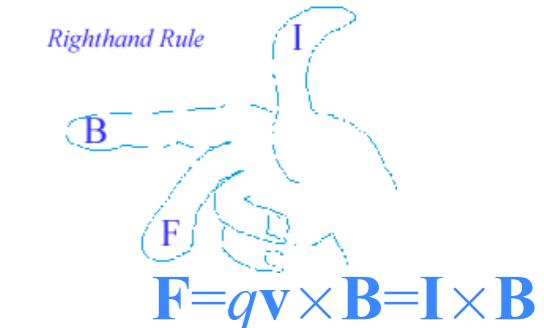
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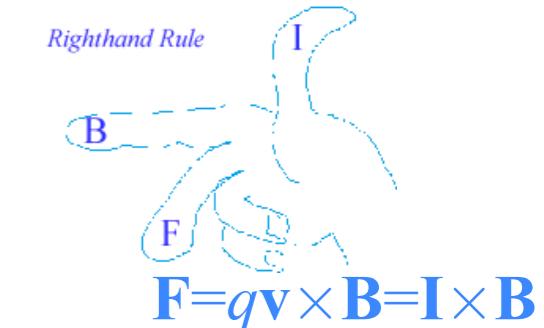
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Newtonian mechanics has *no explicit dependence* of position \mathbf{r} and velocity \mathbf{v} .

\mathbf{r} -partial derivative of \mathbf{v} (or vice-versa) is **identically zero**.

$$\partial_k v^j \equiv 0 \text{ iff : } \nabla \mathbf{v} = \frac{\partial \mathbf{v}}{\partial \mathbf{r}} = \mathbf{0}$$

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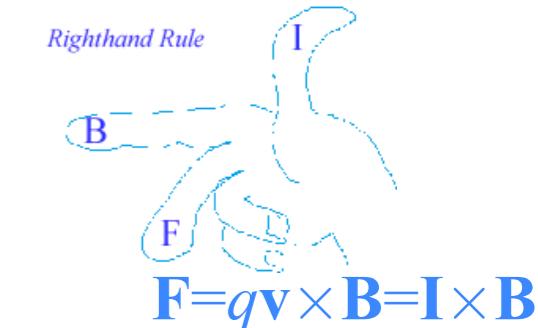
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$$\begin{aligned} &= \epsilon_{kij} v_i (\epsilon_{abj} (\partial_a A_b)) \\ &= \epsilon_{kij} \epsilon_{abj} v_i (\partial_a A_b) \\ &= (\delta_{ka} \delta_{ib} - \delta_{kb} \delta_{ia}) v_i (\partial_a A_b) \\ &= \delta_{ka} \delta_{ib} v_i (\partial_a A_b) - \delta_{kb} \delta_{ia} v_i (\partial_a A_b) \\ &= v_b (\partial_k A_b) - v_a (\partial_a A_k) \\ &= (\partial_k A_b) v_b - v_a (\partial_a A_k) = (\nabla \mathbf{A}) \cdot \mathbf{v} - \mathbf{v} \cdot \nabla \mathbf{A} \\ &= \partial_k (A_b v_b) - (\partial_k v_b) A_b - v_a (\partial_a A_k) = \nabla(\mathbf{A} \cdot \mathbf{v}) - (\nabla \mathbf{v}) \cdot \mathbf{A} - \mathbf{v} \cdot \nabla \mathbf{A} \end{aligned}$$



Applying Levi-Civita ϵ -identity:

$$\epsilon_{kij} \epsilon_{abj} = \delta_{ka} \delta_{ib} - \delta_{kb} \delta_{ia}$$

Converting back to Gibbs's **bold** notation involves *tensors* like $\nabla \mathbf{A}$ and $\nabla \mathbf{v}$.

Newtonian mechanics has *no explicit dependence* of position \mathbf{r} and velocity \mathbf{v} .

\mathbf{r} -partial derivative of \mathbf{v} (or vice-versa) is **identically zero**.

$$\partial_k v^j \equiv 0 \text{ iff : } \nabla \mathbf{v} = \frac{\partial \mathbf{v}}{\partial \mathbf{r}} = \mathbf{0}$$

$$\mathbf{v} \times (\nabla \times \mathbf{A}) = \nabla(\mathbf{A} \cdot \mathbf{v}) - 0 - \mathbf{v} \cdot \nabla \mathbf{A} \quad \text{for particle mechanics}$$

Summary of Vector analysis for particle-in-(A,Φ)-potential

Tensor index notation helps to distinguish $(\nabla \mathbf{A}) \cdot \mathbf{v}$, $\mathbf{v} \cdot (\nabla \mathbf{A})$, and $\nabla(\mathbf{A} \cdot \mathbf{v}) = (\nabla \mathbf{A}) \cdot \mathbf{v} + (\nabla \mathbf{v}) \cdot \mathbf{A}$.

$$[(\nabla \mathbf{A}) \cdot \mathbf{v}]_k = \frac{\partial A_j}{\partial x_k} v_j \\ = (\partial_k A_j) v_j$$

$$[\mathbf{v} \cdot (\nabla \mathbf{A})]_k = v_j \frac{\partial A_k}{\partial x_j} \\ = (v_j \partial_j A_k)$$

$$[\nabla(\mathbf{A} \cdot \mathbf{v})]_k = [(\nabla \mathbf{A}) \cdot \mathbf{v} + (\nabla \mathbf{v}) \cdot \mathbf{A}]_k \\ \partial_k (A_b v_b) = (\partial_k v_b) A_b - (\partial_k A_b) v_b$$

$$\mathbf{v} \times (\nabla \times \mathbf{A}) = \nabla(\mathbf{A} \cdot \mathbf{v}) - 0 - \mathbf{v} \cdot \nabla \mathbf{A} \quad \text{for particle mechanics}$$

Charge mechanics in electromagnetic fields

Vector analysis for particle-in- (A, Φ) -potential

→ *Lagrangian for particle-in- (A, Φ) -potential*

Hamiltonian for particle-in- (A, Φ) -potential

Canonical momentum in (A, Φ) potential

Hamiltonian formulation

Hamilton's equations

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electronic charge:
 $e = -1.602176 \cdot 10^{-19}$ Coulombs

$$m \frac{d\mathbf{v}}{dt} = \mathbf{F} = e(\mathbf{E} + \mathbf{v} \times \mathbf{B})$$

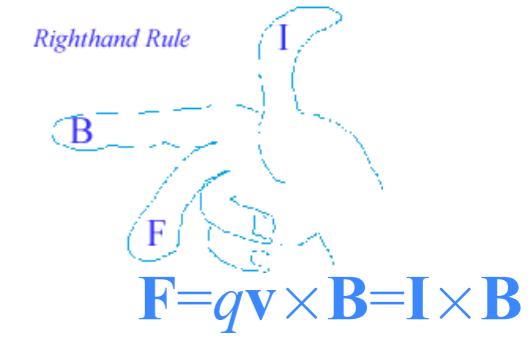
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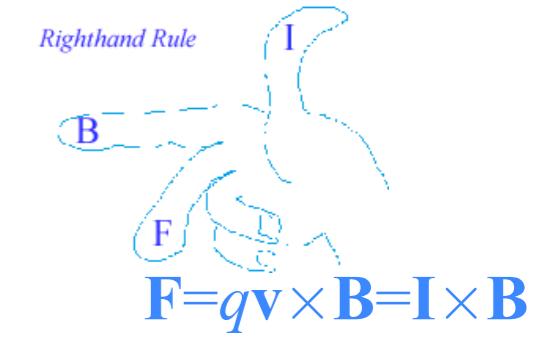
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Chain rule expansion of vector potential total t -derivative: $\frac{d\mathbf{A}}{dt} = \frac{\partial\mathbf{A}}{\partial x} \dot{x} + \frac{\partial\mathbf{A}}{\partial y} \dot{y} + \frac{\partial\mathbf{A}}{\partial z} \dot{z} + \frac{\partial\mathbf{A}}{\partial t} = \boxed{\frac{\partial\mathbf{A}}{\partial t}} + \boxed{(\mathbf{v} \bullet \nabla)\mathbf{A}}$

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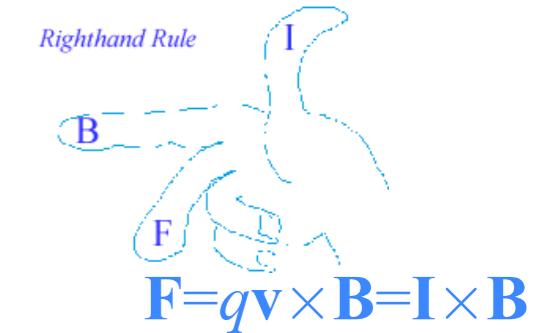
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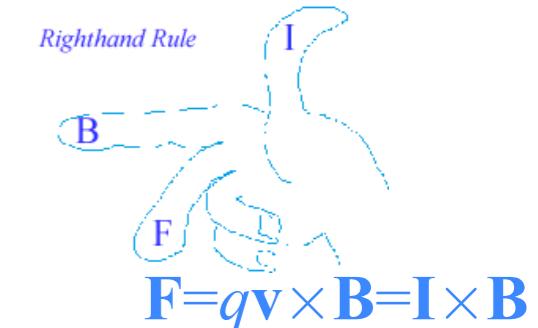
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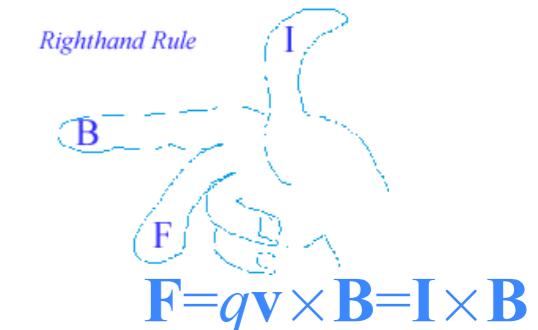
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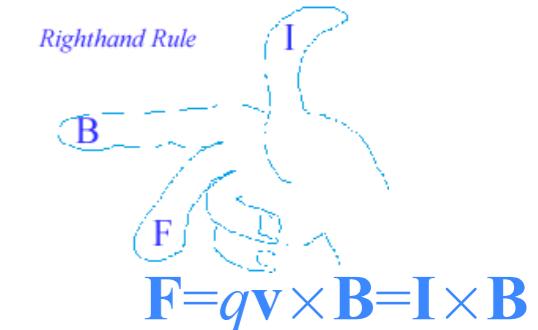
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Inserting Φ -term that $\partial_{\mathbf{v}}$ zeros :

This step requires that : $\frac{\partial}{\partial \mathbf{v}}(e\Phi) = 0$ *(and : $\frac{\partial}{\partial \mathbf{v}}(\mathbf{v} \cdot e\mathbf{A}) = e\mathbf{A}$)*

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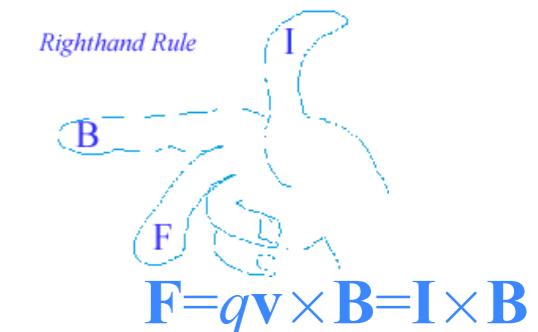
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This step requires that:

$$\nabla \left(\frac{1}{2} m \mathbf{v} \cdot \mathbf{v} \right) \equiv \frac{\partial}{\partial \mathbf{r}} \left(\frac{1}{2} m \mathbf{v} \cdot \mathbf{v} \right) = 0$$

Inserting $\mathbf{v} \cdot \mathbf{v}$ -term that $\partial_{\mathbf{r}}$ zeros :

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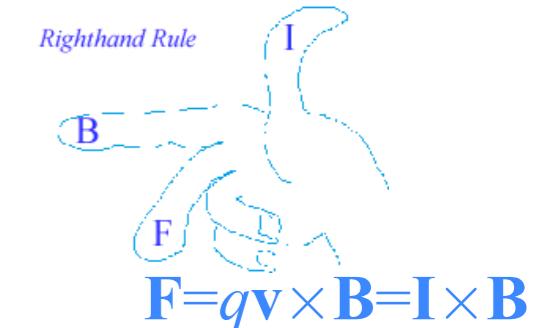
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$$\frac{\partial}{\partial \mathbf{r}} \left(\frac{1}{2} m \mathbf{v} \cdot \mathbf{v} \right) = 0$$

$$\frac{d}{dt} \frac{\partial L}{\partial \mathbf{v}} = \frac{\partial L}{\partial \mathbf{r}}$$

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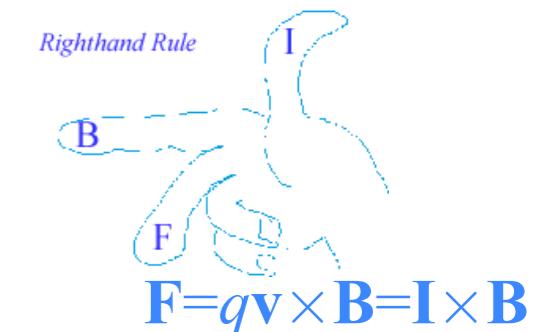
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$$\frac{\partial}{\partial \mathbf{r}} \left(\frac{1}{2} m \mathbf{v} \cdot \mathbf{v} \right) = 0$$

$$\frac{d}{dt} \frac{\partial L}{\partial \mathbf{v}} = \frac{\partial L}{\partial \mathbf{r}}$$

Lagrangian has a *linear* velocity term $e\mathbf{v} \cdot \mathbf{A}$ in addition to the usual quadratic $KE = m\mathbf{v}^2/2$ and $PE = e\Phi$.

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Charge mechanics in electromagnetic fields

Vector analysis for particle-in- (A, Φ) -potential

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Canonical momentum in (A, Φ) potential

Canonical momentum is defined by L 's \mathbf{v} -derivative

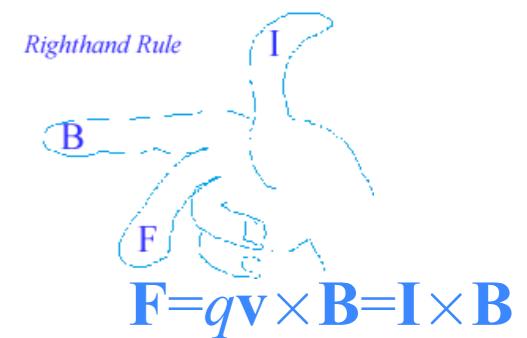
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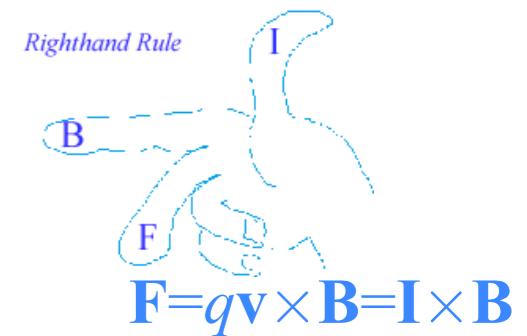
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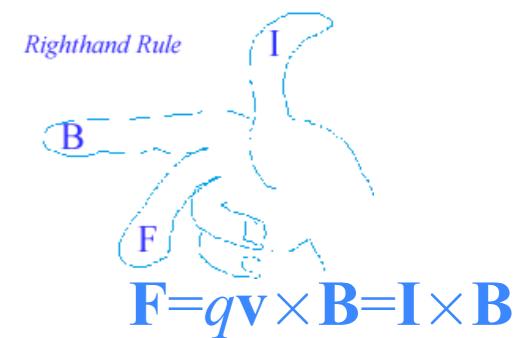
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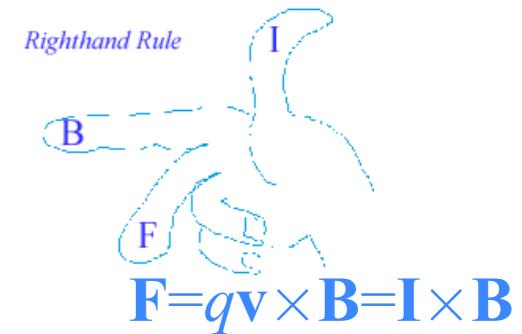
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Otherwise vector potential term $-\mathbf{v} \cdot e\mathbf{A}$ leads to an extraordinary *canonical momentum*: $\mathbf{p} = m\mathbf{v} + e\mathbf{A}(\mathbf{r}, t)$.
Particle momentum $m\mathbf{v}$ is not canonical, but related to *canonical* \mathbf{p} as follows: $m\mathbf{v} = \mathbf{p} - e\mathbf{A}(\mathbf{r}, t)$

Charge mechanics in electromagnetic fields

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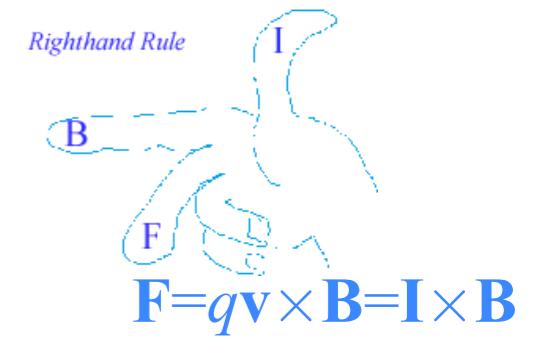
→ *Hamiltonian formulation*

Hamilton's equations

Hamiltonian for charged particle in fields

The Hamiltonian function of the Legendre-Poincare form is the following.

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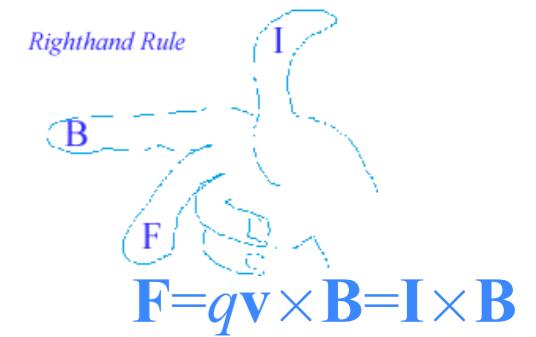


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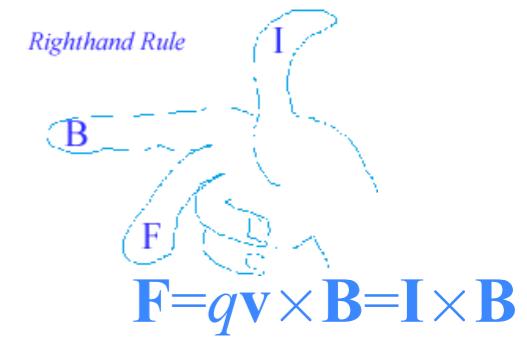


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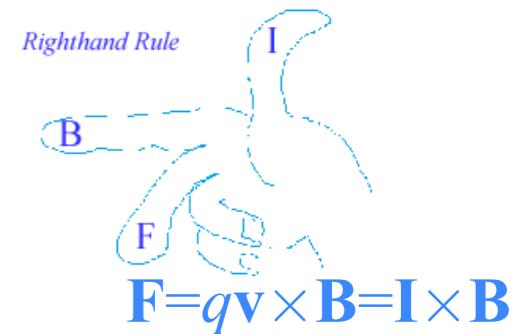
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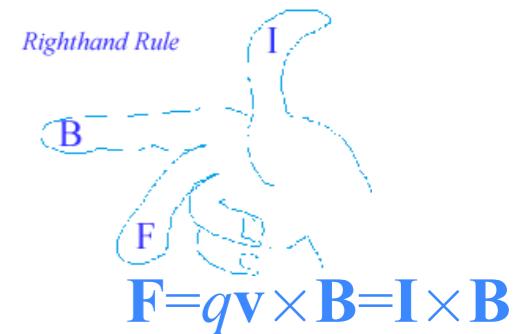
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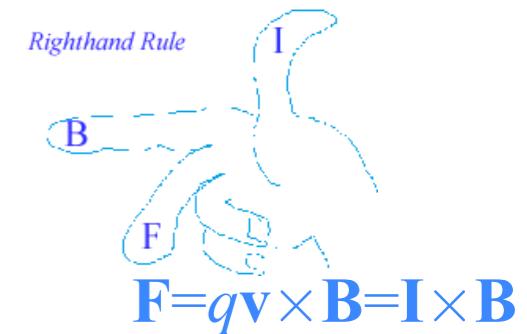
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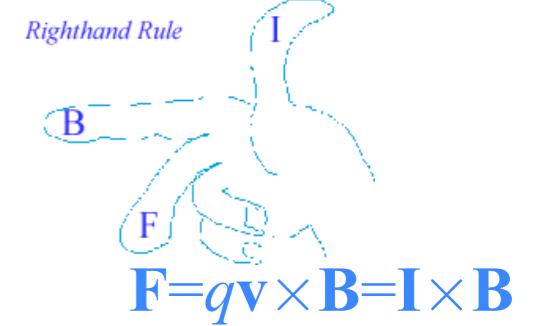


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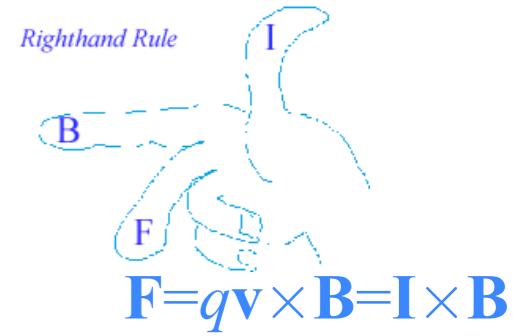
→ *Hamilton's equations*

Hamilton's equations for charged particle in fields

Hamiltonian is explicit function of **momentum p**. Must replace velocity **v** using $m\mathbf{v}=\mathbf{p} - e\mathbf{A}(\mathbf{r},t)$.

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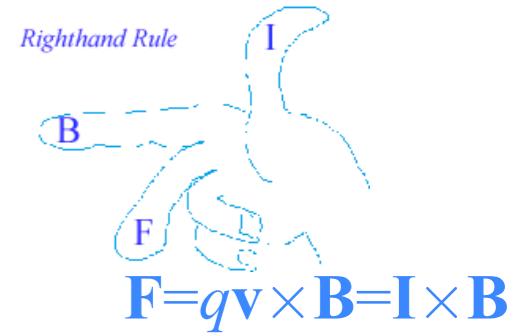
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$$\begin{aligned} \mathbf{E} &= -\nabla\Phi - \frac{\partial \mathbf{A}}{\partial t} \\ E_a &= -\frac{\partial \Phi}{\partial x^a} - \frac{\partial A_a}{\partial t} \\ -\frac{\partial \Phi}{\partial x^a} &= \frac{\partial A_a}{\partial t} + E_a \end{aligned}$$

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$$\dot{p}_a = m\dot{v}_a + e\dot{A}_a = + \underbrace{\frac{(p_\mu - eA_\mu)}{m}}_{m} e \frac{\partial A_\mu}{\partial x_a} - e \frac{\partial \Phi}{\partial x_a}$$

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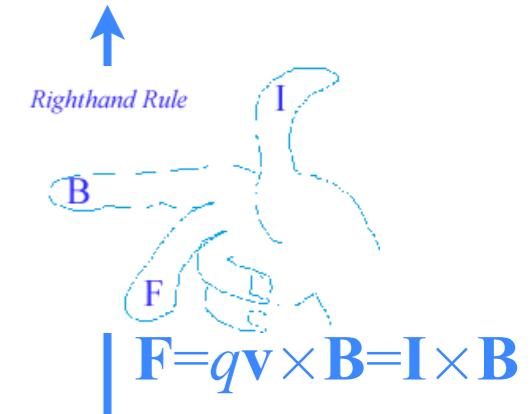
...and now

*we come back
full circle...*

$$m\dot{v}_a = e \left(v_\mu \frac{\partial A_\mu}{\partial x_a} - v_\mu \frac{\partial A_a}{\partial x_\mu} + E_a \right)$$

$$m\dot{\mathbf{v}} = e \left(\mathbf{v} \times (\nabla \times \mathbf{A}) + \mathbf{E} \right) = e(\mathbf{v} \times \mathbf{B} + \mathbf{E})$$

$$\mathbf{v} \times (\nabla \times \mathbf{A}) = \mathbf{v} \cdot (\nabla \mathbf{A}) - (\mathbf{v} \cdot \nabla) \mathbf{A} \quad \text{for particle mechanics}$$



$$\mathbf{E} = -\nabla\Phi - \frac{\partial \mathbf{A}}{\partial t}$$

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Crossed E and B field mechanics

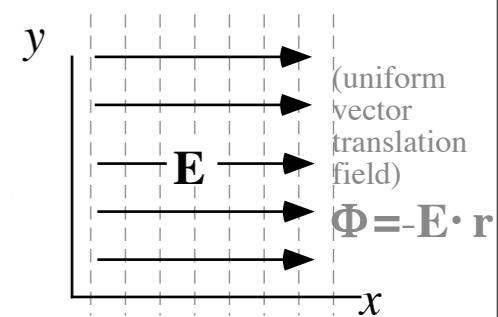
- *Classical Hall-effect and cyclotron orbit orbit equations*
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Crossed E and B field mechanics

A constant **E** field has a scalar potential field Φ with constant gradient.

$$\Phi(\mathbf{r}) = -\mathbf{E} \bullet \mathbf{r}, \quad -\nabla\Phi(\mathbf{r}) = \nabla(-\mathbf{E} \bullet \mathbf{r}) = \mathbf{E} = \text{const.}$$

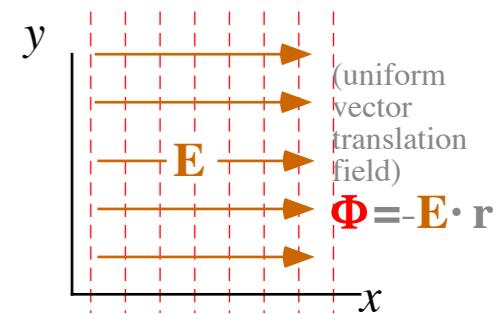
Fig. 2.4.1.



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A constant **B** field has a vector potential field \mathbf{A} that resembles a disc spinning counter-clockwise around the **B** axis.

$$\mathbf{A}(\mathbf{r}) = \frac{1}{2}\mathbf{B} \times \mathbf{r}, \quad \nabla \times \mathbf{A}(\mathbf{r}) = \nabla \times \left(\frac{1}{2}\mathbf{B} \times \mathbf{r} \right) = \mathbf{B} = \text{const.}$$

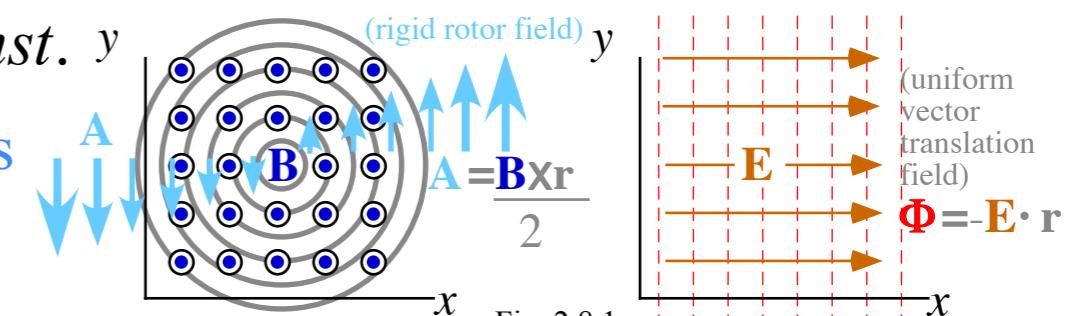


Fig. 2.8.1.

This mechanical analog of (E_x, B_z) field mimics \mathbf{A} -field with tabletop v-field



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Newtonian electromagnetic equations of motion: $m\ddot{\mathbf{v}} = e(\mathbf{E} + \mathbf{v} \times \mathbf{B})$

$$\ddot{\mathbf{v}} = \frac{e}{m}\mathbf{E} + \mathbf{v} \times \frac{e}{m}\mathbf{B}.$$

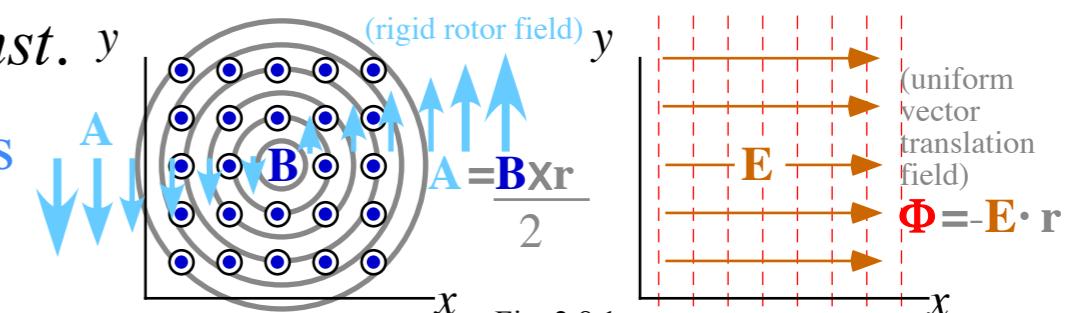
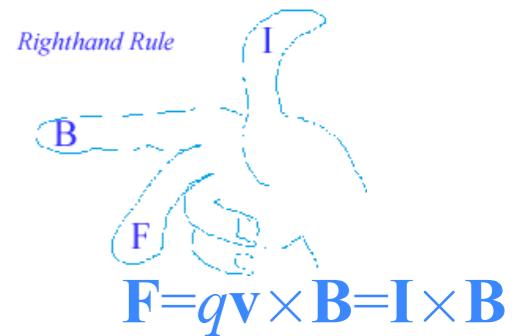


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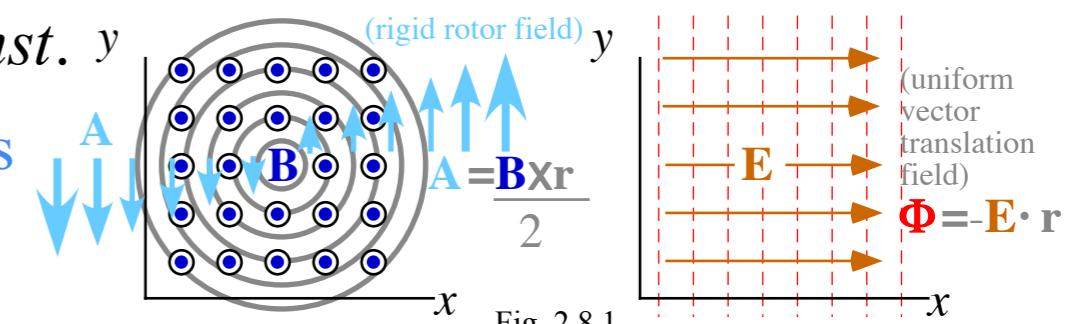


Fig. 2.8.1.

$$\dot{\mathbf{v}} = \frac{e}{m} \mathbf{E} + \mathbf{v} \times \frac{e}{m} \mathbf{B} = \boldsymbol{\varepsilon} + \mathbf{v} \times \frac{e}{m} B \hat{\mathbf{e}}_z$$

$$\boldsymbol{\varepsilon}_x = \frac{e}{m} E_x \quad \boldsymbol{\varepsilon}_y = \frac{e}{m} E_y \quad B = \frac{e}{m} B_z$$

Shorthand Labeling

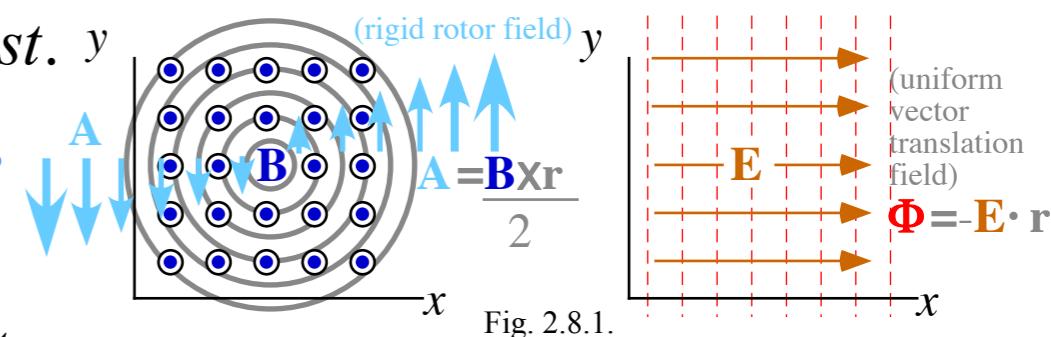
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Shorthand Labeling

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Classical Hall-effect and cyclotron orbit equations

→ *Vector theory vs. complex variable theory*

Mechanical analog of cyclotron and FBI rule

Cycloid geometry and flying sticks

Practical poolhall application

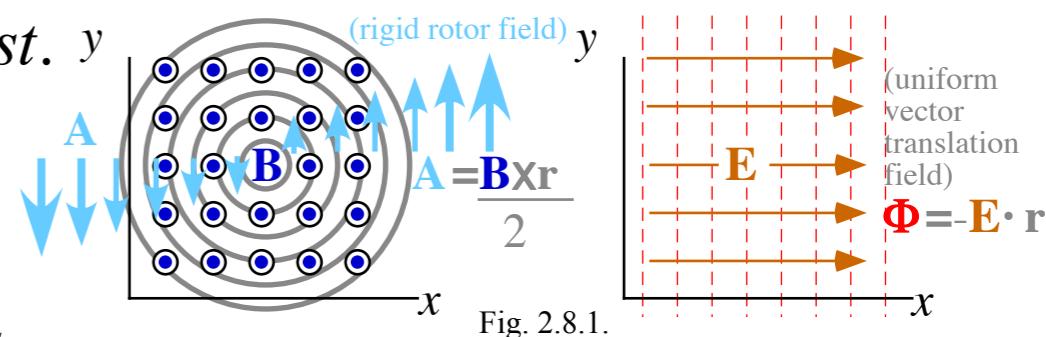
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Shorthand Labeling

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Complex variable velocity: $v = v_x + i v_y$ and electric field: $\boldsymbol{\varepsilon} = \varepsilon_x + i \varepsilon_y$

$$\dot{v}_x + i \dot{v}_y = \varepsilon_x + i \varepsilon_y - i B v_x + B v_y = \varepsilon_x + i \varepsilon_y - i B(v_x + i v_y)$$

$$\dot{v} = \boldsymbol{\varepsilon} - i B v \quad \text{with replacements: } \hat{\mathbf{e}}_x \rightarrow 1 \quad \text{and: } \hat{\mathbf{e}}_y \rightarrow i = \sqrt{-1}$$

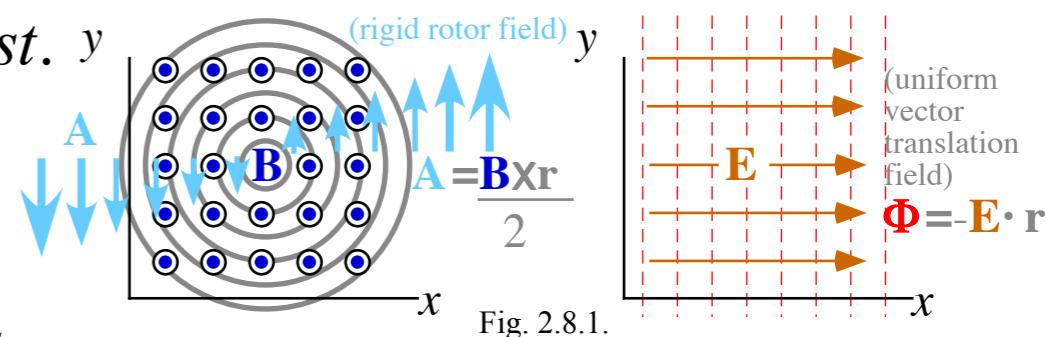
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$$\begin{aligned}\dot{\mathbf{v}} &= \frac{e}{m} \mathbf{E} + \mathbf{v} \times \frac{e}{m} \mathbf{B} = \boldsymbol{\varepsilon} + \mathbf{v} \times \frac{e}{m} \mathbf{B} \hat{\mathbf{e}}_z \\ \varepsilon_x &= \frac{e}{m} E_x \quad \varepsilon_y = \frac{e}{m} E_y \quad B = \frac{e}{m} B_z\end{aligned}$$

Shorthand Labeling

$$\text{where: } \hat{\mathbf{e}}_x \times \hat{\mathbf{e}}_z = -\hat{\mathbf{e}}_x \quad \text{and: } \hat{\mathbf{e}}_y \times \hat{\mathbf{e}}_z = \hat{\mathbf{e}}_x$$

Complex variable velocity: $v = v_x + i v_y$ and electric field: $\boldsymbol{\varepsilon} = \varepsilon_x + i \varepsilon_y$

$$\begin{aligned}\dot{v}_x + i \dot{v}_y &= \varepsilon_x + i \varepsilon_y - i B v_x + B v_y = \varepsilon_x + i \varepsilon_y - i B(v_x + i v_y) \\ \dot{v} &= \boldsymbol{\varepsilon} - i B v \quad \text{with replacements: } \hat{\mathbf{e}}_x \rightarrow 1 \quad \text{and: } \hat{\mathbf{e}}_y \rightarrow i = \sqrt{-1}\end{aligned}$$

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$$\dot{V}(t) = \dot{v}(t) + \dot{\beta} = \boldsymbol{\varepsilon} - i B v = \boldsymbol{\varepsilon} - i B(V(t) - \beta) = -i B V(t)$$

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Crossed E and B field mechanics

A constant **E** field has a scalar potential field Φ with constant gradient.

$$\Phi(\mathbf{r}) = -\mathbf{E} \bullet \mathbf{r}, \quad -\nabla \Phi(\mathbf{r}) = -\nabla(-\mathbf{E} \bullet \mathbf{r}) = \mathbf{E} = \text{const.}$$

A constant **B** field has a vector potential field \mathbf{A} that resembles a disc spinning counter-clockwise around the **B** axis.

$$\mathbf{A}(\mathbf{r}) = \frac{1}{2} \mathbf{B} \times \mathbf{r}, \quad \nabla \times \mathbf{A}(\mathbf{r}) = \nabla \times \left(\frac{1}{2} \mathbf{B} \times \mathbf{r} \right) = \mathbf{B} = \text{const.}$$

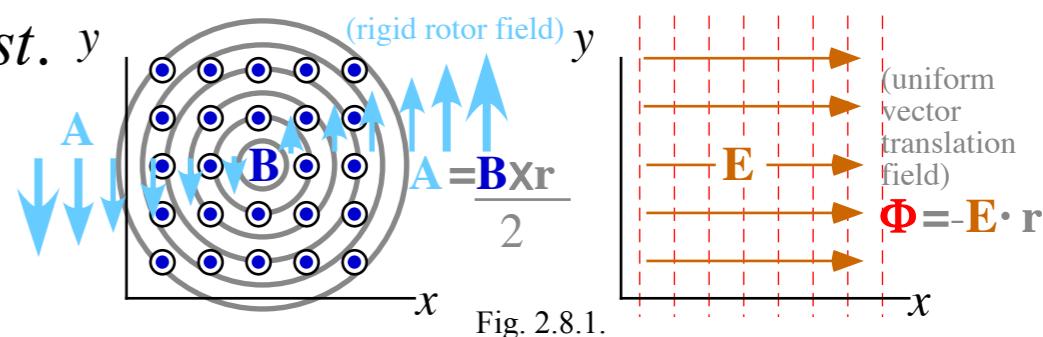


Fig. 2.8.1.

Newtonian electromagnetic equations of motion: $m\dot{\mathbf{v}} = e(\mathbf{E} + \mathbf{v} \times \mathbf{B})$

Gibb's notation:

$$\begin{aligned}\dot{\mathbf{v}} &= \boldsymbol{\varepsilon} + \mathbf{v} \times B \hat{\mathbf{e}}_z \\ \dot{v}_x \hat{\mathbf{e}}_x + \dot{v}_y \hat{\mathbf{e}}_y &= \varepsilon_x \hat{\mathbf{e}}_x + \varepsilon_y \hat{\mathbf{e}}_y + (v_x \hat{\mathbf{e}}_x + v_y \hat{\mathbf{e}}_y) \times B \hat{\mathbf{e}}_z \\ &= \varepsilon_x \hat{\mathbf{e}}_x + \varepsilon_y \hat{\mathbf{e}}_y - B v_x \hat{\mathbf{e}}_y + B v_y \hat{\mathbf{e}}_x\end{aligned}$$

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where: $\hat{\mathbf{e}}_x \times \hat{\mathbf{e}}_z = -\hat{\mathbf{e}}_x$ and: $\hat{\mathbf{e}}_y \times \hat{\mathbf{e}}_z = \hat{\mathbf{e}}_x$

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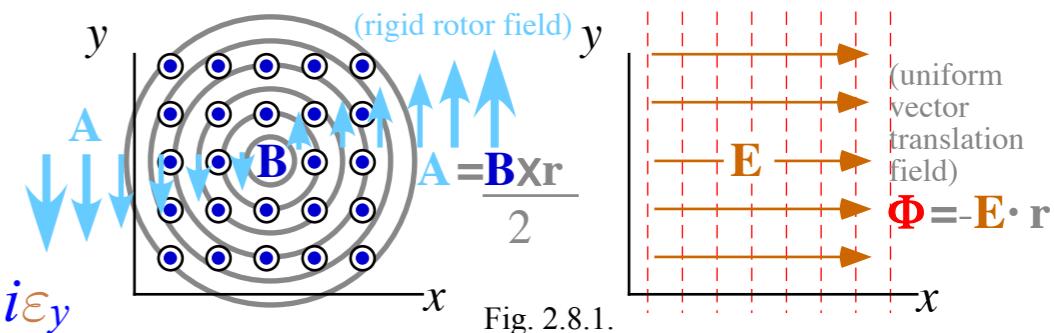
Move last part of this calculation UP↑

Crossed E and B field mechanics (Solution by complex variables)

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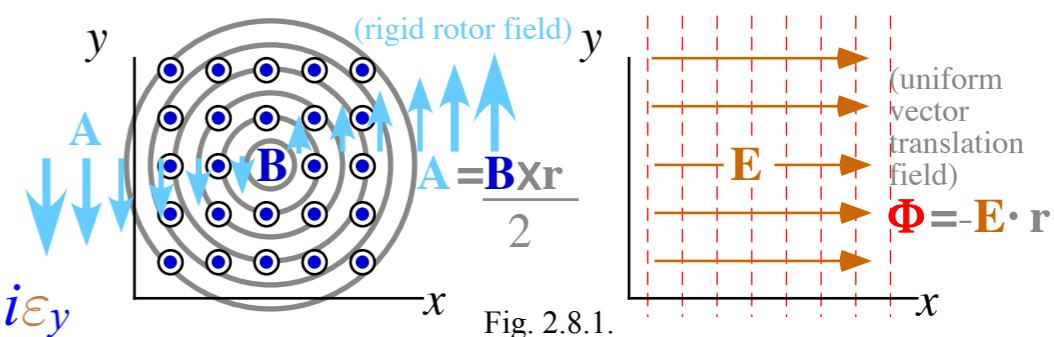
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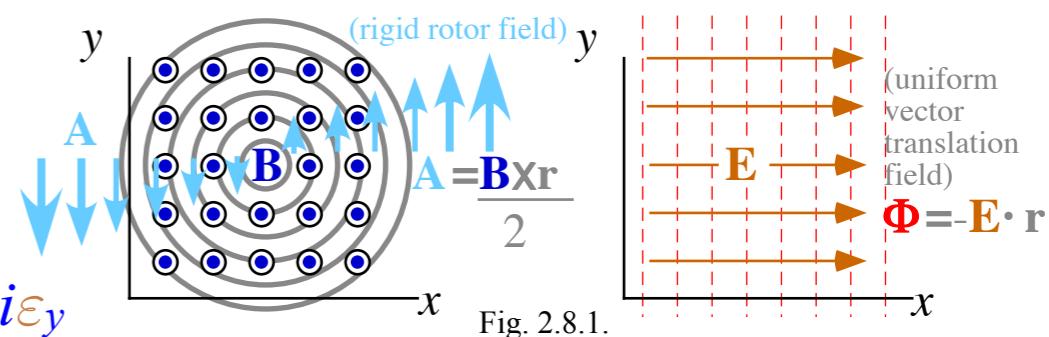
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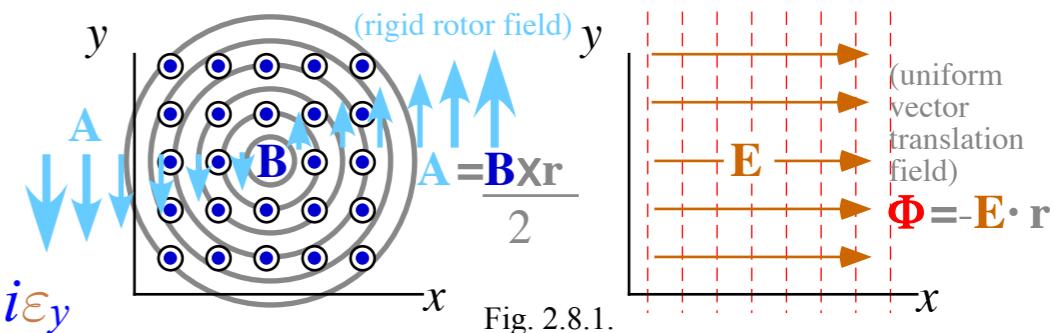
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complex form

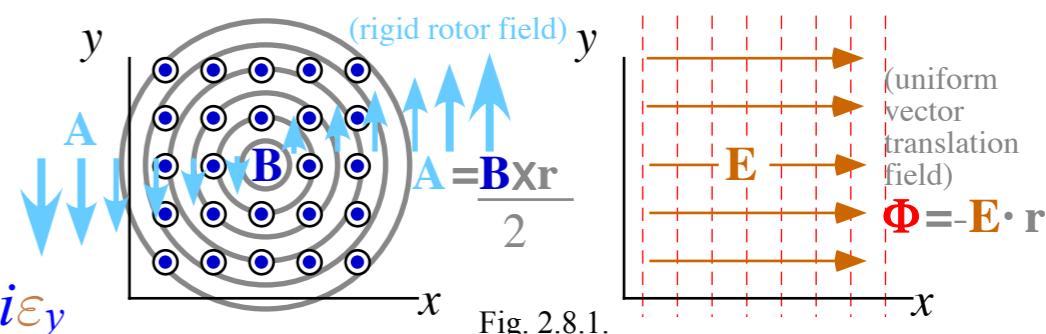
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Crossed E and B field mechanics (Solution by complex variables)

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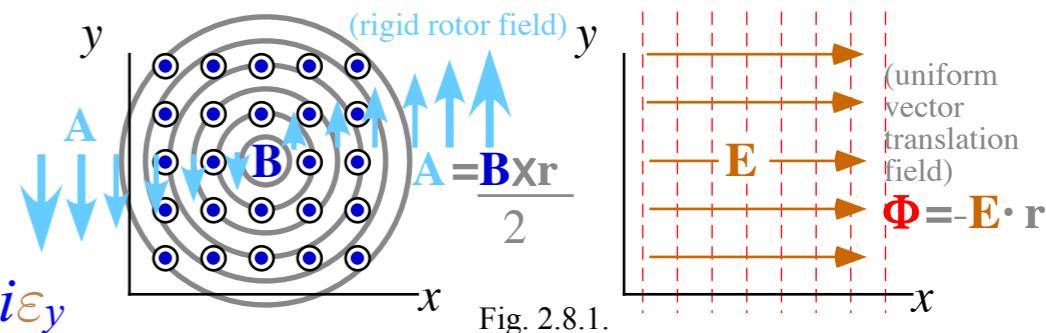
vector form

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vector form

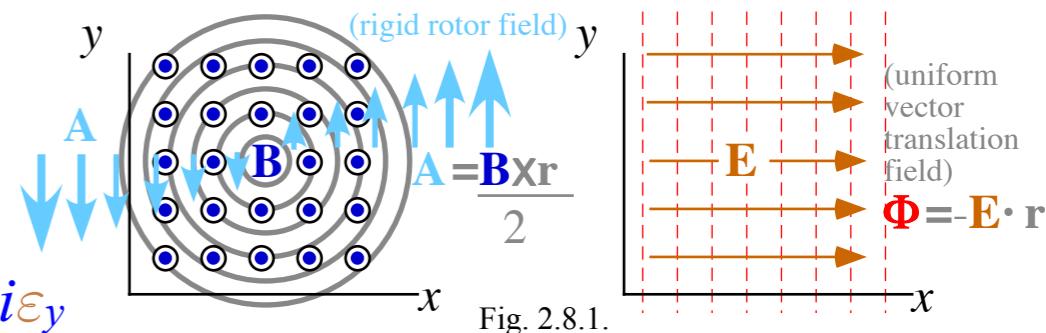
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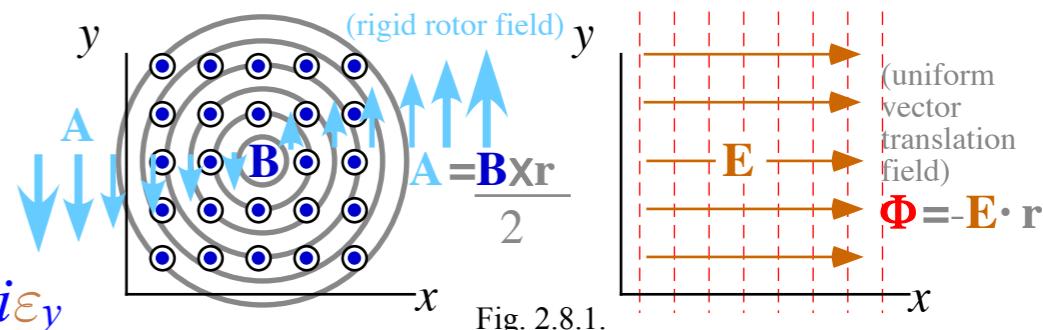
$$q(t) = \int v(t) dt = \frac{e^{-iBt}}{-iB} (v(0) + i\frac{\boldsymbol{\varepsilon}}{B}) - i\frac{\boldsymbol{\varepsilon}}{B} \cdot t + \text{Const.} \quad \text{where: } \text{Const.} = q(0) - \left(\frac{v(0)}{-iB} - \frac{\boldsymbol{\varepsilon}}{B^2} \right) \quad \text{complex form}$$

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$$q(t) = \int v(t) dt = \frac{e^{-iBt}}{-iB} (v(0) + i\frac{\boldsymbol{\varepsilon}}{B}) - i\frac{\boldsymbol{\varepsilon}}{B} \cdot t + \text{Const.} \quad \text{where: } \text{Const.} = q(0) - \left(\frac{v(0)}{-iB} - \frac{\boldsymbol{\varepsilon}}{B^2} \right) \quad \text{complex form}$$

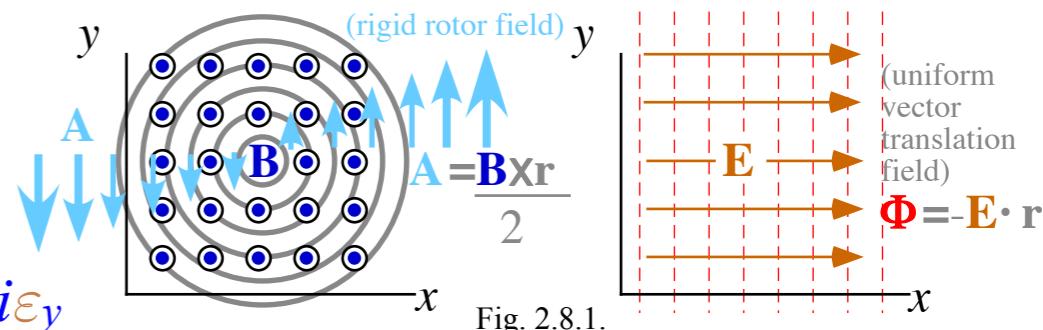
$$x(t) + iy(t) = e^{-iBt} \left(i \frac{v(0)}{B} - \frac{\boldsymbol{\varepsilon}}{B^2} \right) - i \frac{\boldsymbol{\varepsilon}}{B} \cdot t + x(0) + iy(0) - i \frac{v(0)}{B} + \frac{\boldsymbol{\varepsilon}}{B^2}$$

Crossed E and B field mechanics (Solution by complex variables)

$$\dot{\mathbf{v}} = \frac{e}{m} \mathbf{E} + \mathbf{v} \times \frac{e}{m} \mathbf{B} = \boldsymbol{\varepsilon} + \mathbf{v} \times \frac{e}{m} B \hat{\mathbf{e}}_z$$

$$\boldsymbol{\varepsilon}_x = \frac{e}{m} E_x \quad \boldsymbol{\varepsilon}_y = \frac{e}{m} E_y \quad B = \frac{e}{m} B_z$$

Shorthand Labeling



Complex variable velocity: $v = v_x + i v_y$ and electric field: $\boldsymbol{\varepsilon} = \boldsymbol{\varepsilon}_x + i \boldsymbol{\varepsilon}_y$

$$\dot{v}_x + i \dot{v}_y = \boldsymbol{\varepsilon}_x + i \boldsymbol{\varepsilon}_y - iBv_x + Bv_y = \boldsymbol{\varepsilon}_x + i \boldsymbol{\varepsilon}_y - iB(v_x + i v_y)$$

$$\dot{v} = \boldsymbol{\varepsilon} - iBv \quad \text{with replacements: } \hat{\mathbf{e}}_x \rightarrow 1 \quad \text{and: } \hat{\mathbf{e}}_y \rightarrow i = \sqrt{-1}$$

A velocity transformation $V(t) = v(t) + \beta$ cancels constant $\boldsymbol{\varepsilon}$ -field to give an equation: $\dot{V} = (\text{const.})V$

$$\boxed{\dot{V}(t) = \dot{v}(t) + \dot{\beta} = \boldsymbol{\varepsilon} - iBv = \boldsymbol{\varepsilon} - iB(V(t) - \beta) = -iBV(t)}$$

$$\text{where: } \boxed{\beta = -\frac{\boldsymbol{\varepsilon}}{iB} = i \frac{\boldsymbol{\varepsilon}}{B}}$$

An exponential $V(t) = e^{-iBt}V(0)$ solution results: e^{-iBt} is a clockwise 2D rotation.

complex form

$$v(t) + \beta = V(t) = e^{-iBt}V(0) = e^{-iBt}(v(0) + \beta) \quad \text{or:} \quad v(t) = e^{-iBt}(v(0) + \beta) - \beta = e^{-iBt}(v(0) + i\frac{\boldsymbol{\varepsilon}}{B}) - i\frac{\boldsymbol{\varepsilon}}{B}$$

Expanding e^{-iBt} , $v = v_x + i v_y$, and $\boldsymbol{\varepsilon} = \boldsymbol{\varepsilon}_x + i \boldsymbol{\varepsilon}_y$ reveals x (Real) and y (Imaginary) components

$$\begin{pmatrix} v_x(t) \\ v_y(t) \end{pmatrix} = \begin{pmatrix} \cos B \cdot t & \sin B \cdot t \\ -\sin B \cdot t & \cos B \cdot t \end{pmatrix} \begin{pmatrix} v_x(0) - \frac{\boldsymbol{\varepsilon}_y}{B} \\ v_y(0) + \frac{\boldsymbol{\varepsilon}_x}{B} \end{pmatrix} + \begin{pmatrix} \frac{\boldsymbol{\varepsilon}_y}{B} \\ -\frac{\boldsymbol{\varepsilon}_x}{B} \end{pmatrix}$$

vector form

Integrating $v(t)$ yields complex coordinate $q = x + iy$ affected by both $\boldsymbol{\varepsilon}_x$ and $\boldsymbol{\varepsilon}_y$.

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Move last part of this calculation UP↑

Crossed E and B field mechanics (Solution by complex variables)

$$\dot{V}(t) = \dot{v}(t) + \dot{\beta} = \varepsilon - iBv = \varepsilon - iB(V(t) - \beta) = -iBV(t)$$

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$$\begin{pmatrix} v_x(t) \\ v_y(t) \end{pmatrix} = \begin{pmatrix} \cos B \cdot t & \sin B \cdot t \\ -\sin B \cdot t & \cos B \cdot t \end{pmatrix} \begin{pmatrix} v_x(0) - \frac{\varepsilon_y}{B} \\ v_y(0) + \frac{\varepsilon_x}{B} \end{pmatrix} + \begin{pmatrix} \frac{\varepsilon_y}{B} \\ -\frac{\varepsilon_x}{B} \end{pmatrix}$$

vector form

Integrating $v(t)$ yields complex coordinate $q = x + iy$ affected by both ε_x and ε_y .

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$$x(t) + iy(t) = e^{-iBt} \left(i\frac{v(0)}{B} - \frac{\varepsilon}{B^2} \right) - i\frac{\varepsilon}{B} \cdot t + x(0) + iy(0) - i\frac{v(0)}{B} + \frac{\varepsilon}{B^2}$$

complex form

Crossed E and B field mechanics (Solution by complex variables)

$$\dot{V}(t) = \dot{v}(t) + \dot{\beta} = \varepsilon - iBv = \varepsilon - iB(V(t) - \beta) = -iBV(t)$$

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complex form

$$x(t) + iy(t) = e^{-iBt} \left(i\frac{v(0)}{B} - \frac{\varepsilon}{B^2}\right) - i\frac{\varepsilon}{B} \cdot t + x(0) + iy(0) - i\frac{v(0)}{B} + \frac{\varepsilon}{B^2}$$

complex form

$$\begin{pmatrix} x(t) \\ y(t) \end{pmatrix} = \begin{pmatrix} \cos B \cdot t & \sin B \cdot t \\ -\sin B \cdot t & \cos B \cdot t \end{pmatrix} \begin{pmatrix} -\frac{v_y(0)}{B} - \frac{\varepsilon_x}{B^2} \\ \frac{v_x(0)}{B} - \frac{\varepsilon_y}{B^2} \end{pmatrix} + \begin{pmatrix} \frac{\varepsilon_y}{B} t \\ -\frac{\varepsilon_x}{B} t \end{pmatrix} + \begin{pmatrix} x(0) + \frac{v_y(0)}{B} + \frac{\varepsilon_x}{B^2} \\ y(0) - \frac{v_x(0)}{B} + \frac{\varepsilon_y}{B^2} \end{pmatrix}$$

vector form

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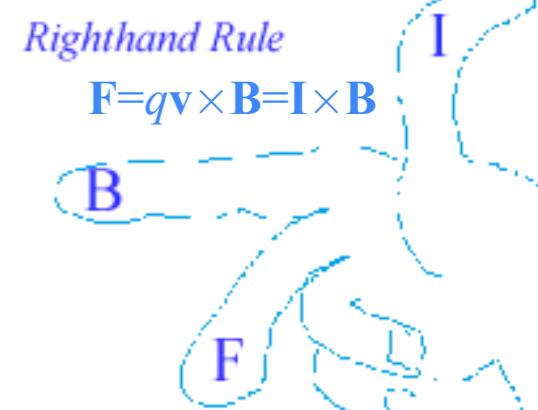
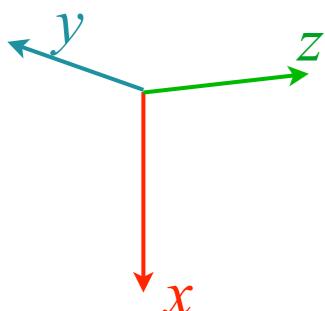
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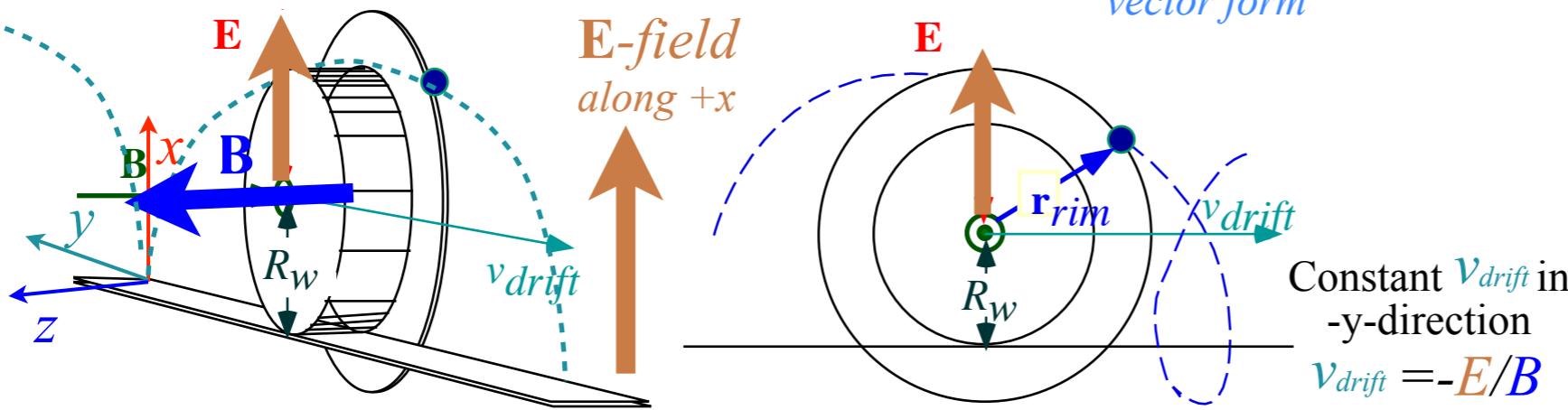
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vector form



Righthand Rule
 $\mathbf{F} = q\mathbf{v} \times \mathbf{B} = \mathbf{I} \times \mathbf{B}$



Cycloid example:
initial $(x(0), y(0)) = (0,0)$
and $(v_x(0), v_y(0)) = (0,0)$

$\begin{pmatrix} x(t) \\ y(t) \end{pmatrix}$ is on rim of a wheel of radius $R_W = E/B^2$

$$\begin{pmatrix} \cos B \cdot t & \sin B \cdot t \\ -\sin B \cdot t & \cos B \cdot t \end{pmatrix} \begin{pmatrix} -\frac{E}{B^2} \\ 0 \end{pmatrix}$$

$$+ \begin{pmatrix} 0 \\ -\frac{E}{B} t \end{pmatrix} + \begin{pmatrix} \frac{E}{B^2} \\ 0 \end{pmatrix}$$

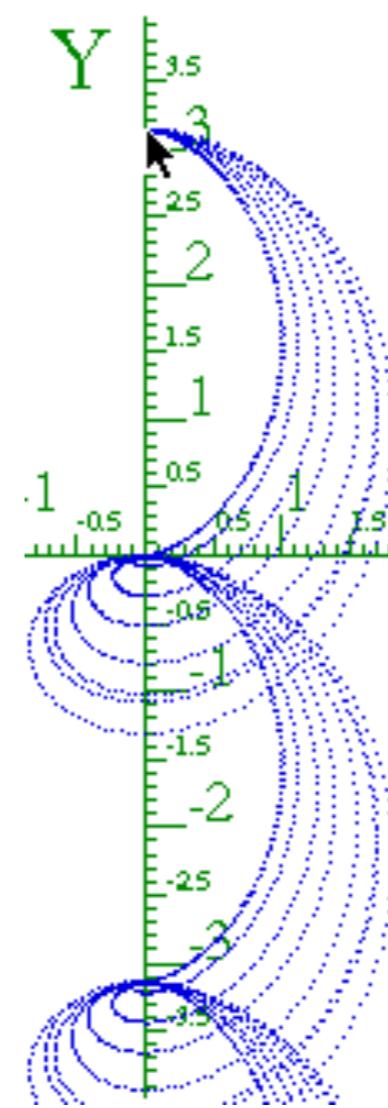
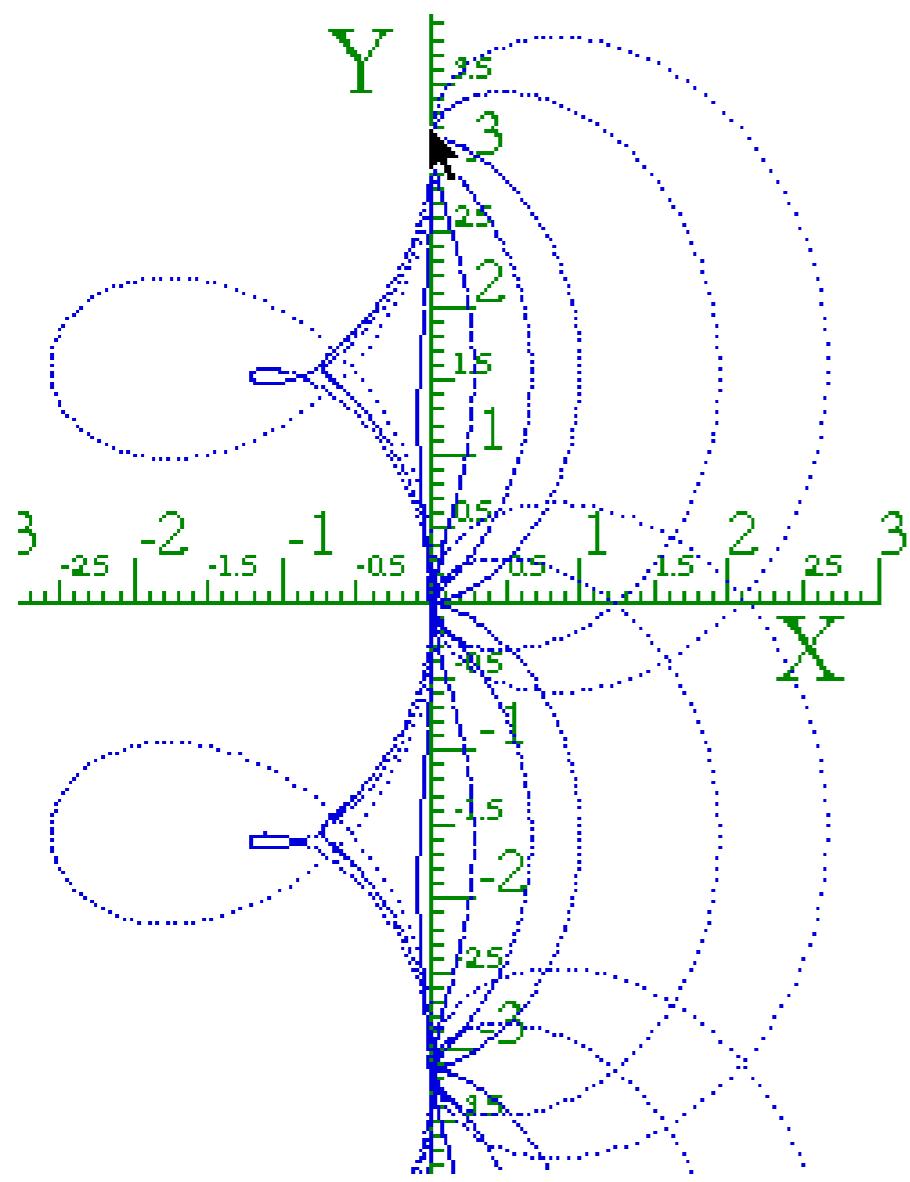
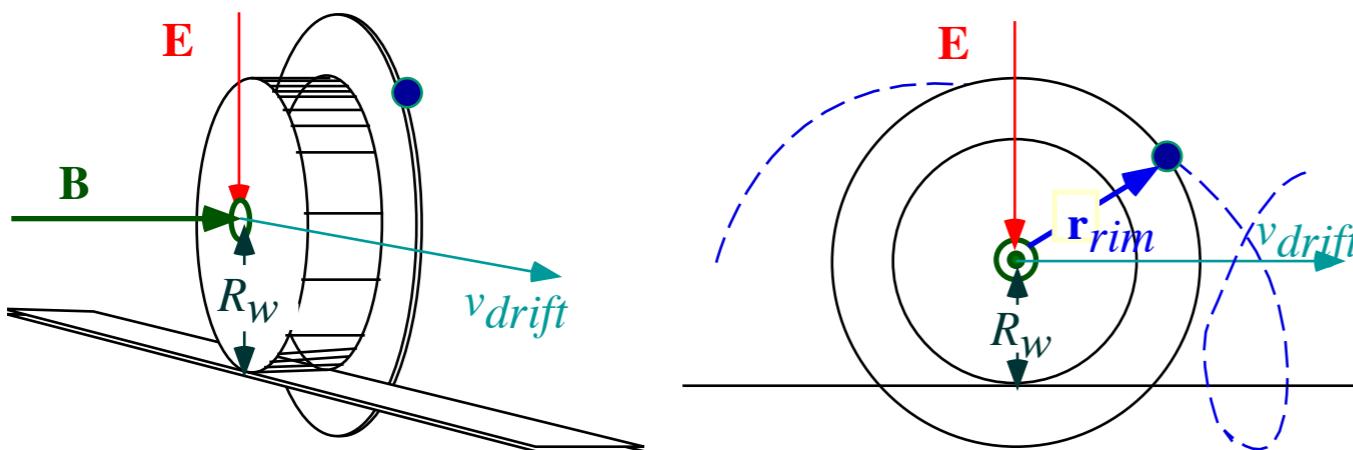


Fig. 2.8.2 Trajectories of unit charge and mass in magnetic and electric fields ($E=1/2$, $B=1$)

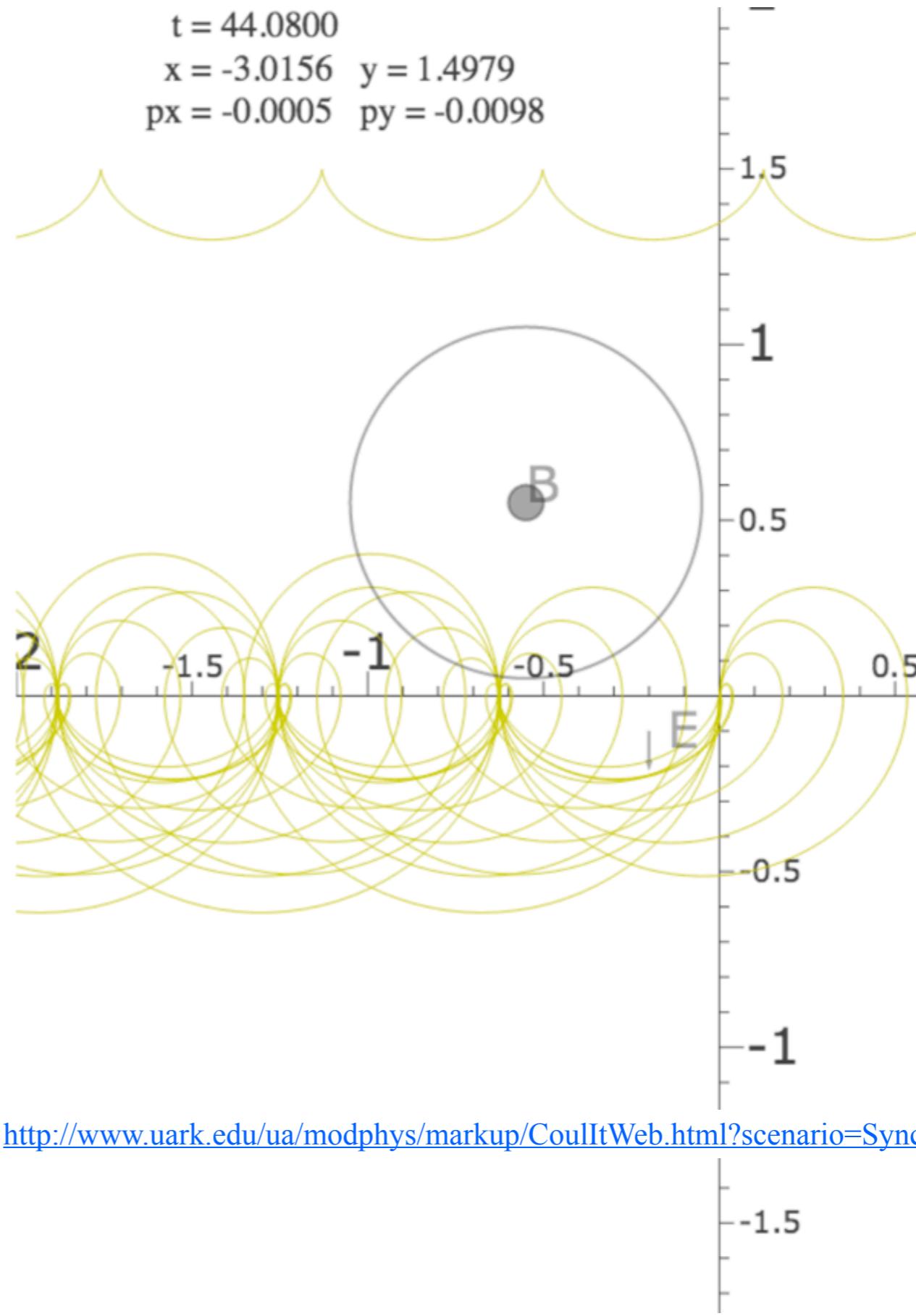
Fig. 2.8.3 Rolling railroad wheel and rim analogy for cyclotron orbits



Initial position $x(0) = 1.38263$
 Initial position $y(0) = 1.49839$
 Initial momentum $px(0) = 0$
 Initial momentum $py(0) = 0$

 Terminal time $t(\text{off}) = 6.28318$
 Maximum step size $dt = 0.08$
 Charge of Nucleus 1 = 0
 Charge of Nucleus 2 = 0
 Coulomb (k_{12}) = 0
 Core thickness $r = 0.00000$
 x-Stark field $Ex = 0$
 y-Stark field $Ey = -0.1$
 Zeeman field $Bz = 1$
 Diamagnetic strength $k = 0$
 Plank constant $\hbar = 1.57079$
 Color quantization hues = 64
 Color quantization bands = 2
 Fractional Error (e^{-x}), $x = 8$
 Particle Size = 8

 Fix $r(0)$ Fix $p(0)$ Do swarm Beam
 Plot $r(t)$ Plot $p(t)$
 Color action No stops Field vectors Info
 Draw masses Axes Coordinates Lenz
 Set p by ϕ Elastic
 Save to GIF



Initial position $x(0)$ = -0.0021

Initial position $y(0)$ = -0.0064

Initial momentum $px(0)$ = -0.5016

Initial momentum $py(0)$ = 0

Terminal time $t(\text{off})$ = 6.28318

Maximum step size dt = 0.08

Charge of Nucleus 1 = 0

Charge of Nucleus 2 = 0

Coulomb (k_{12}) = 0

Core thickness r = 0.00000

x -Stark field Ex = 0

y -Stark field Ey = -0.1

Zeeman field Bz = 1

Diamagnetic strength k = 0

Plank constant \hbar = 1.57079

Color quantization hues = 64

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Fractional Error (e^{-x}), x = 8

Particle Size = 8

Fix $r(0)$ Fix $p(0)$ Do swarm Beam

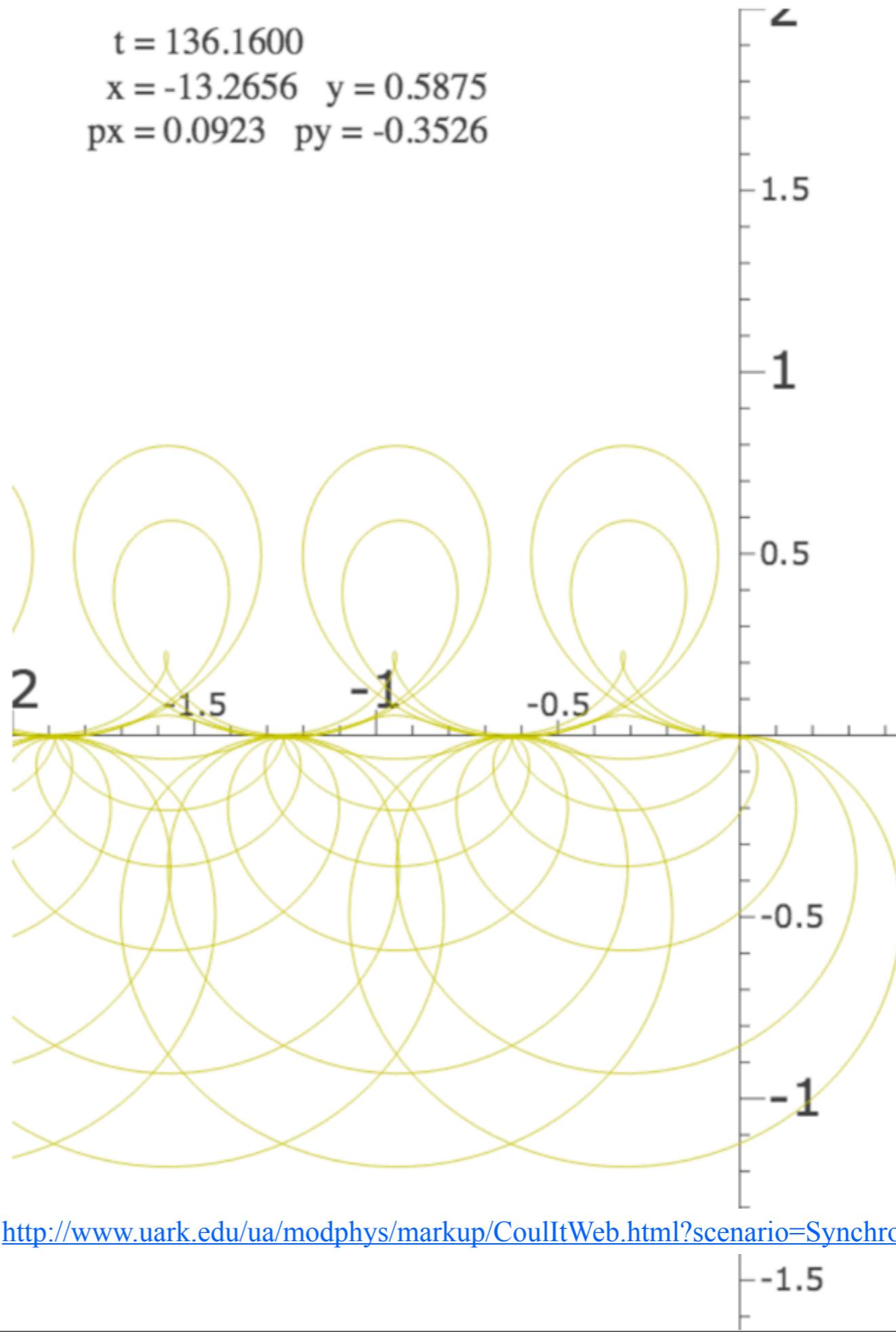
Plot $r(t)$ Plot $p(t)$

Color action No stops Field vectors Info

Draw masses Axes Coordinates Lenz

Set p by ϕ Elastic 2 Free

$t = 136.1600$
 $x = -13.2656 \quad y = 0.5875$
 $px = 0.0923 \quad py = -0.3526$



<http://www.uark.edu/ua/modphys/markup/CoulItWeb.html?scenario=SynchrotronMotion2>

Crossed E and B field mechanics

Classical Hall-effect and cyclotron orbit equations

Vector theory vs. complex variable theory

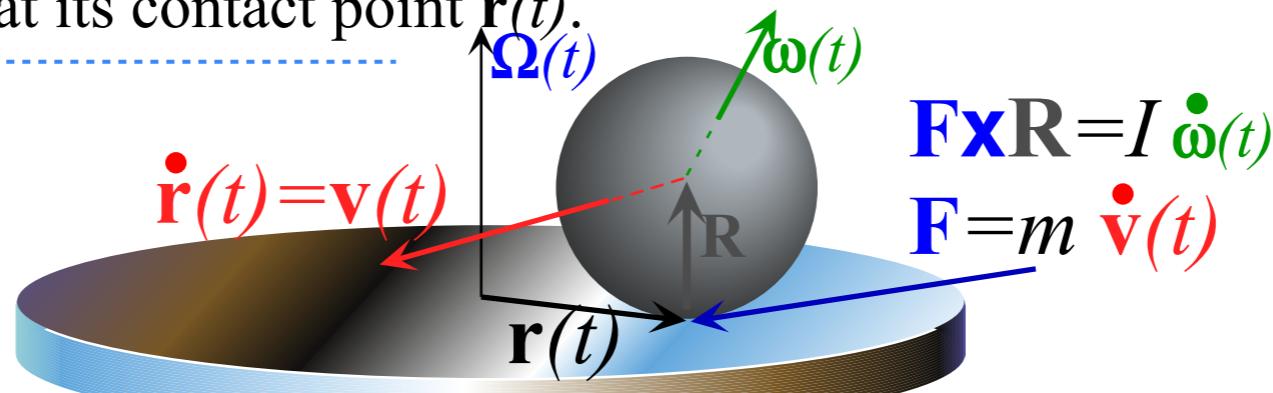
→ *Mechanical analog of cyclotron and FBI rule*

Cycloid geometry and flying sticks

Practical poolhall application

Mechanical analog of cyclotron and FBI rule

Velocity vector of the ball contact point ($\mathbf{v}(t)$) equals
table surface velocity $\Omega \times \mathbf{r}(t)$ at its contact point $\mathbf{r}(t)$.



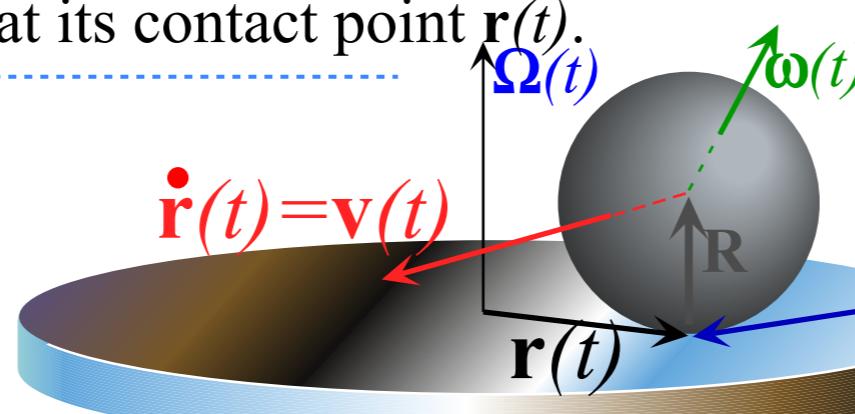
Turntable turning at constant angular velocity $\Omega = \Omega \hat{\mathbf{z}}$.



[YouTube Video of Analog to Syncrotron Motion](#)

Mechanical analog of cyclotron and FBI rule

Velocity vector of the ball contact point ($\mathbf{v}(t)$) equals
table surface velocity $\Omega \times \mathbf{r}(t)$ at its contact point $\mathbf{r}(t)$.



Equations of Motion:

rotation Torque = $\mathbf{F} \times \mathbf{R} = I \ddot{\omega}$

$$\mathbf{F} \times \mathbf{R} = I \ddot{\omega}$$

$$\mathbf{F} = m \ddot{\mathbf{v}}$$

translation Force = $\mathbf{F} = m \dot{\mathbf{v}}$

Turntable turning at constant angular velocity $\Omega = \Omega \hat{\mathbf{z}}$.

Torque-and-F=ma
equations of motion:

$$I \ddot{\omega}(t) = \mathbf{F}(t) \times \mathbf{R}$$

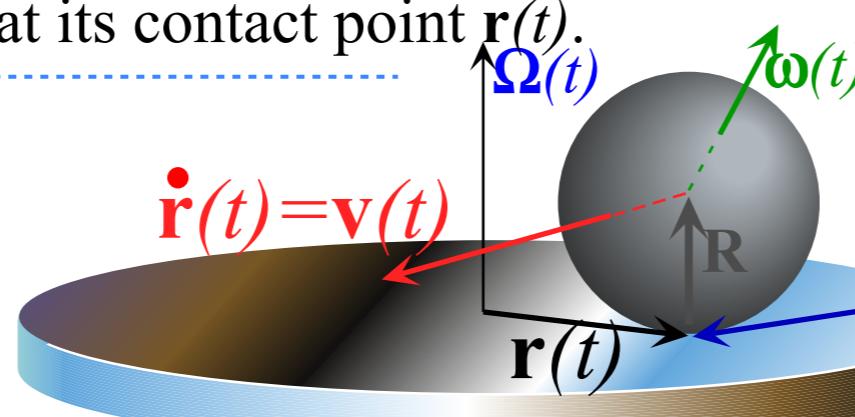
$$= m \ddot{\mathbf{v}}(t) \times \mathbf{R}$$

$$= m \ddot{\mathbf{v}}(t) \times \hat{\mathbf{z}} R$$

Mechanical analog of cyclotron and FBI rule

Velocity vector of the ball contact point ($\mathbf{v}(t)$) equals table surface velocity $\Omega \times \mathbf{r}(t)$ at its contact point $\mathbf{r}(t)$.

Rolling Constraint



Equations of Motion:

rotation Torque $= \mathbf{F} \times \mathbf{R} = I \ddot{\omega}$

$$\mathbf{F} \times \mathbf{R} = I \ddot{\omega}$$

$$\mathbf{F} = m \ddot{\mathbf{v}}$$

translation Force $= \mathbf{F} = m \ddot{\mathbf{v}}$

Turntable turning at constant angular velocity $\Omega = \Omega \hat{\mathbf{z}}$.

No-slipping: $\mathbf{v}(t) - \omega(t) \times \mathbf{R} = \Omega \times \mathbf{r}(t)$ (where: $\mathbf{R} = R \hat{\mathbf{z}}$ and $\Omega = \Omega \hat{\mathbf{z}}$ are constant.)

Torque-and-F=ma
equations of motion:

$$I \ddot{\omega}(t) = \mathbf{F}(t) \times \mathbf{R}$$

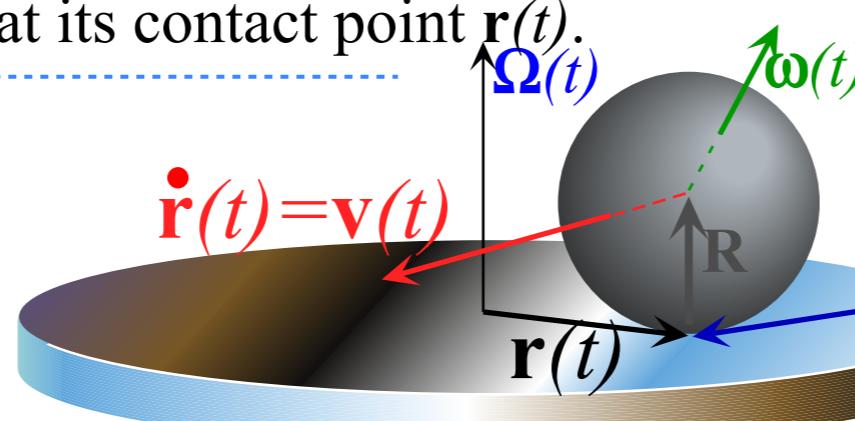
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Mechanical analog of cyclotron and FBI rule

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Rolling Constraint



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$$\mathbf{F} \times \mathbf{R} = I \dot{\omega}$$

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translation Force = $\mathbf{F} = m \dot{\mathbf{v}}$

Turntable turning at constant angular velocity $\Omega = \Omega \hat{\mathbf{z}}$.

No-slipping: $\mathbf{v}(t) - \omega(t) \times \mathbf{R} = \Omega \times \mathbf{r}(t)$ (where: $\mathbf{R} = R \hat{\mathbf{z}}$ and $\Omega = \Omega \hat{\mathbf{z}}$ are constant.)

$$\mathbf{v}(t) = \Omega \times \mathbf{r}(t) + \omega(t) \times \mathbf{R} = \Omega \times \mathbf{r}(t) + \omega(t) \times \hat{\mathbf{z}} R$$

Torque-and-F=ma
equations of motion:

$$I \dot{\omega}(t) = \mathbf{F}(t) \times \mathbf{R}$$

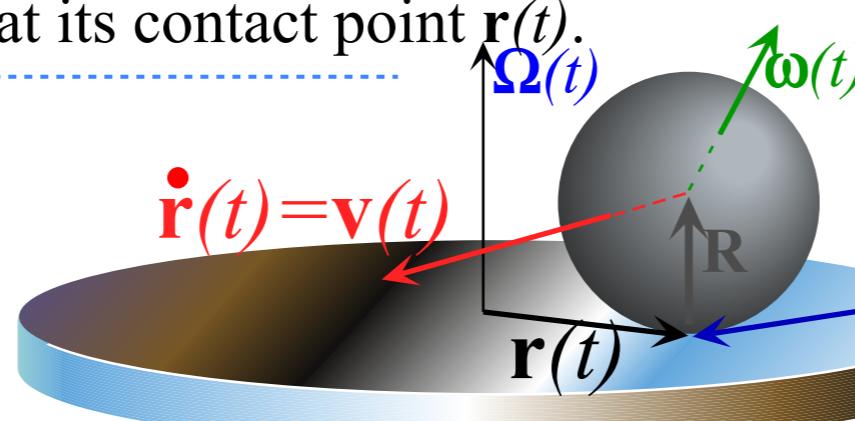
$$= m \dot{\mathbf{v}}(t) \times \mathbf{R}$$

$$= m \dot{\mathbf{v}}(t) \times \hat{\mathbf{z}} R$$

Mechanical analog of cyclotron and FBI rule

Velocity vector of the ball contact point ($\mathbf{v}(t)$) equals table surface velocity $\Omega \times \mathbf{r}(t)$ at its contact point $\mathbf{r}(t)$.

Rolling Constraint



Equations of Motion:

rotation Torque = $\mathbf{F} \times \mathbf{R} = I\dot{\omega}$

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$$\mathbf{F} = m \dot{\mathbf{v}}$$

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Turntable turning at constant angular velocity $\Omega = \Omega \hat{\mathbf{z}}$.

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$$\mathbf{v}(t) = \Omega \times \mathbf{r}(t) + \omega(t) \times \mathbf{R} = \Omega \times \mathbf{r}(t) + \omega(t) \times \hat{\mathbf{z}}R \quad \text{Do time-derivative}$$

$$\dot{\mathbf{v}}(t) = \Omega \times \dot{\mathbf{r}}(t) + \dot{\omega}(t) \times \hat{\mathbf{z}}R = \Omega \times \mathbf{v}(t) + \dot{\omega}(t) \times \hat{\mathbf{z}}R$$

Torque-and-F=ma
equations of motion:

$$I\dot{\omega}(t) = \mathbf{F}(t) \times \mathbf{R}$$

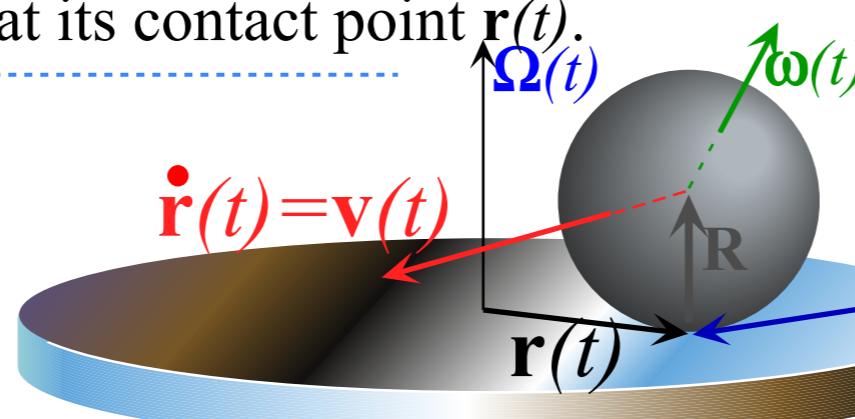
$$= m\dot{\mathbf{v}}(t) \times \mathbf{R}$$

$$= m\dot{\mathbf{v}}(t) \times \hat{\mathbf{z}}R$$

Mechanical analog of cyclotron and FBI rule

Velocity vector of the ball contact point ($\mathbf{v}(t)$) equals table surface velocity $\Omega \times \mathbf{r}(t)$ at its contact point $\mathbf{r}(t)$.

Rolling Constraint



Equations of Motion:

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$$\dot{\mathbf{v}}(t) = \Omega \times \dot{\mathbf{r}}(t) + \dot{\omega}(t) \times \hat{\mathbf{z}}R \quad \text{use: } \dot{\omega}(t) = \frac{m \dot{\mathbf{v}}(t) \times \hat{\mathbf{z}}R}{I}$$

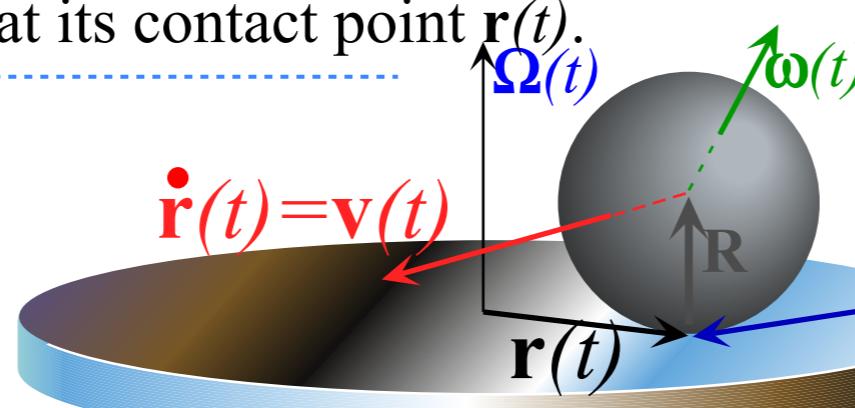
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$$\begin{aligned} I \dot{\omega}(t) &= \mathbf{F}(t) \times \mathbf{R} \\ &= m \dot{\mathbf{v}}(t) \times \mathbf{R} \\ &= m \dot{\mathbf{v}}(t) \times \hat{\mathbf{z}}R \end{aligned}$$

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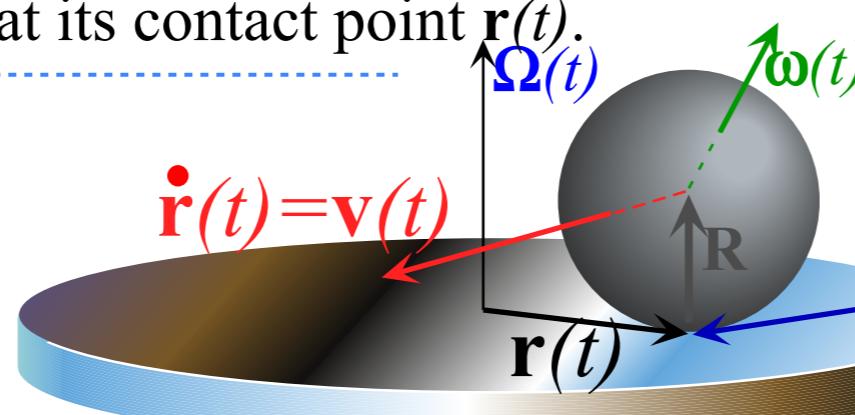
$$= m \dot{\mathbf{v}}(t) \times \hat{\mathbf{z}}R$$

$$\dot{\mathbf{v}}(t) = \Omega \times \mathbf{v}(t) + \frac{m \dot{\mathbf{v}}(t) \times \hat{\mathbf{z}}R}{I} \times \hat{\mathbf{z}}R$$

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($\mathbf{v}(t)$ always normal to $\hat{\mathbf{z}}$)

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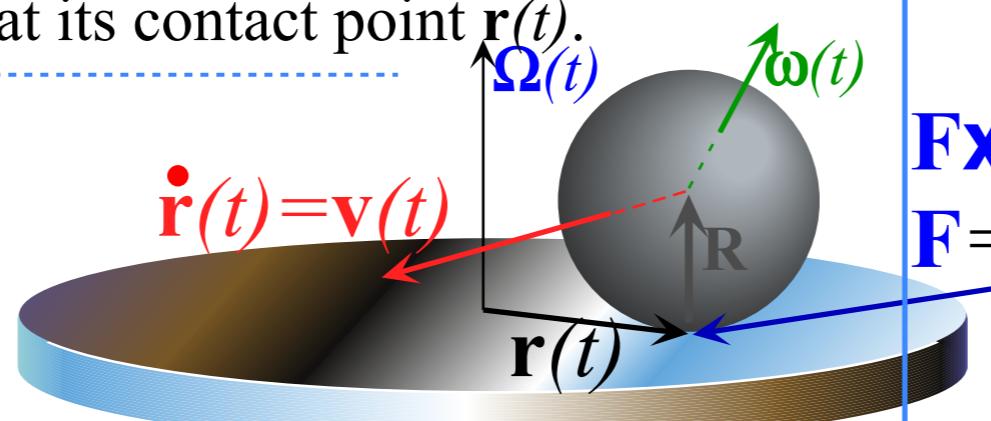
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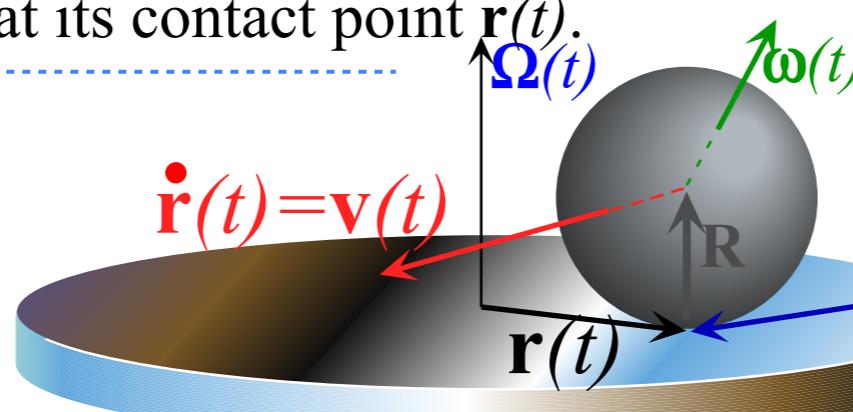
$$\dot{\mathbf{v}}(t) = \Omega \times \mathbf{v}(t) + 0 - \frac{m R^2}{I} \dot{\mathbf{v}}(t)$$

since $\dot{\mathbf{v}}(t)$ always in table plane

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$$\left(1 + \frac{m R^2}{I}\right) \dot{\mathbf{v}}(t) = \Omega \times \mathbf{v}(t)$$

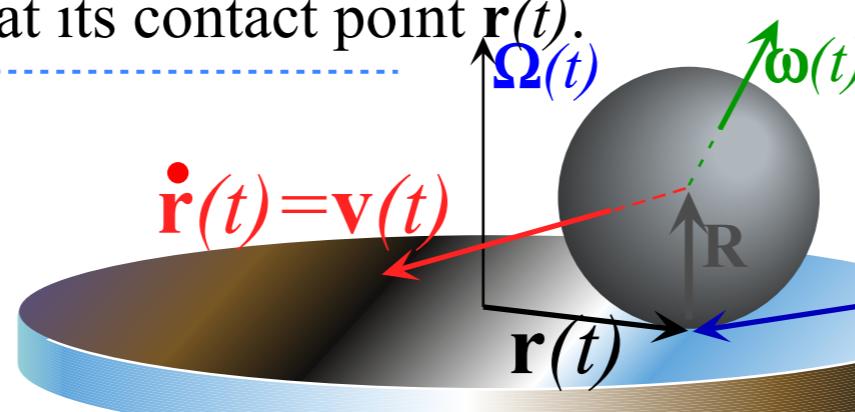
F=B×v mechanical analog:

$$\text{or: } \dot{\mathbf{v}}(t) = \frac{\Omega}{1 + \frac{m R^2}{I}} \times \mathbf{v}(t)$$

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ma = eB × v mechanical analog:

$$\dot{\mathbf{v}}(t) = \frac{\Omega}{1 + \frac{m R^2}{I}} \times \mathbf{v}(t)$$

or:

Torque-and-F=ma
equations of motion:

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*Mechanical analog
cyclotron frequency*

$$\omega = \frac{e}{m} B = \frac{\Omega}{1 + \frac{m R^2}{I}}$$

$$\omega = \frac{2}{7} \Omega \text{ for: } \frac{I}{m R^2} = \frac{2}{5} \quad \text{or: } \frac{I}{m R^2} = \frac{2}{3}$$



[YouTube Video of Analog to Syncrotron Motion](#)

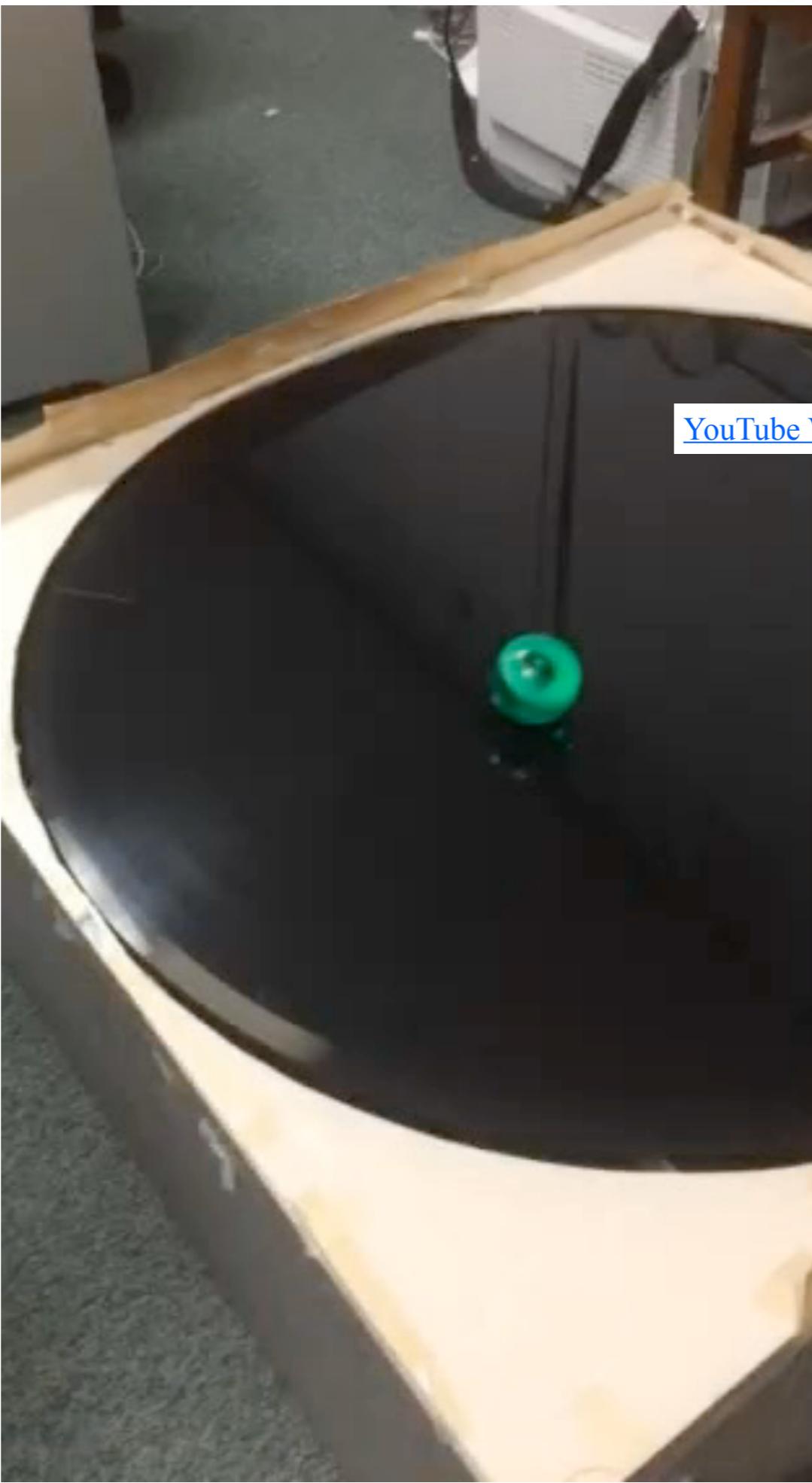
Solid ball has 2 orbits
as table turns 7 rotations

Mechanical analog cyclotron frequency

$$\omega = \frac{e}{m} B = \frac{\Omega}{1 + \frac{I}{mR^2}}$$

$\omega = \frac{2}{7} \Omega$ for: $\frac{I}{mR^2} = \frac{2}{5}$

$= \frac{2}{5} \Omega$ for: $\frac{I}{mR^2} = \frac{2}{3}$



Crossed E and B field mechanics

Classical Hall-effect and cyclotron orbits

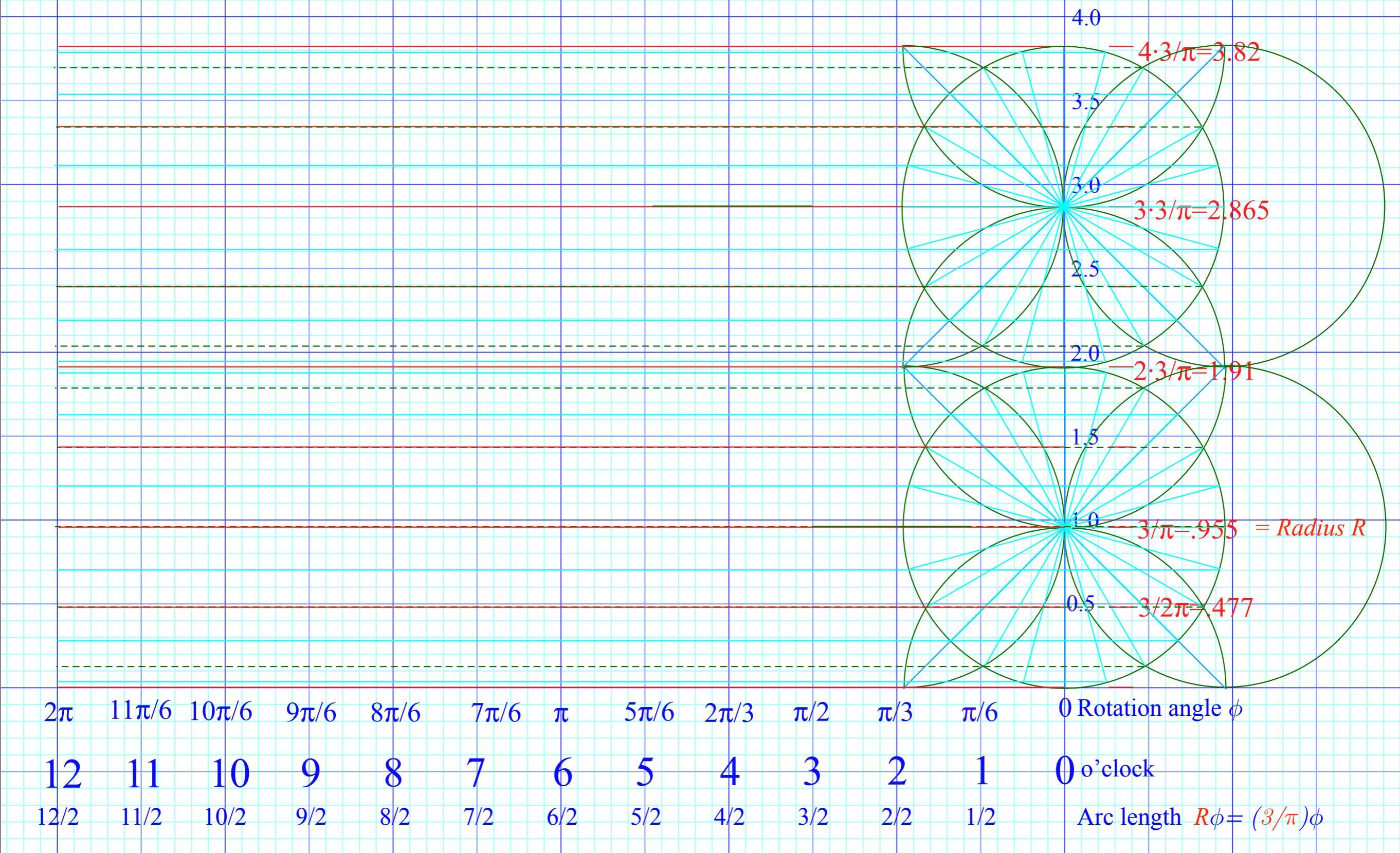
Vector theory vs. complex variable theory

Mechanical analog of cyclotron and FBI rule

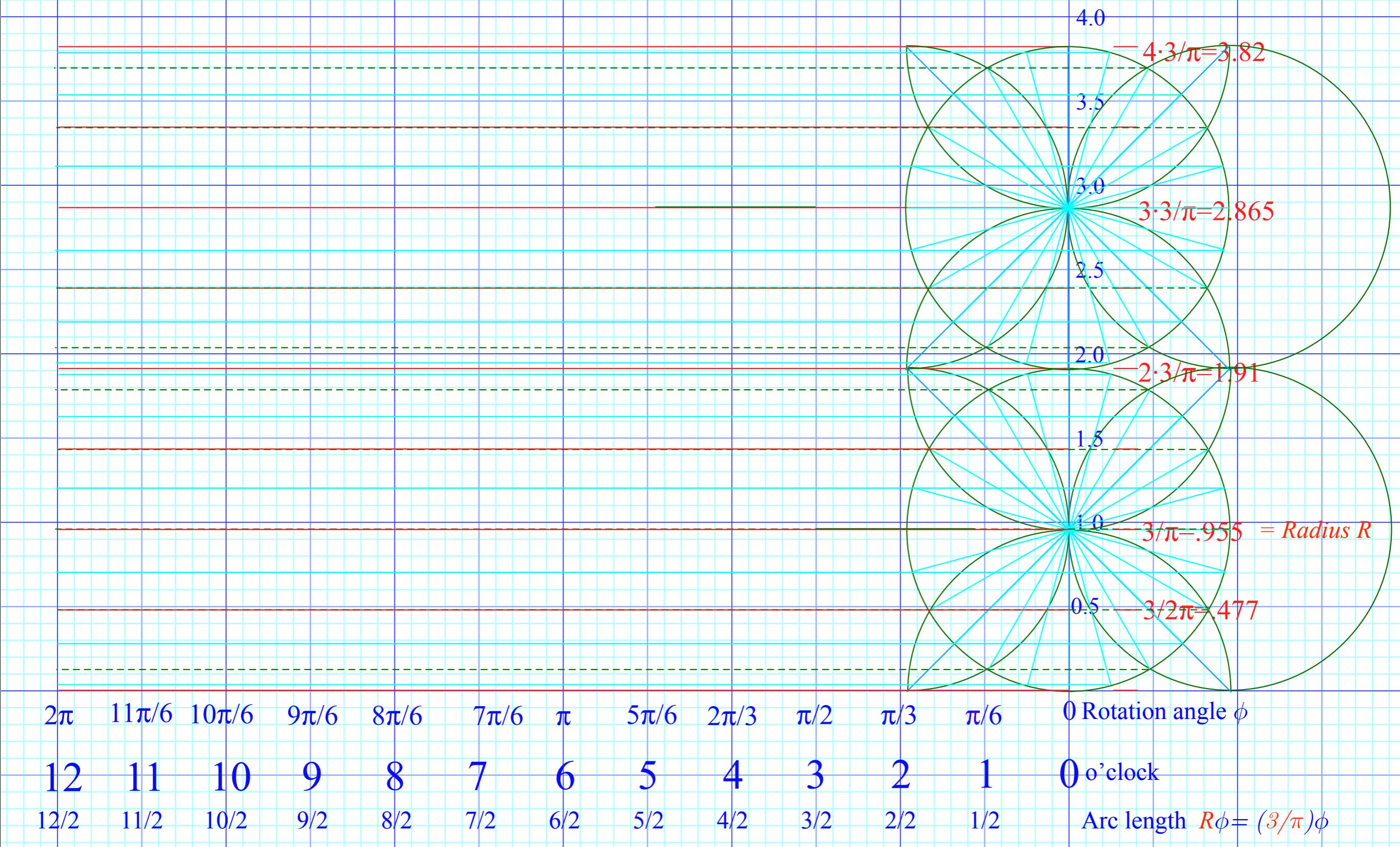
→ *Cycloid geometry and flying sticks*

Practical poolhall application

Here the radius is plotted as an irrational $R = 3/\pi = 0.955$ length so rolling by rational angle $\phi = m\pi/n$ is a rational length of rolled-out circumference $R\phi = (3/\pi)m\pi/n = 3m/n$.



Here the radius is plotted as an irrational $R=3/\pi=0.955$ length so rolling by rational angle $\phi=m\pi/n$ is a rational length of rolled-out circumference $R\phi=(3/\pi)m\pi/n=3m/n$. Diameter is $2R=6/\pi=1.91$



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Red circle rolls left-to-right on $y=3.82$ ceiling

Contact point goes from $(x=6/2, y=3.82)$ to $x=0$.

Ceiling $y=3.82$

$\pi/6$

4.0

$4 \cdot 3/\pi = 3.82$

3.5

$3 \cdot 3/\pi = 2.865$

3.0

2.5

2.0

$2 \cdot 3/\pi = 1.91$

Ceiling $y=1.91$

Green circle rolls right-to-left on $y=1.91$ ceiling

Contact point goes from $(x=0, y=1.91)$ to $x=6/2$.

$\pi/6$

1.5

$3/\pi = .955 = \text{Radius } R$

1.0

$3/2\pi = .477$

0.5

$2\pi \quad 11\pi/6 \quad 10\pi/6 \quad 9\pi/6 \quad 8\pi/6 \quad 7\pi/6 \quad \pi \quad 5\pi/6 \quad 2\pi/3 \quad \pi/2 \quad \pi/3 \quad \pi/6 \quad$ Rotation angle ϕ

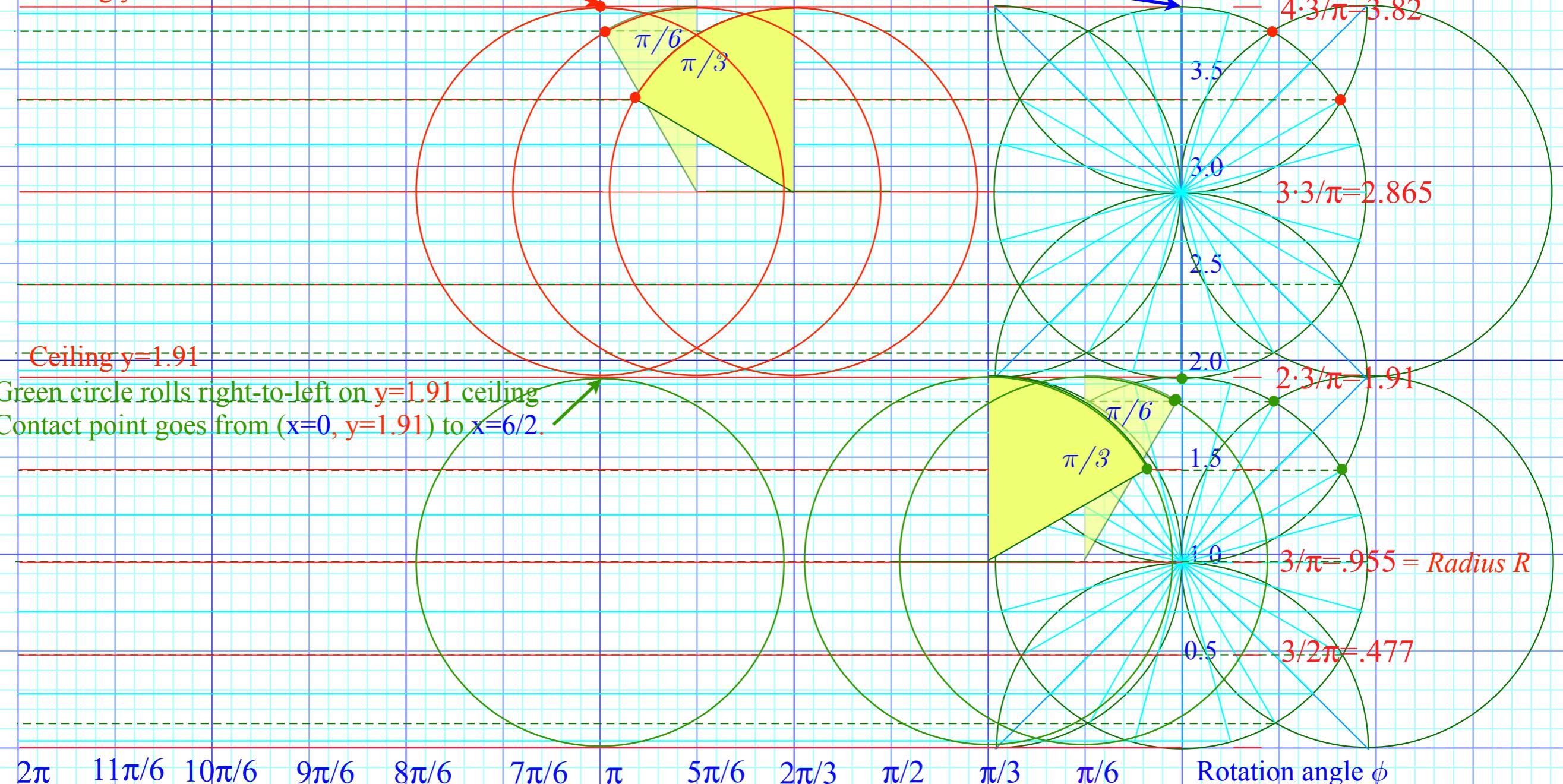
12	11	10	9	8	7	6	5	4	3	2	1	0 o'clock
12/2	11/2	10/2	9/2	8/2	7/2	6/2	5/2	4/2	3/2	2/2	1/2	Arc length $R\phi = (3/\pi)\phi$

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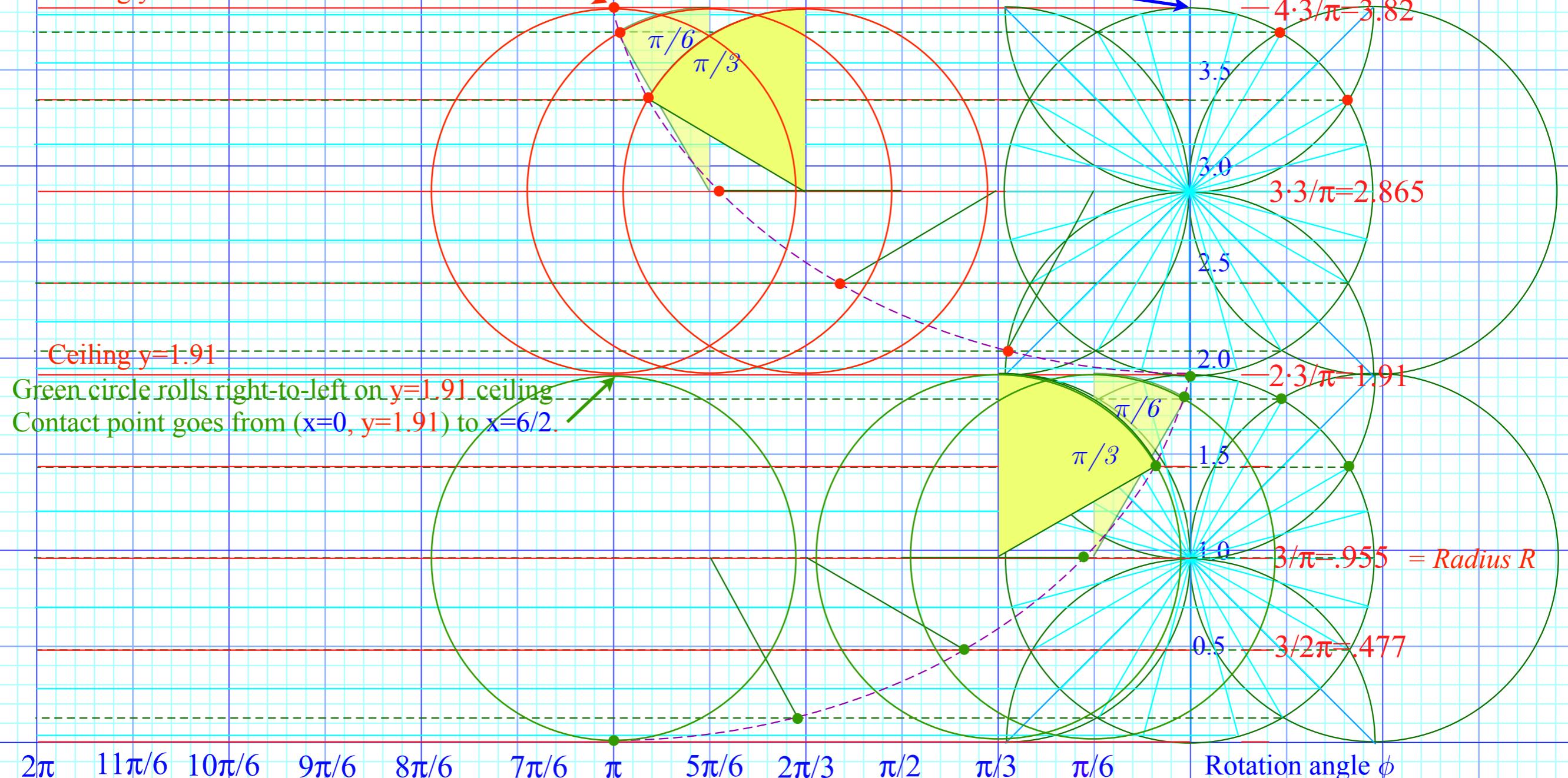
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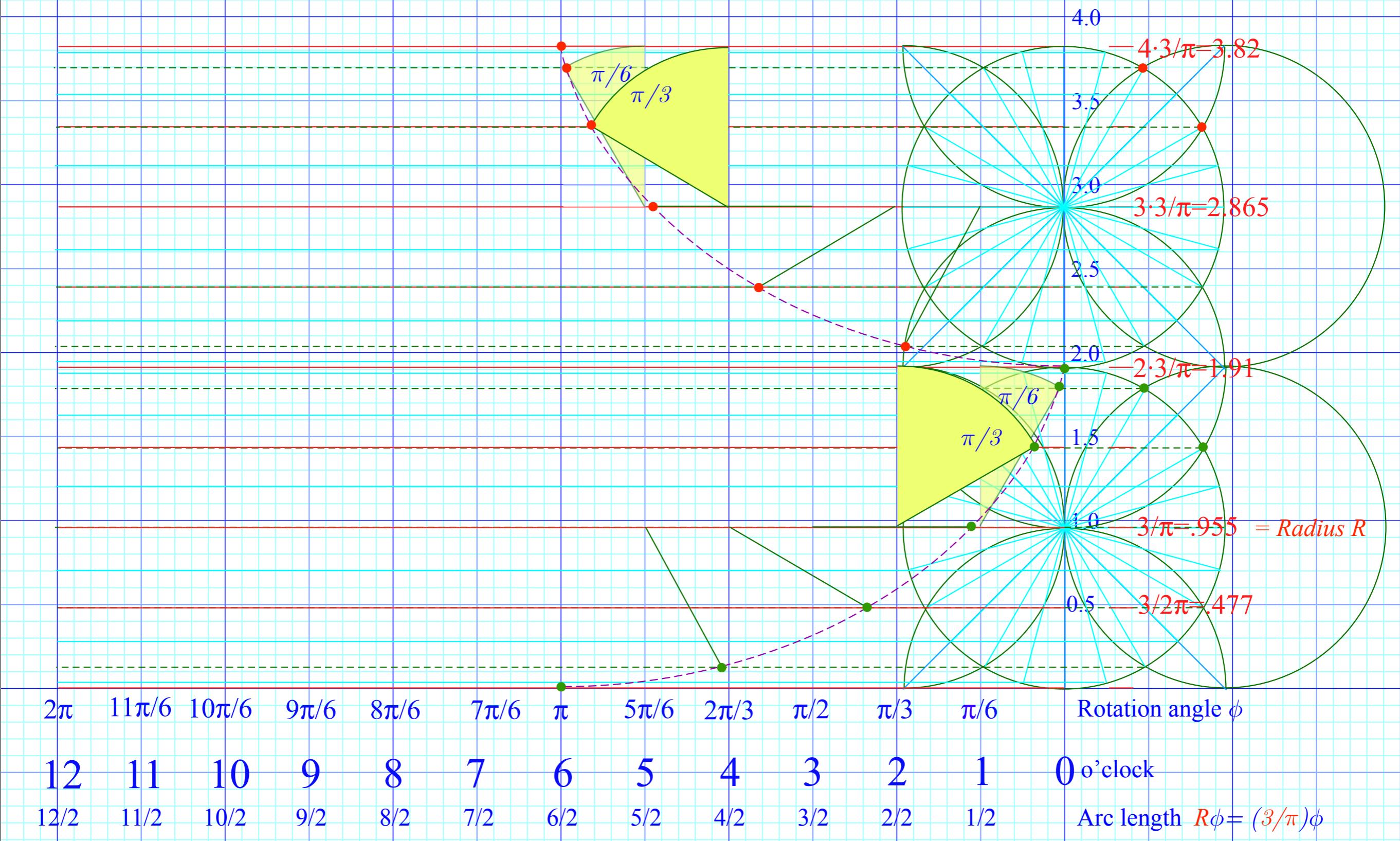
Red circle rolls left-to-right on $y=3.82$ ceiling

Contact point goes from $(x=6/2, y=3.82)$ to $x=0$.

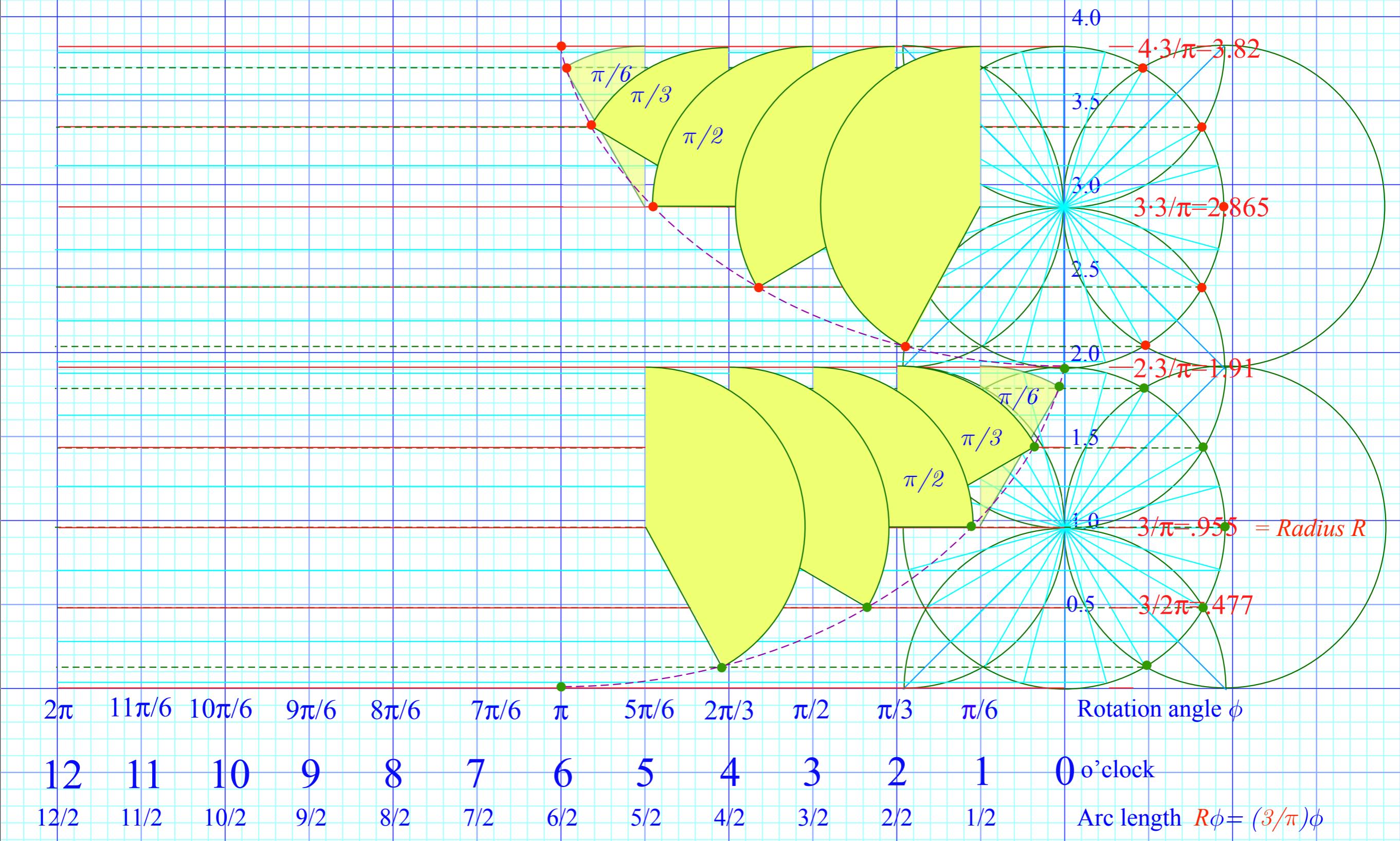
Ceiling $y=3.82$

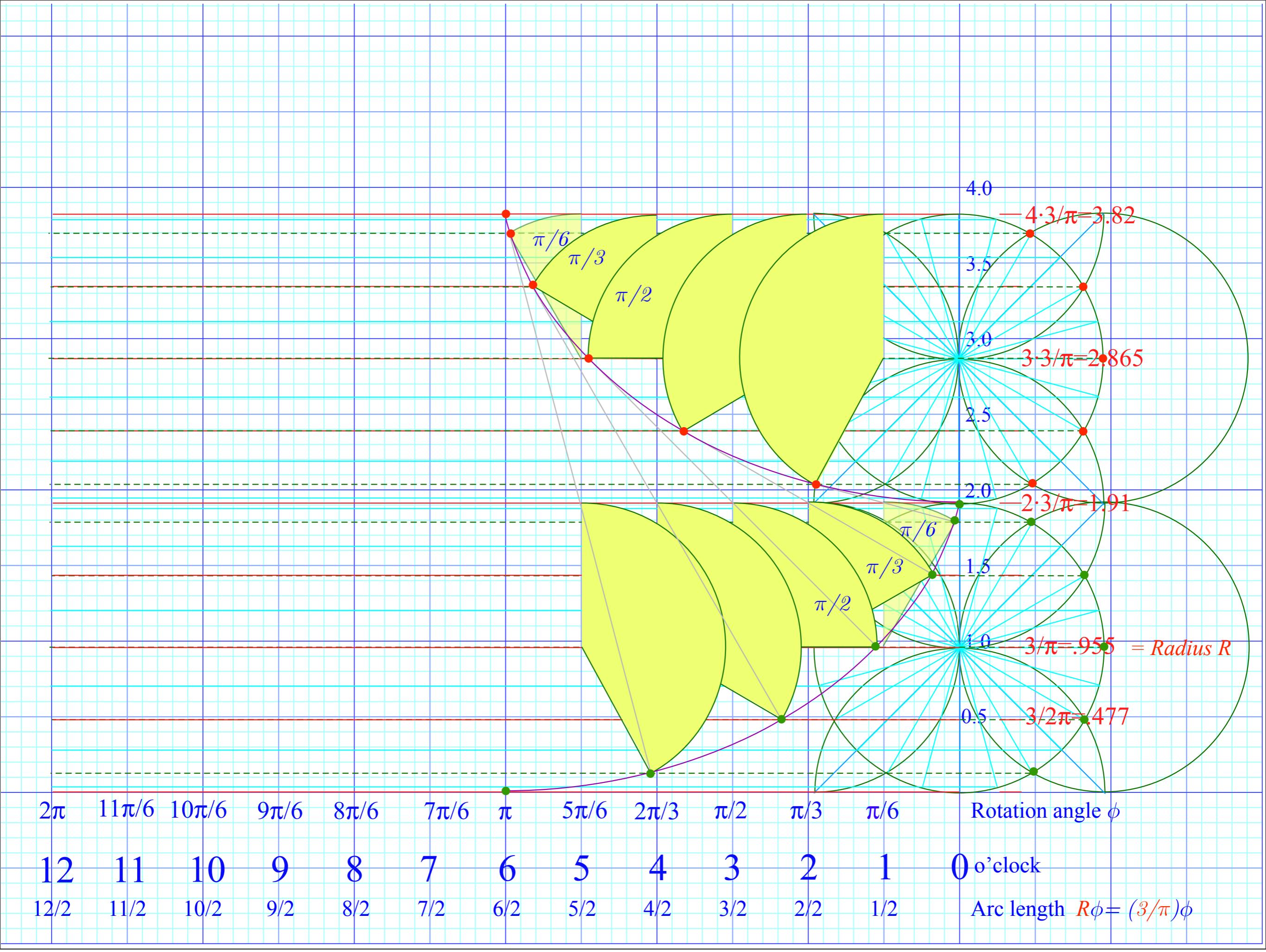


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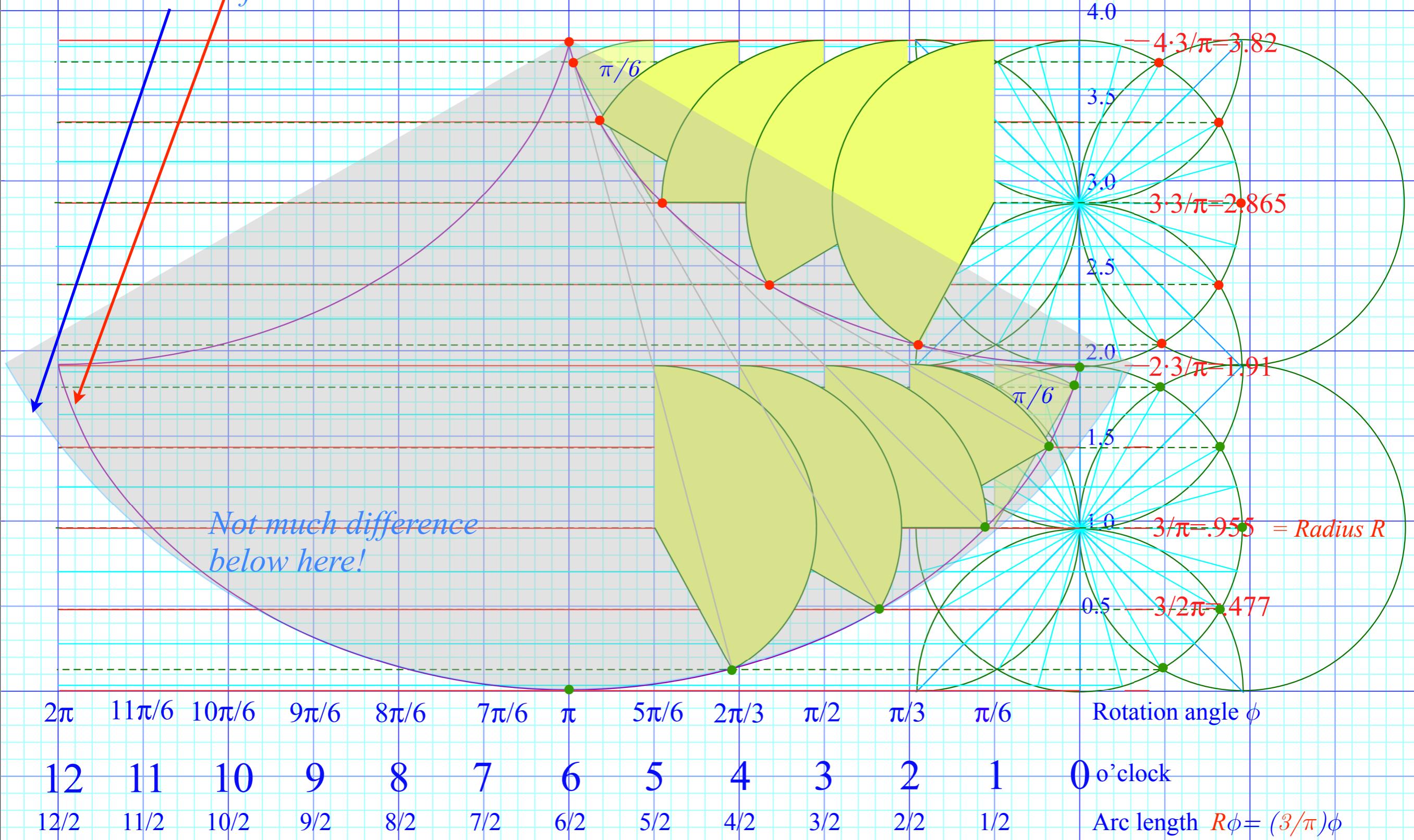
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*Compare cycloid of y-diameter $2R$ and x-diameter $2\pi R$
to circle arc of radius $4R$*



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you give it some linear momentum Π
and some angular momentum $\Lambda = h \cdot \Pi$

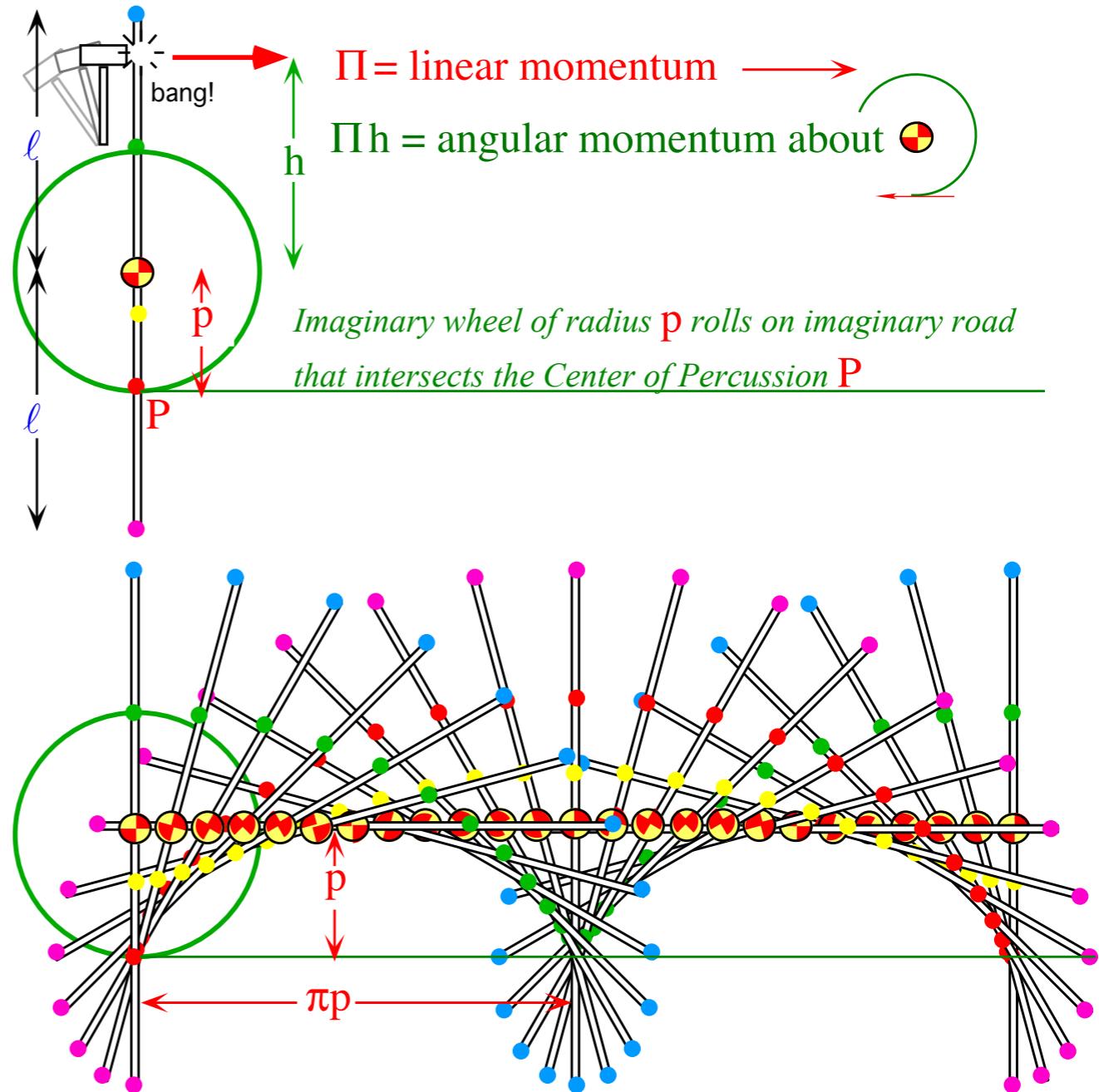


Fig. 2.A.1 Cycloidal paths due to hitting a stationary stick.

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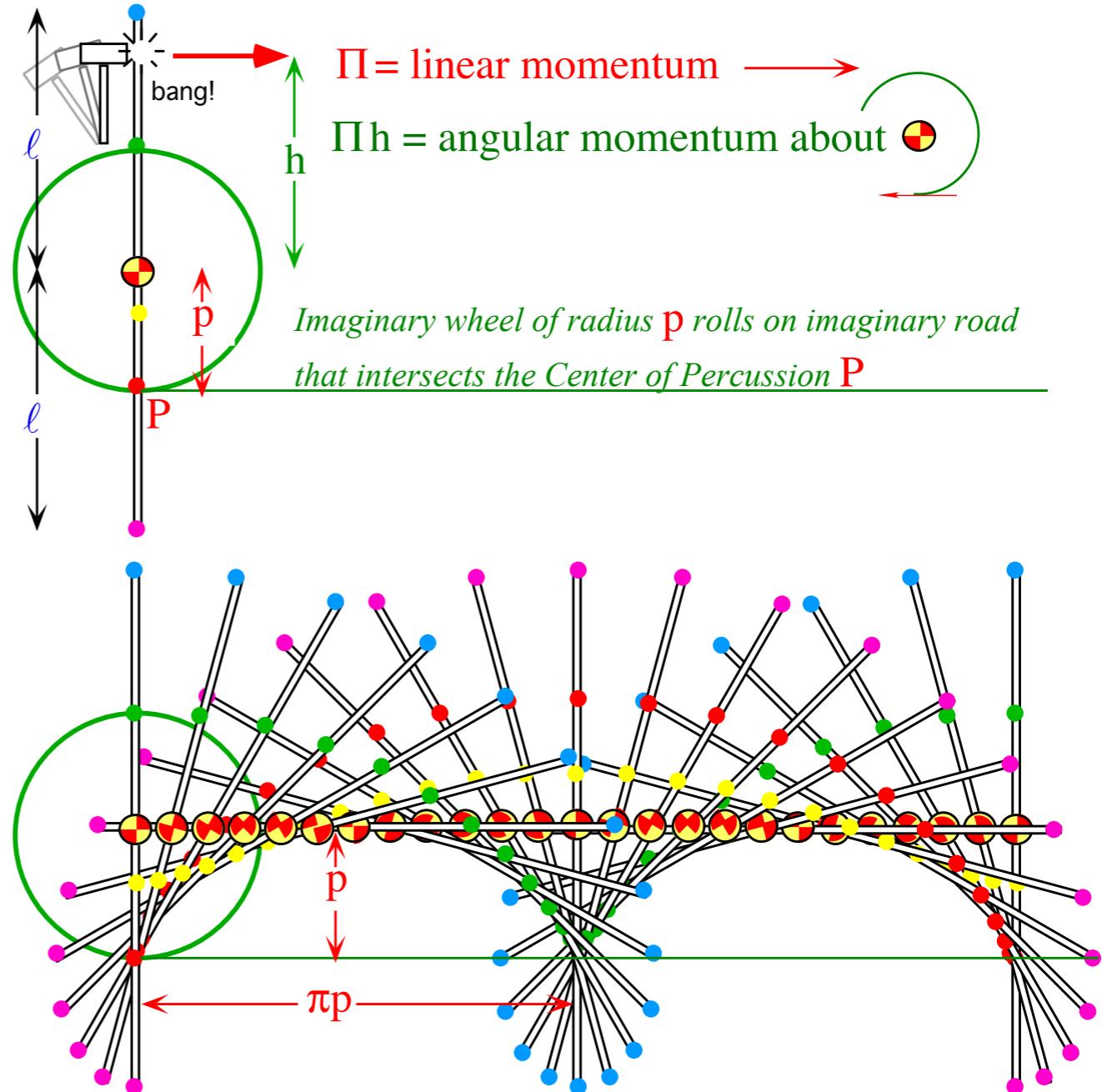


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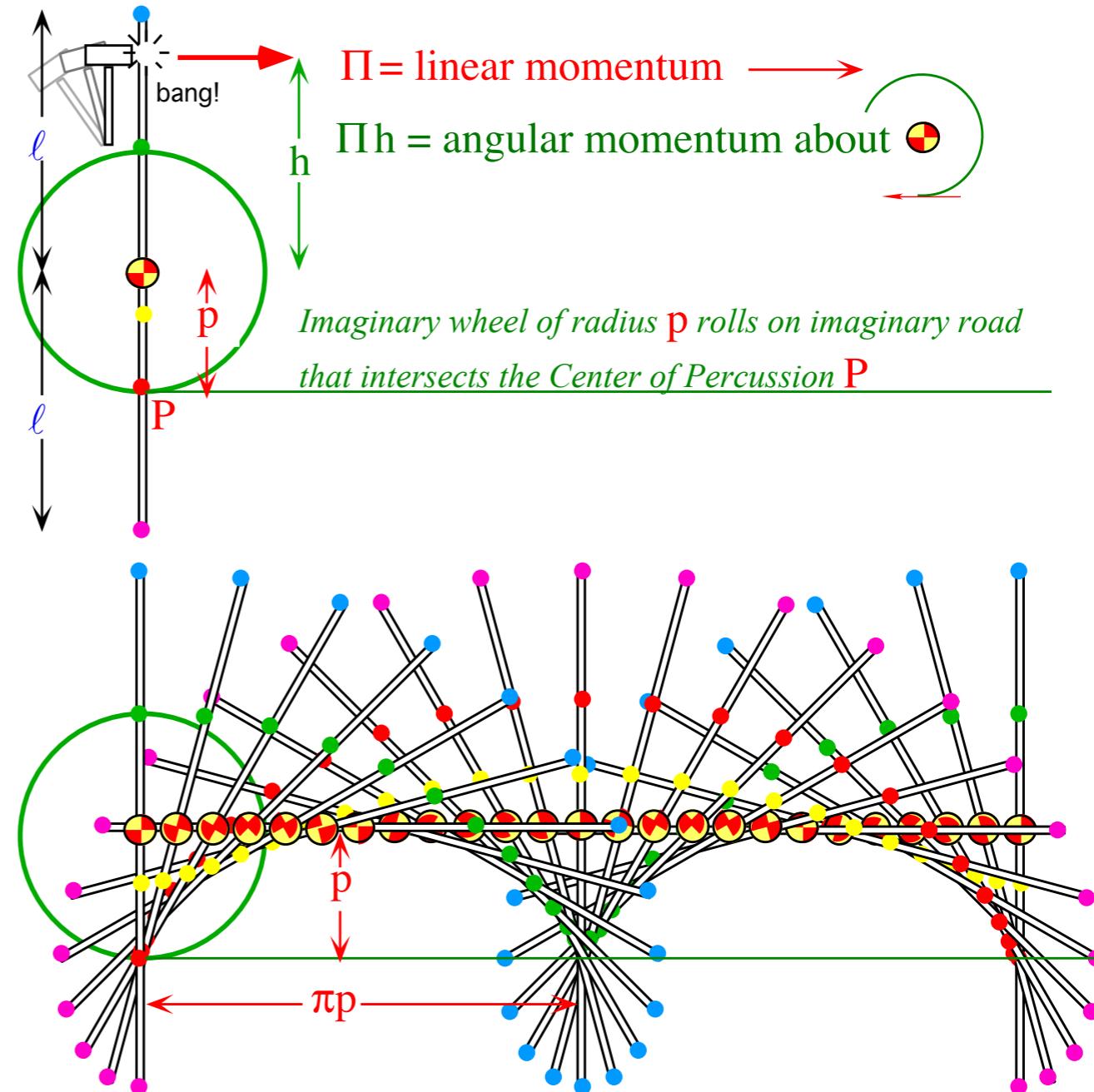


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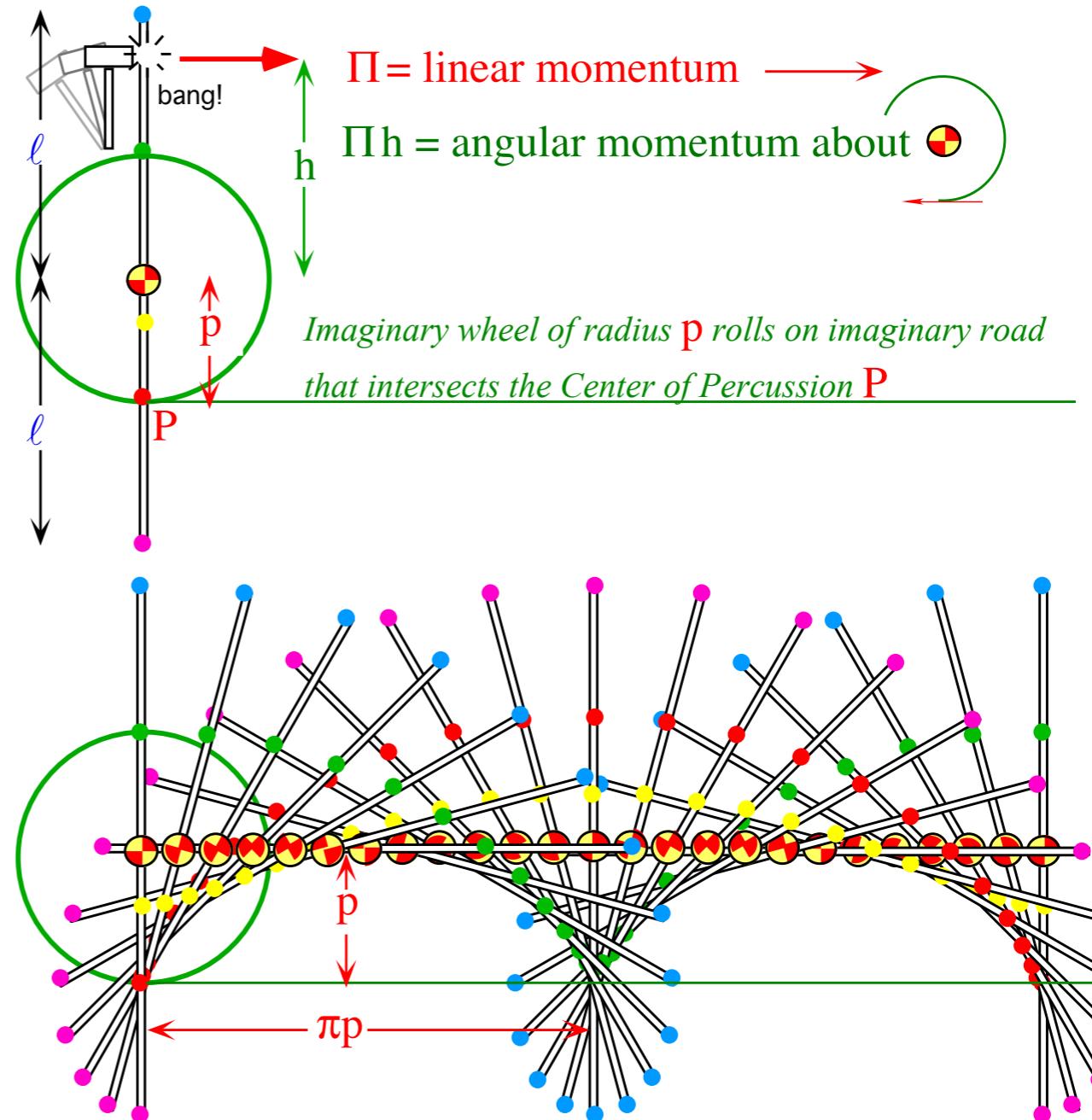


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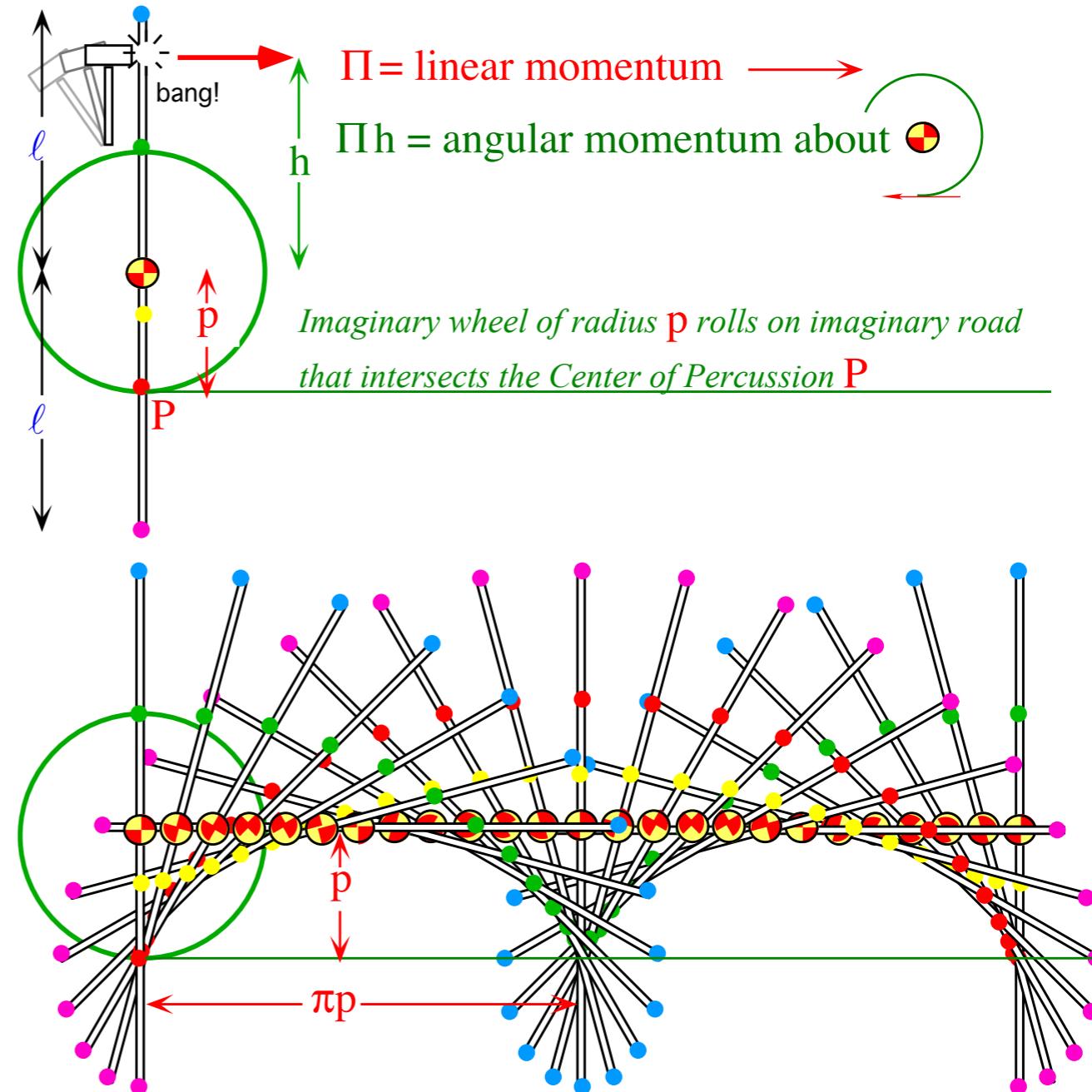


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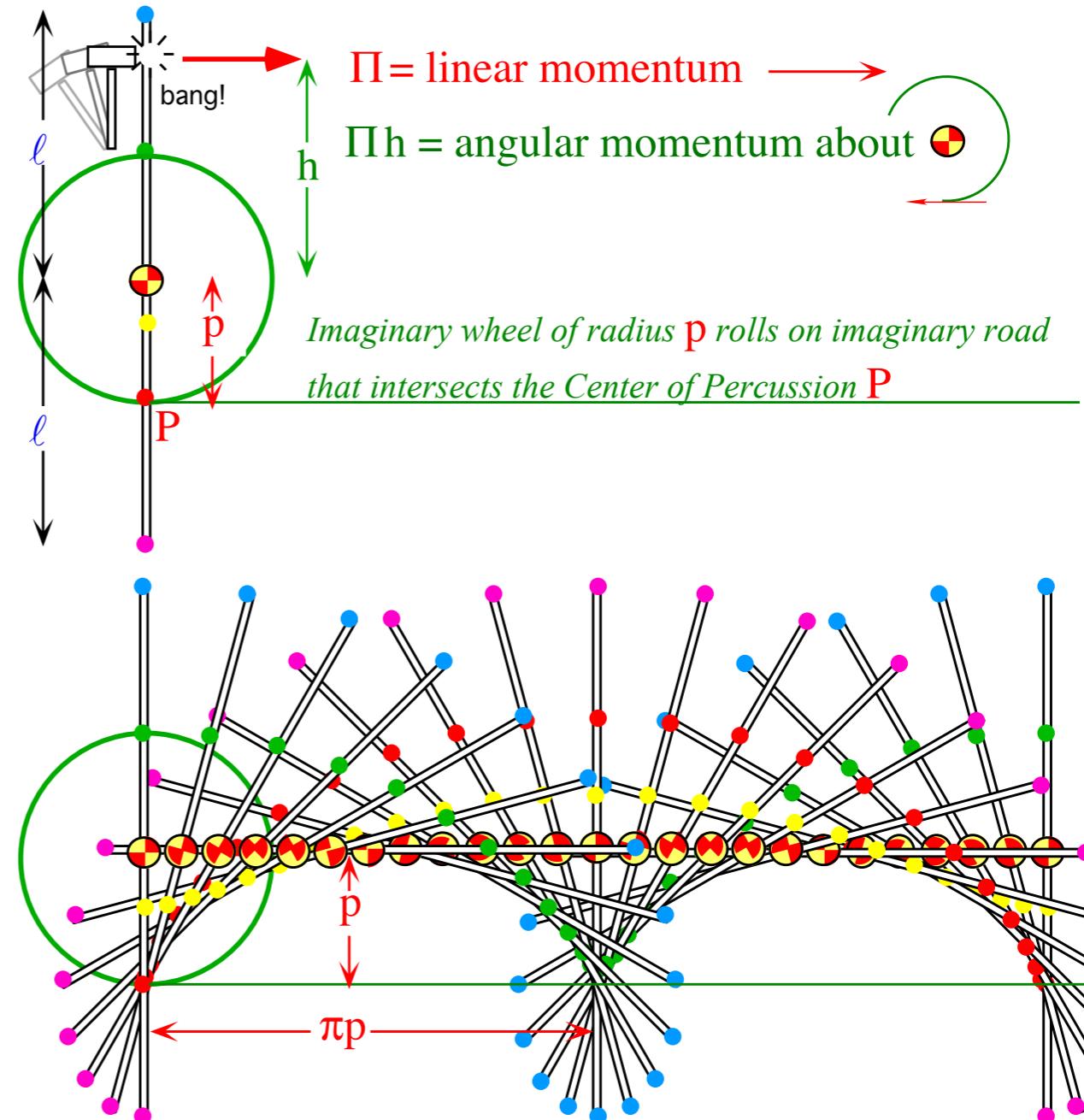


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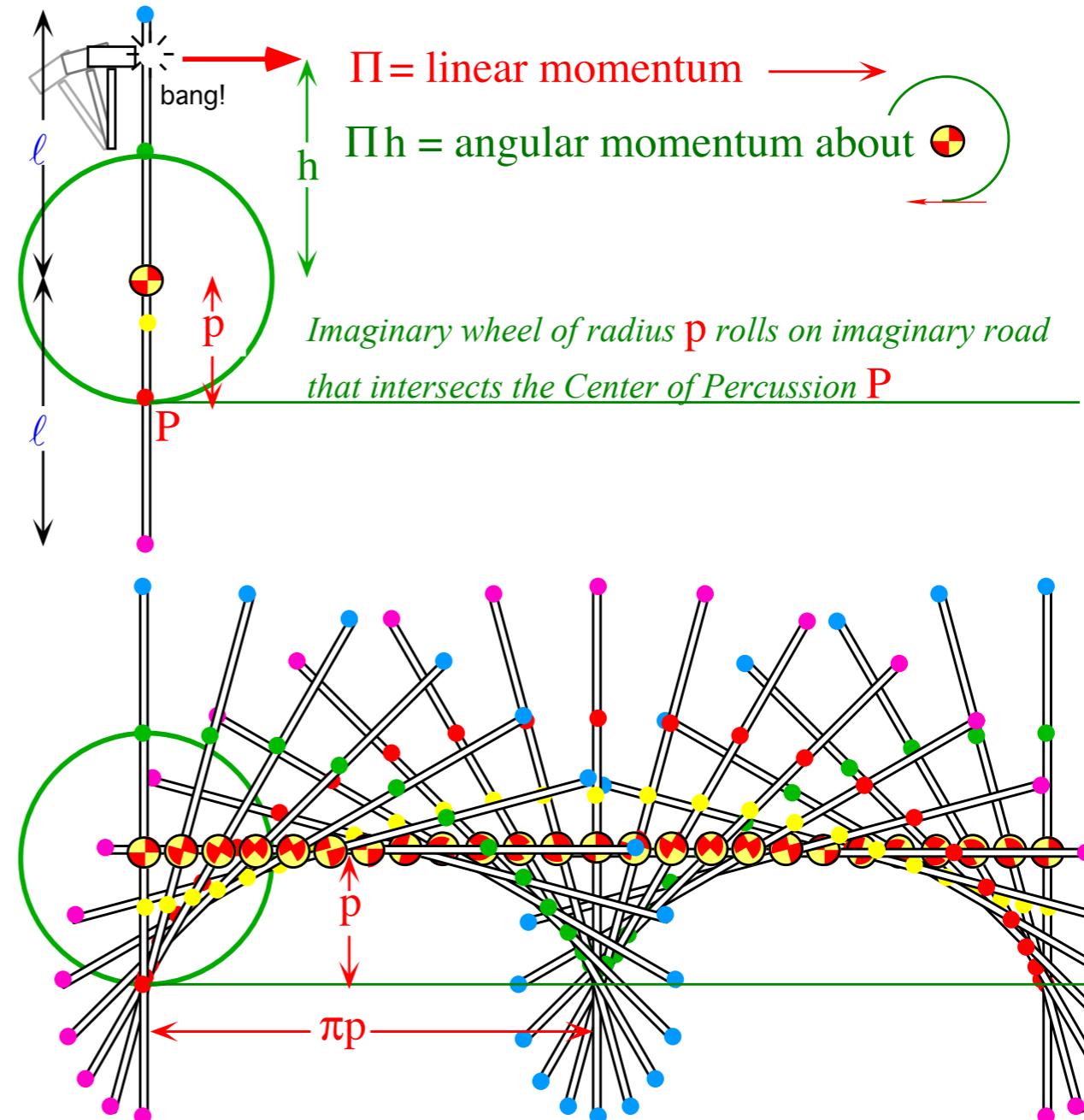


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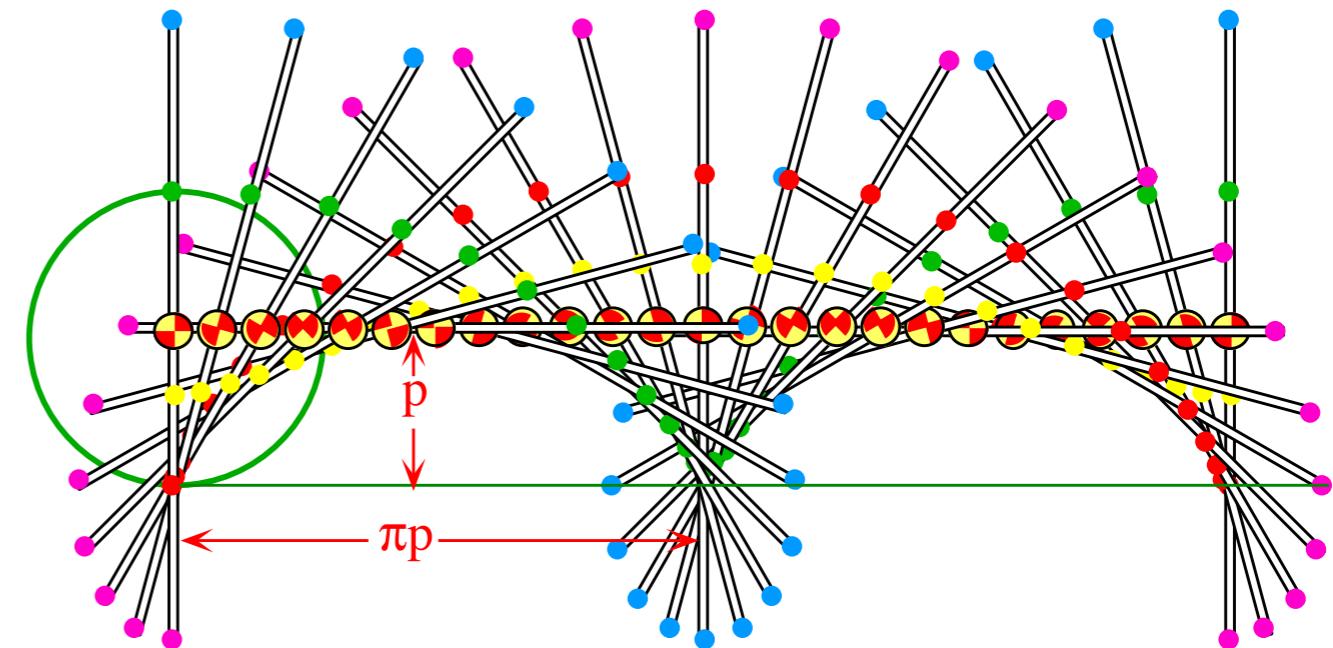
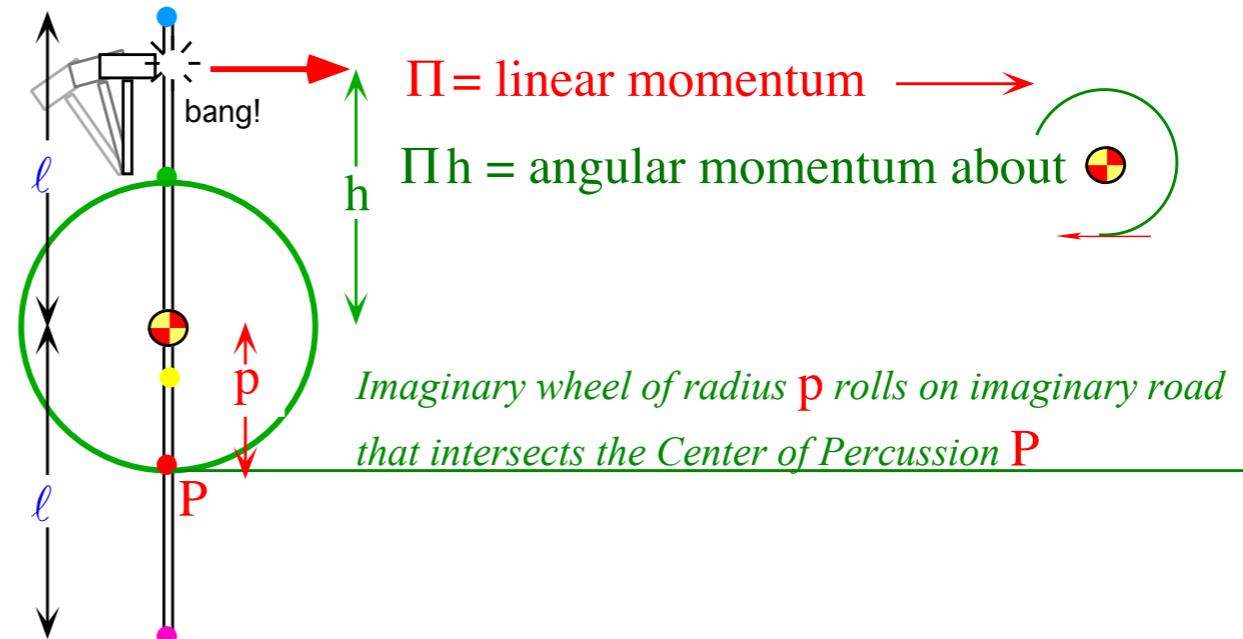


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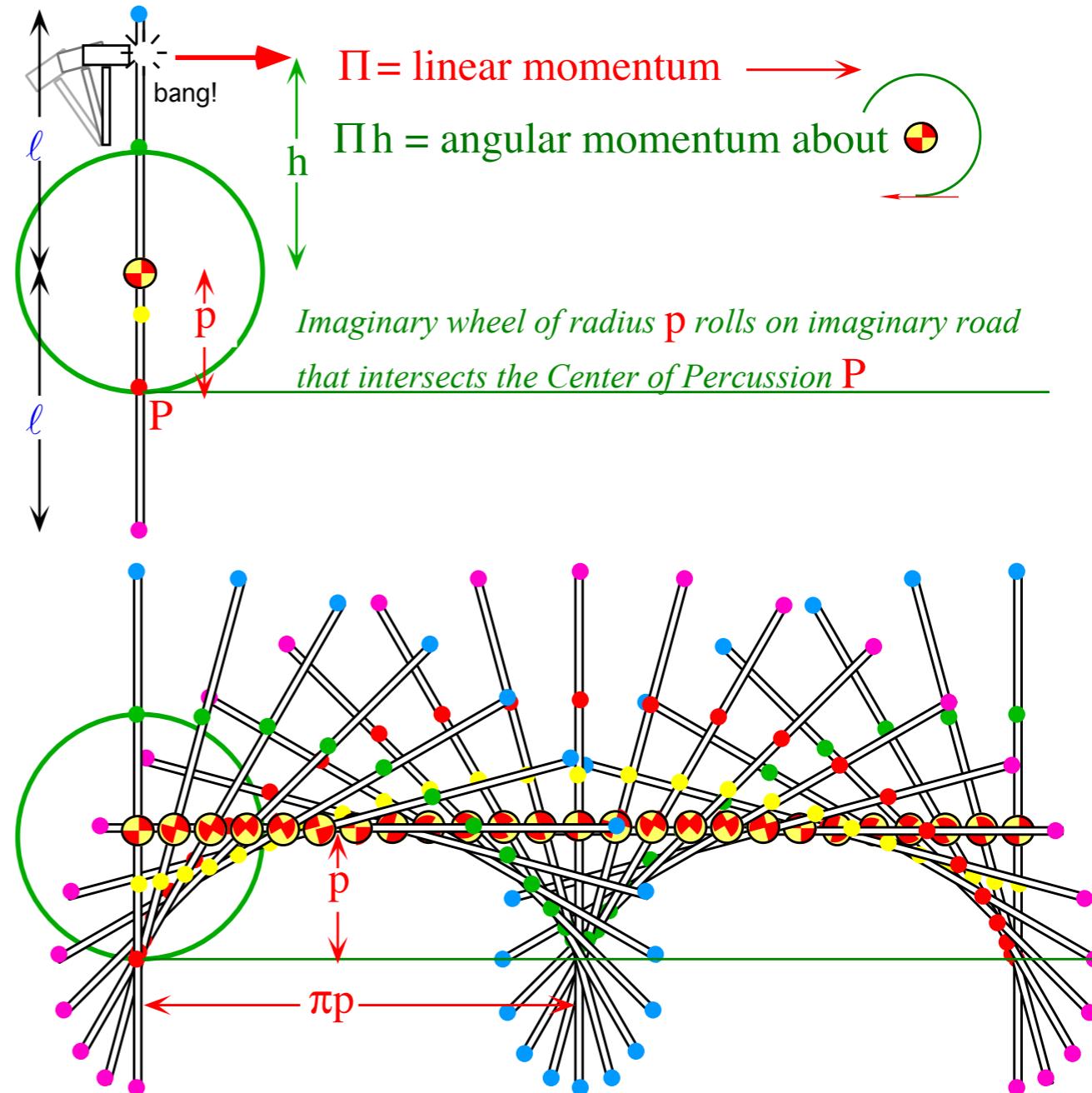


Fig. 2.A.1 Cycloidal paths due to hitting a stationary stick.

The *percussion radius* $p = \ell^2/3h$ is of the CoP point that has no velocity just after hammer hits at h .

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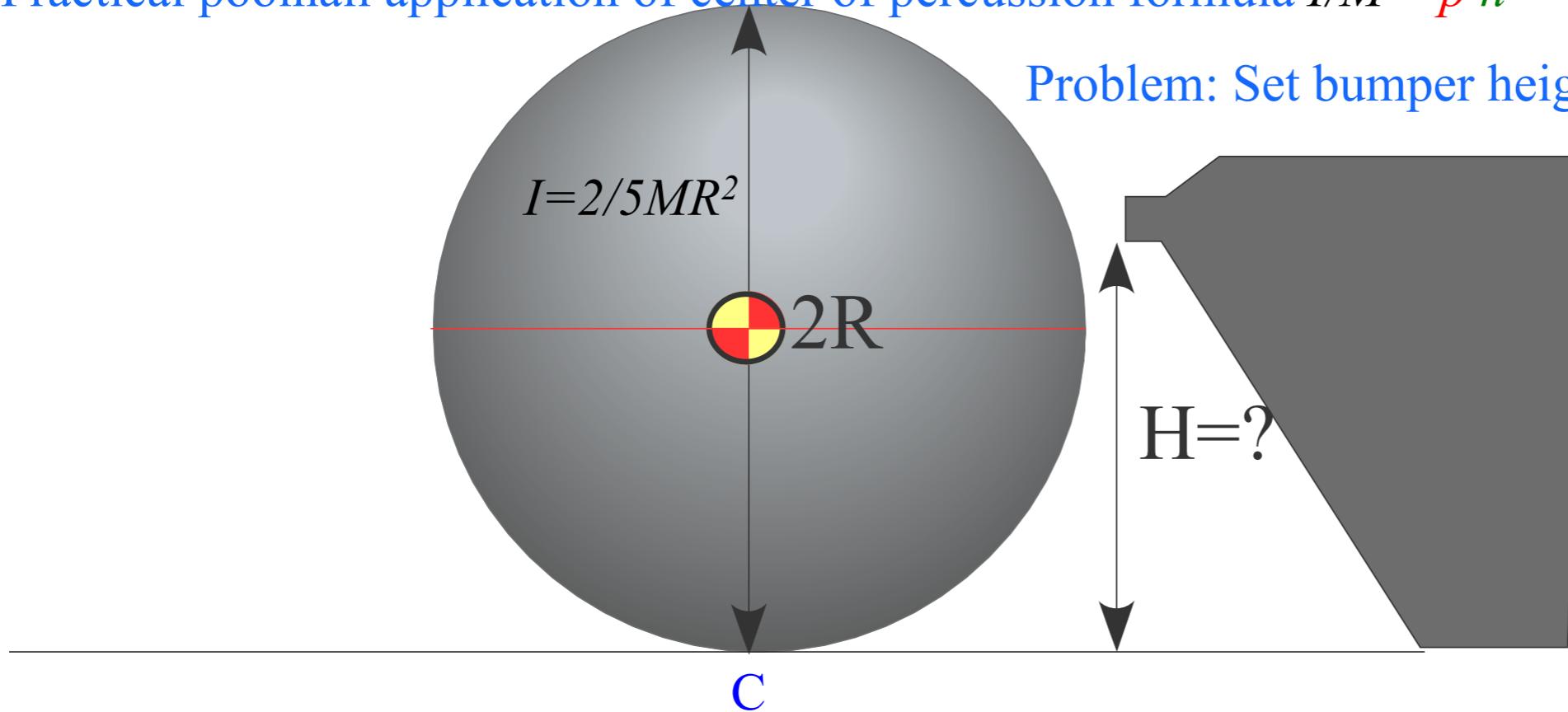
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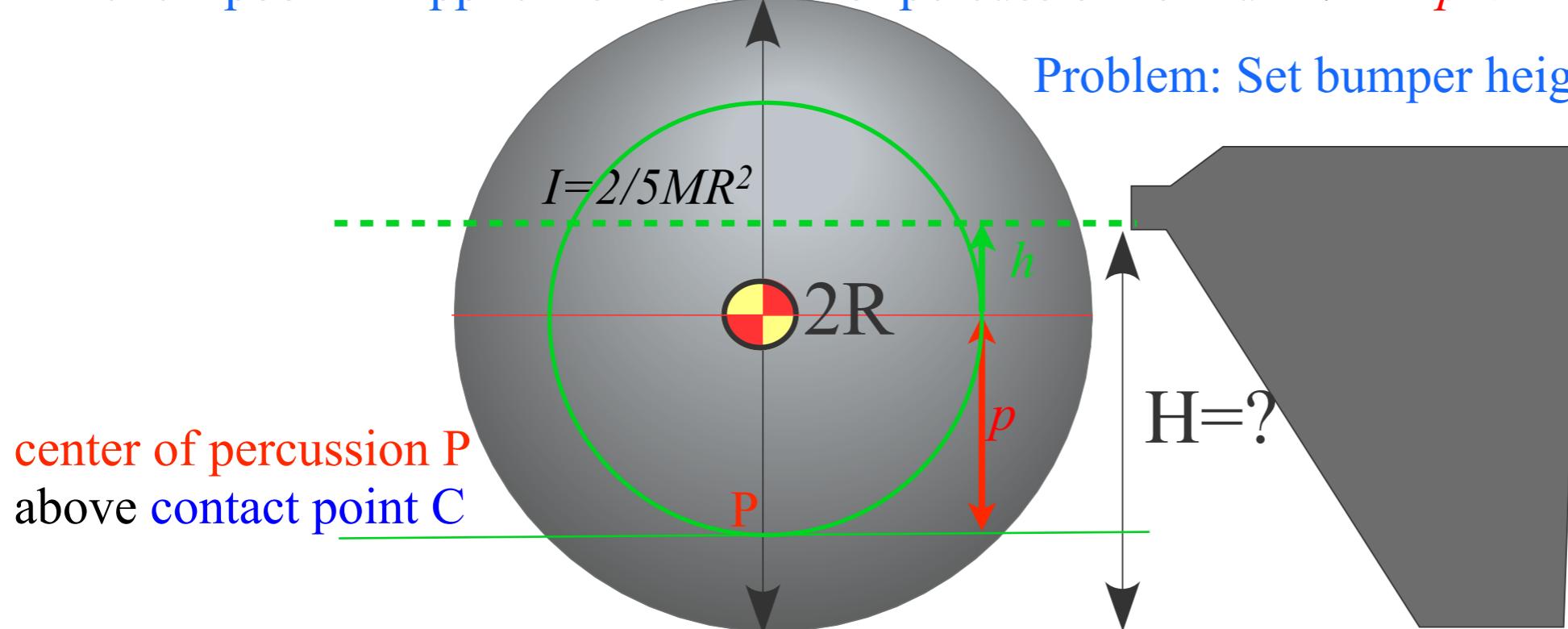
→ *Practical poolhall application*

Practical poolhall application of center of percussion formula $I/M = p \cdot h$

Problem: Set bumper height H so ball does not skid.



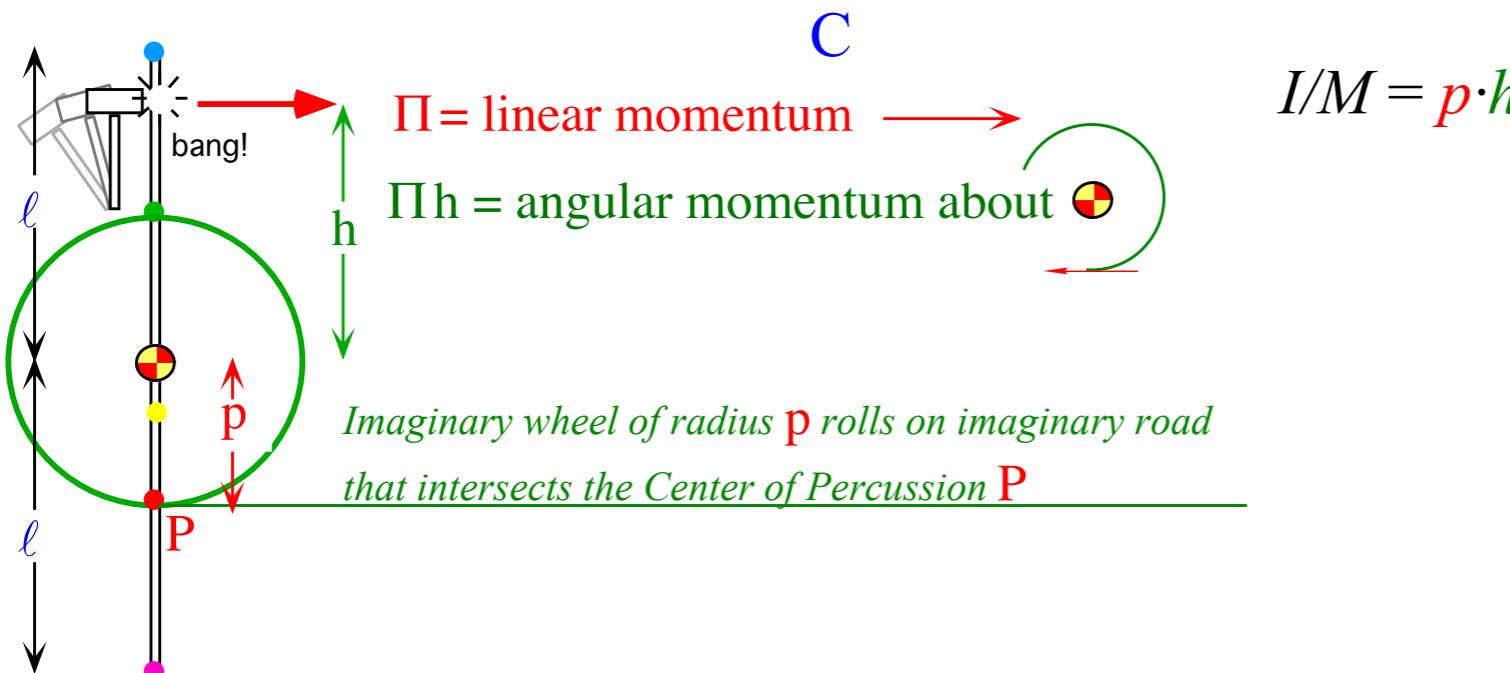
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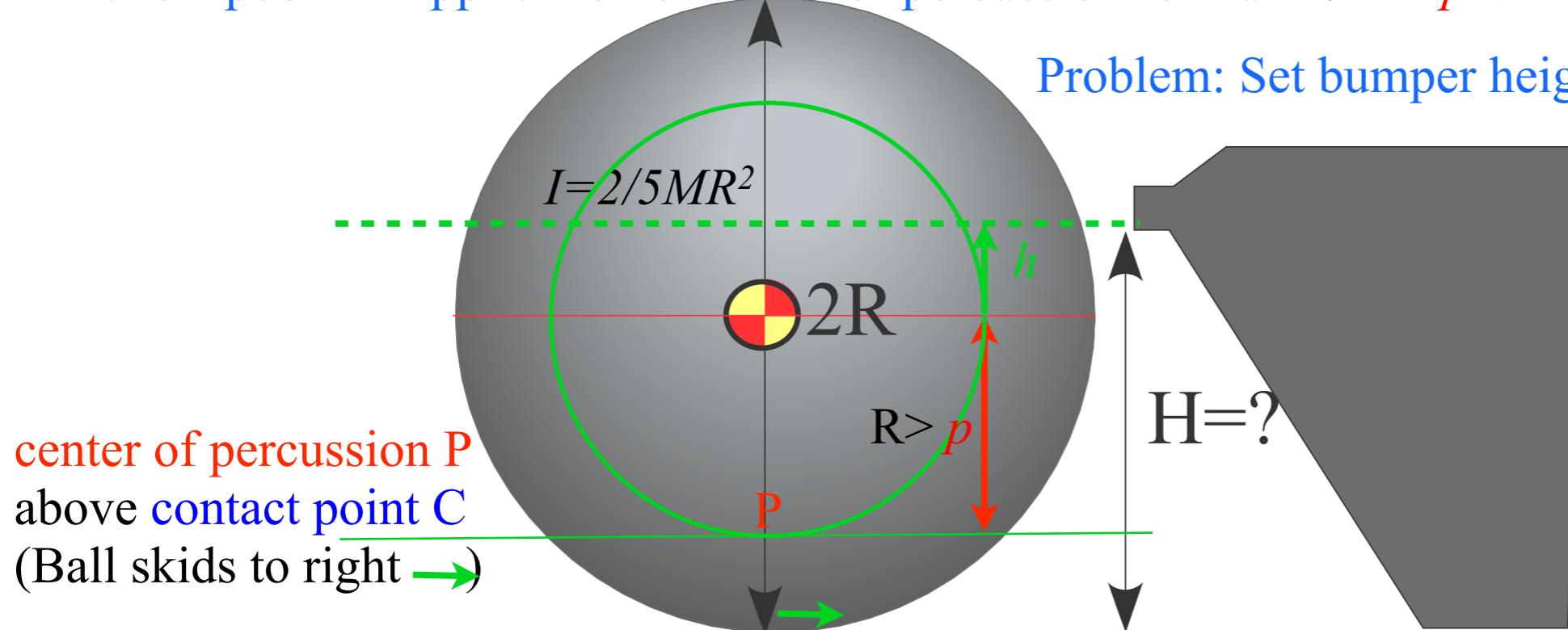
center of percussion P
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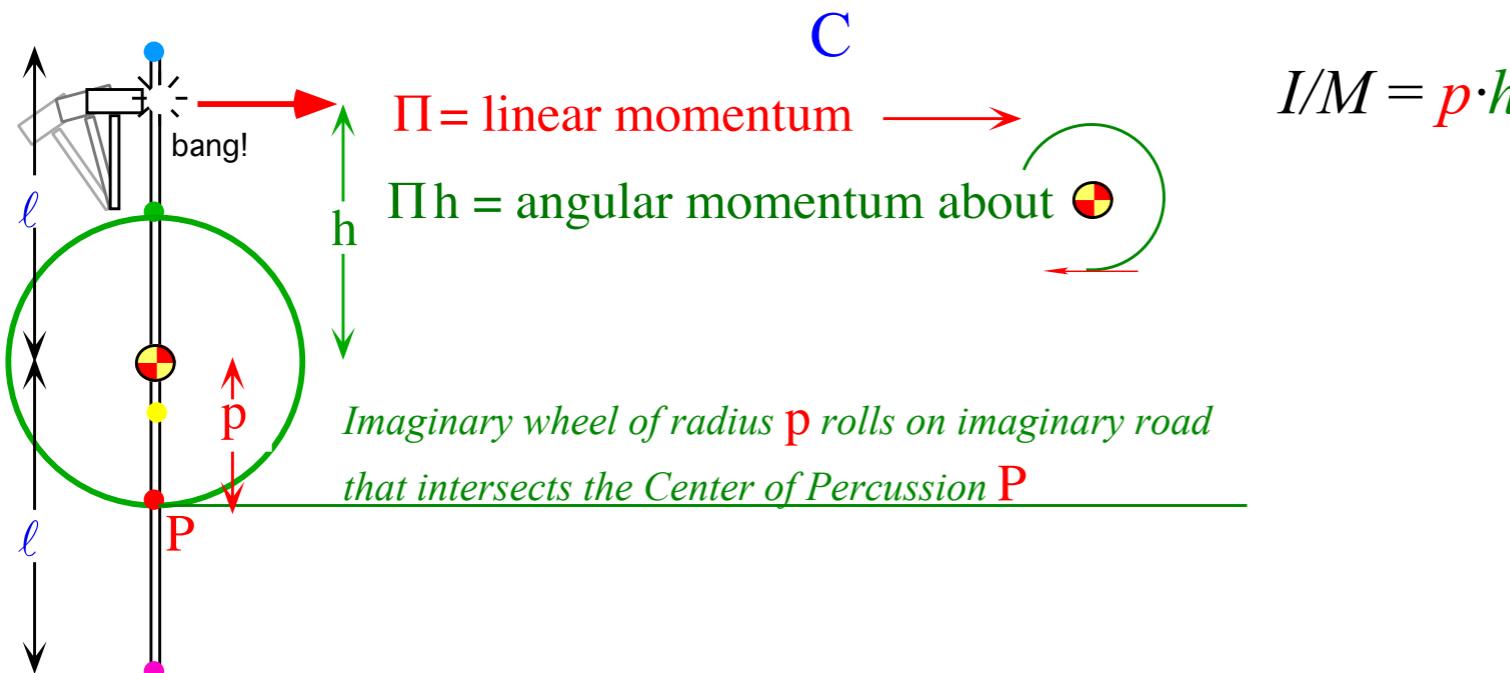
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center of percussion P
above contact point C
(Ball skids to right →)

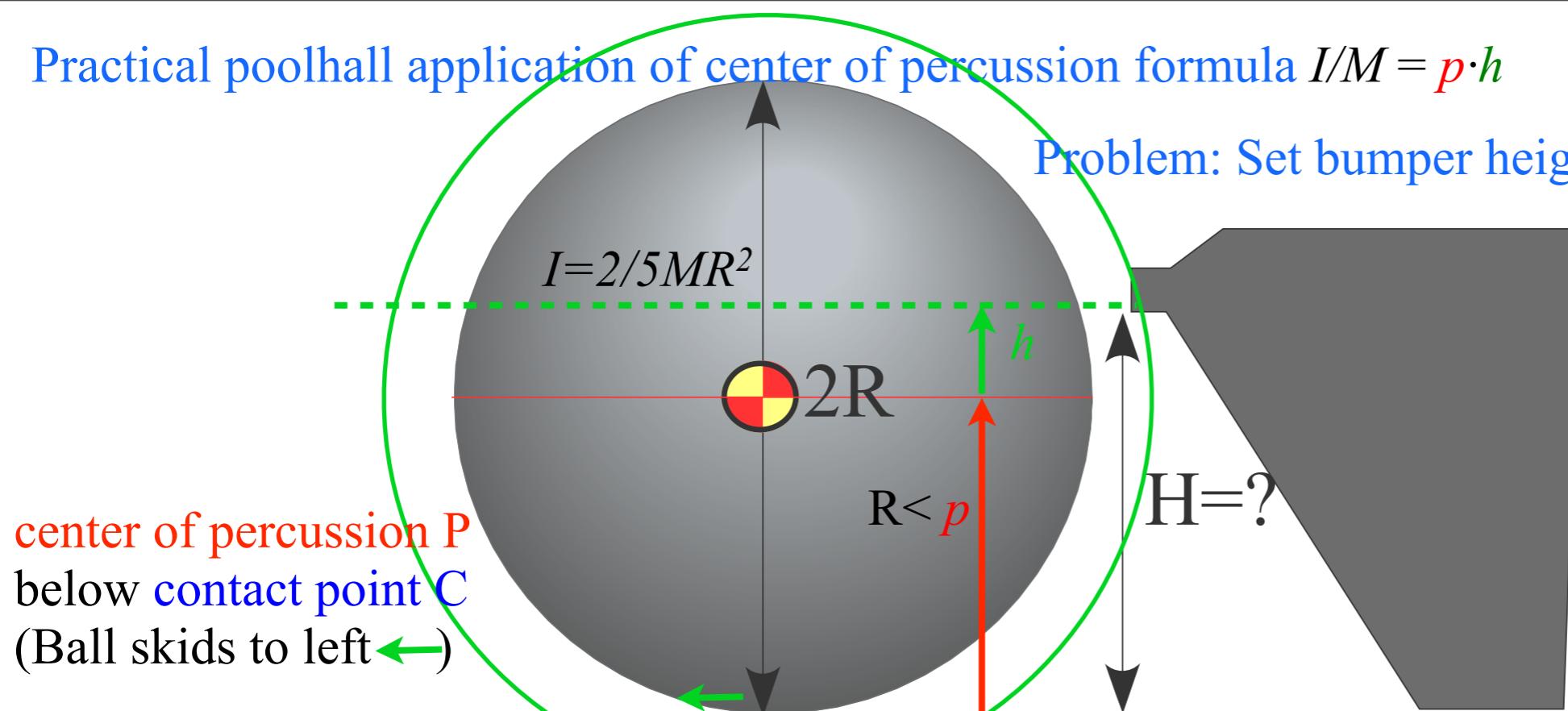
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$$I/M = p \cdot h$$

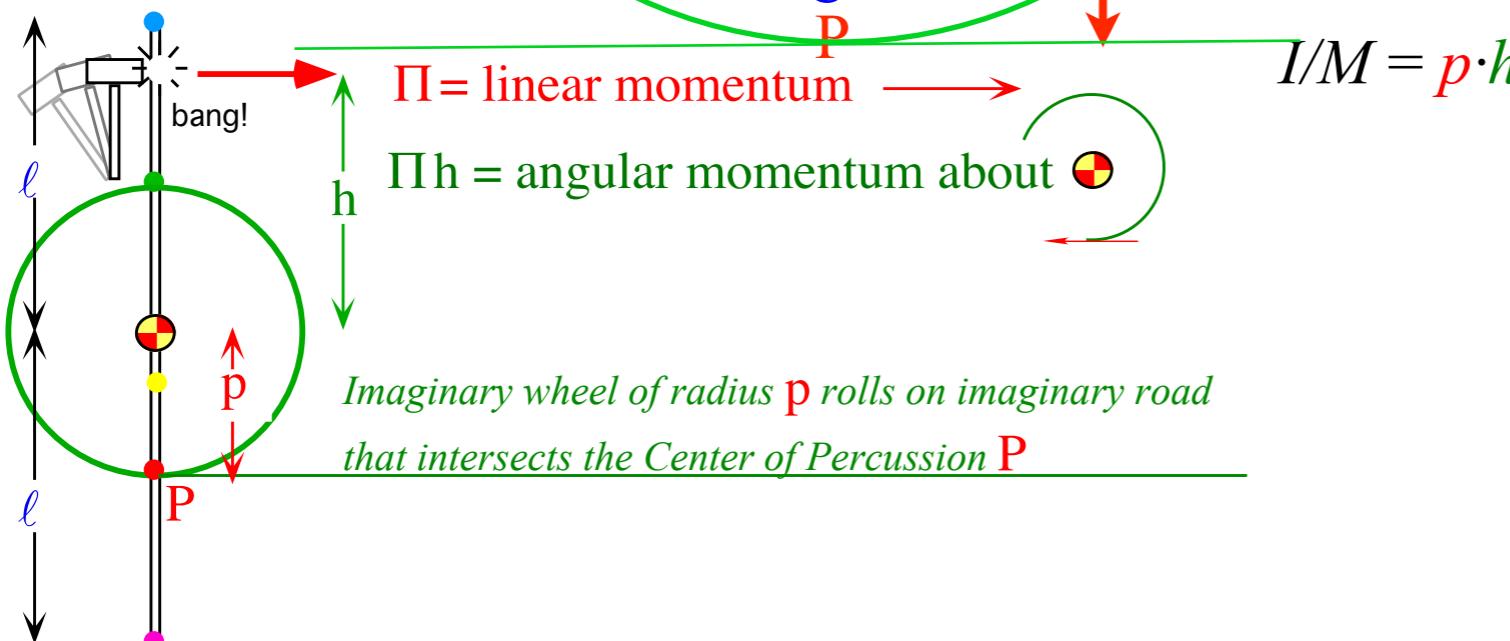
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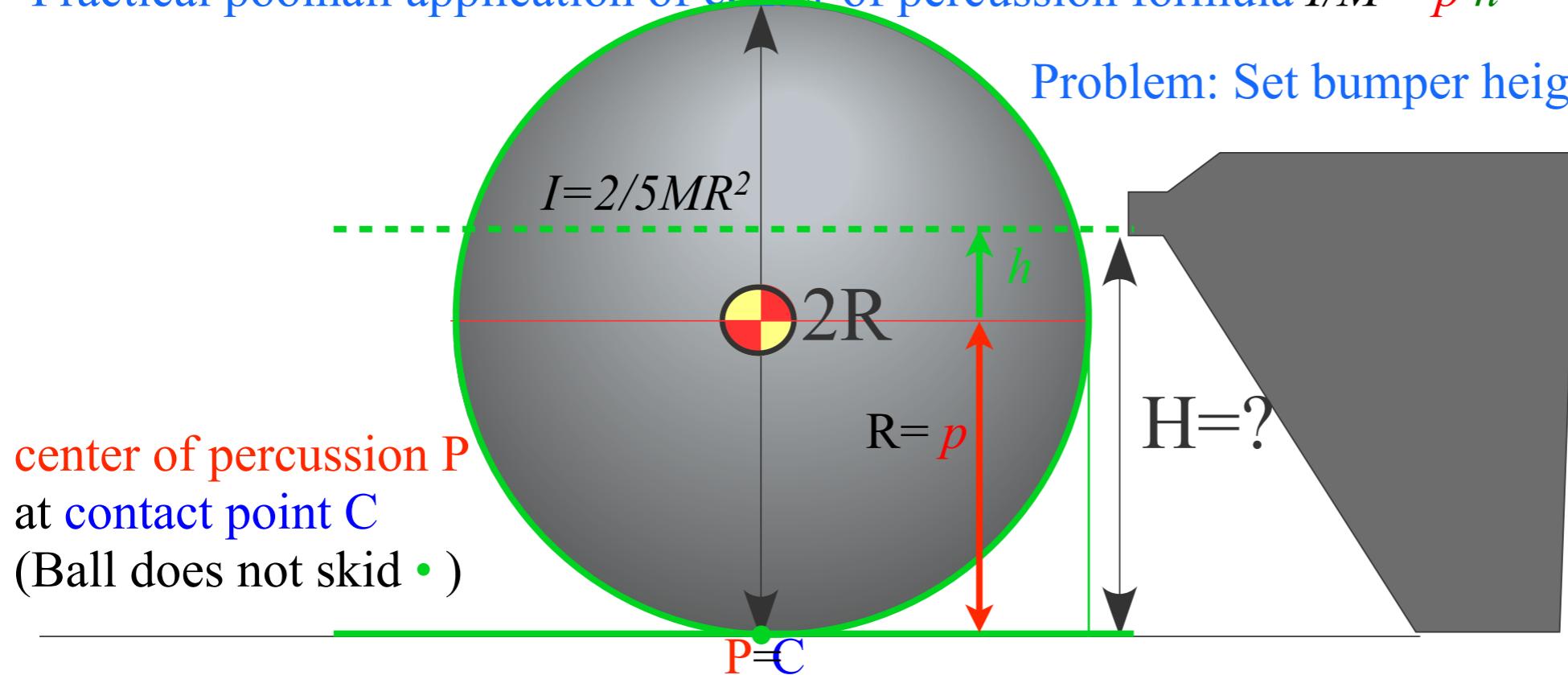
center of percussion P
below contact point C
(Ball skids to left ←)

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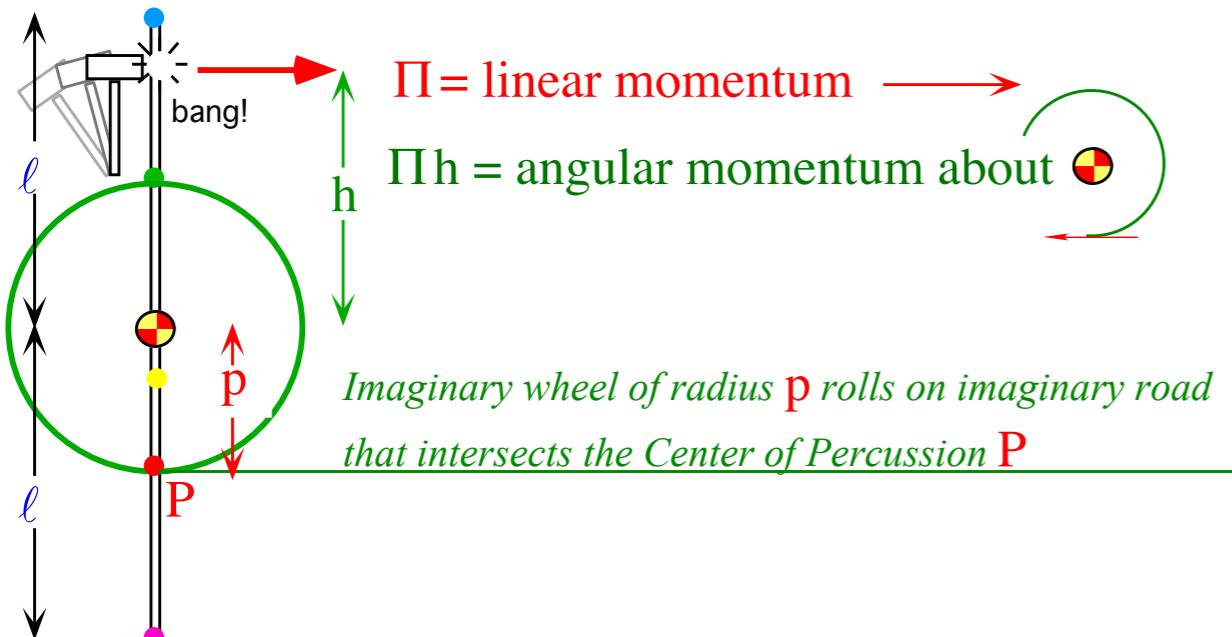
Practical poolhall application of center of percussion formula $I/M = p \cdot h$



center of percussion P
at contact point C
(Ball does not skid •)

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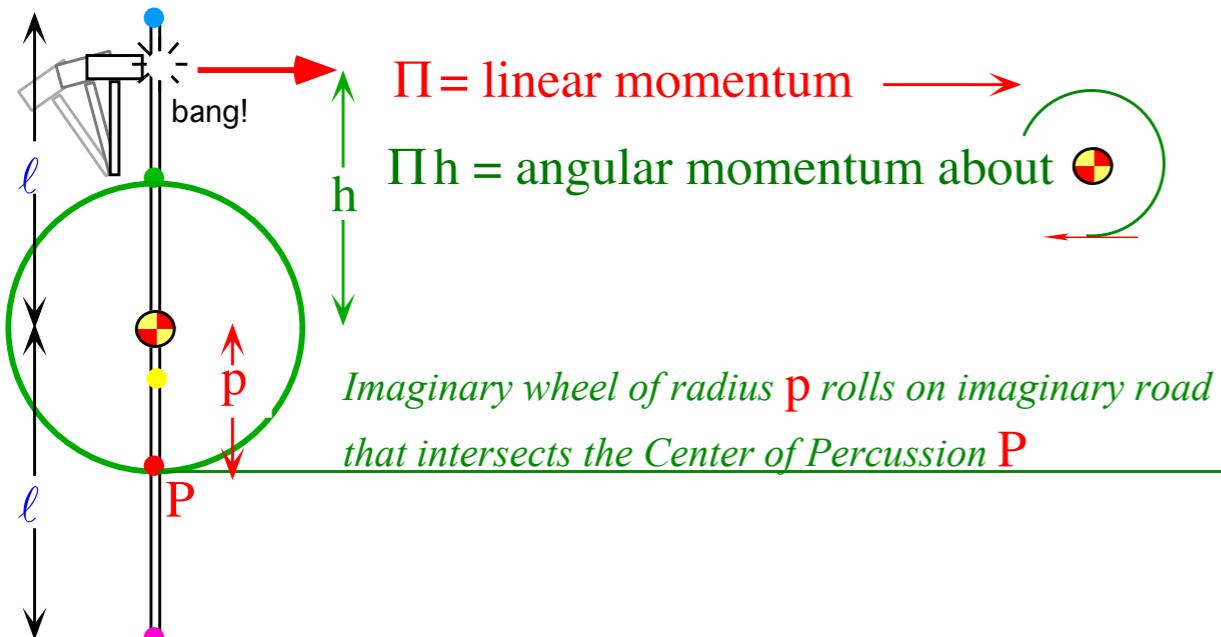
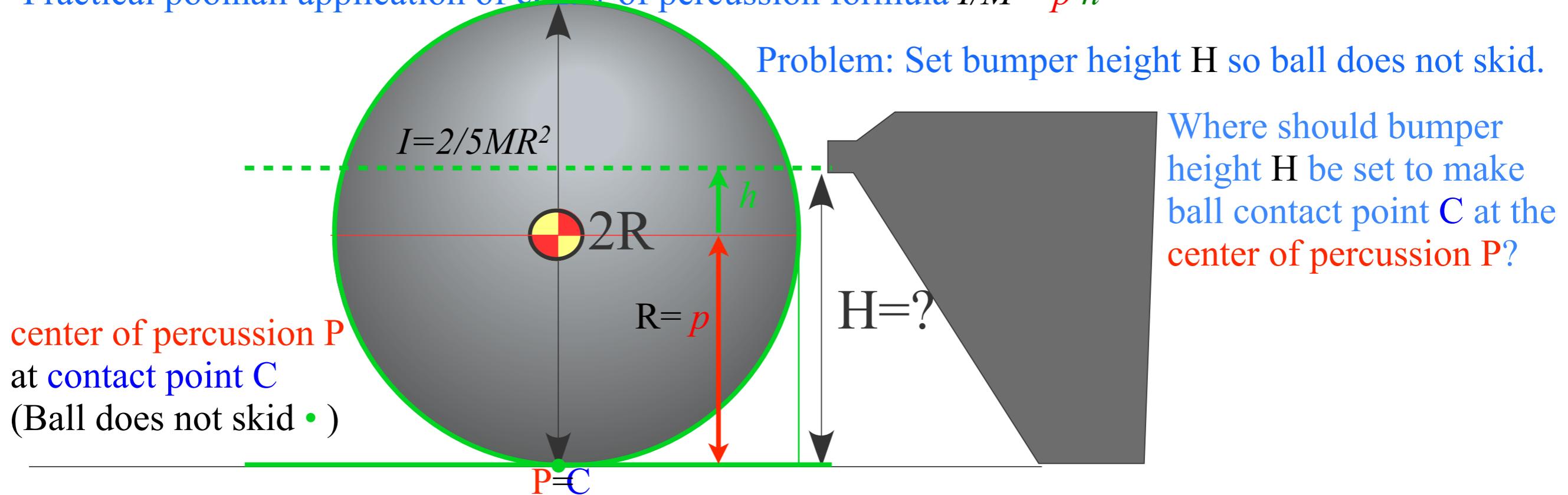


$$I/M = p \cdot h$$

$$h = I/Mp = I/MR$$

(For $R = p$)

Practical poolhall application of center of percussion formula $I/M = p \cdot h$



$$\begin{aligned} I/M &= p \cdot h \\ h &= I/Mp = I/MR \quad (\text{For } R = p) \\ &= 2/5MR^2/MR \\ &= 2/5R \end{aligned}$$

For: $H = R + h = 7/10(2R)$ ball does not skid.

Thats all folks!

